

# 摄动方法在薄板弯曲问题中的某些应用

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(1979年8月收到)

## 摘 要

本文应用摄动方法研究了薄板在侧向载荷和中面力的联合作用下的弯曲问题。

## 引 论

五十年代以来,人们开始广泛地应用摄动方法来研究薄板、薄壳的弯曲和稳定性问题,得到许多重要的结果<sup>[1]—[6]</sup>。1968年,W. E. Alzheimer和R. T. Davis<sup>[6]</sup>曾研究了环形薄板在中面力作用下的弯曲问题,在该文中假设中面力:  $N_r = N_\theta = N$  (常数) 和  $N_{r\theta} = 0$  本文对环形薄板和圆薄板在侧向载荷和中面力的联合作用下作了一般的研究。

## 一、环 形 薄 板

采用极坐标系 $(r, \theta)$ , 我们知道薄板在侧向载荷和中面力联合作用下的挠度曲面微分方程为<sup>[7]</sup>

$$\Delta \Delta W - \frac{1}{D} \left[ q + N_r(r, \theta) \frac{\partial^2 W}{\partial r^2} + N_\theta(r, \theta) \left( \frac{1}{r} \frac{\partial W}{\partial r} + \frac{1}{r^2} \frac{\partial^2 W}{\partial \theta^2} \right) + 2 N_{r\theta} \frac{\partial}{\partial r} \left( \frac{1}{r} \frac{\partial W}{\partial \theta} \right) \right] = 0 \quad (1.1)$$

其中  $W(r, \theta)$  表示挠度函数;  $N_r, N_\theta$  和  $N_{r\theta}$  分别表示中面上单位长度所作用的径向力, 环向力和剪力;  $D = \frac{Eh^3}{12(1-\nu^2)}$  表示板的弯曲刚度,  $h$  表示板的厚度,  $E$  表示弹性模数,  $\nu$  表示泊松比,  $\Delta$  是拉普拉斯算子:

$$\Delta \equiv \frac{\partial^2}{\partial r^2} + \frac{1}{r} \frac{\partial}{\partial r} + \frac{1}{r^2} \frac{\partial^2}{\partial \theta^2}$$

设板的内缘的半径为  $r_0$ , 外缘的半径为  $r_1$ , 引进无量纲量:

$$\tilde{W} = \frac{W}{h}, \tilde{r} = \frac{r}{r_1}, \tilde{N}_r = \frac{N_r}{r_1 E}, \tilde{N}_\theta = \frac{N_\theta}{r_1 E}, \tilde{N}_{r\theta} = \frac{N_{r\theta}}{r_1 E}, \tilde{q} = \frac{r_1 q}{h E}$$

方程(1.1)化为 (省去了字母上的“~”号)

$$\varepsilon^2 \Delta \Delta W - \left[ q + N_r \frac{\partial^2 W}{\partial r^2} + N_\theta \left( \frac{1}{r} \frac{\partial W}{\partial r} + \frac{1}{r^2} \frac{\partial^2 W}{\partial \theta^2} \right) \right]$$

$$+ 2 N_{r\theta} \frac{\partial}{\partial r} \left( \frac{1}{r} \frac{\partial W}{\partial \theta} \right) = 0 \quad (1.2)$$

$$\text{式中 } \varepsilon^2 = \frac{h^3}{12(1-\nu^2)r_1^3}, \quad b = \frac{r_0}{r_1}$$

为了便于和[6]的结果相比较,先考察第一类边值问题,给出边界条件:

$$W \Big|_{r=b} = f_0(\theta), \quad \frac{\partial W}{\partial r} \Big|_{r=b} = g_0(\theta) \quad (1.3)$$

$$W \Big|_{r=r_1} = f_1(\theta), \quad \frac{\partial W}{\partial r} \Big|_{r=r_1} = g_1(\theta) \quad (1.4)$$

对于其它类型的边界条件可以类似地处理(见[注2])。

$$\text{记 } A(r, \theta) = N_r(r, \theta), \quad B(r, \theta) = \frac{N_{r\theta}(r, \theta)}{r}, \quad C(r, \theta) = \frac{N_\theta(r, \theta)}{r^2},$$

$$D(r, \theta) = \frac{N_\theta(r, \theta)}{r}, \quad E(r, \theta) = \frac{-2 N_{r\theta}(r, \theta)}{r^2}, \quad \text{将方程(1.2)写成}$$

$$L_\varepsilon[W] \equiv \varepsilon^2 \Delta \Delta W - \left[ q + A(r, \theta) \frac{\partial^2 W}{\partial r^2} + 2B(r, \theta) \frac{\partial^2 W}{\partial r \partial \theta} + C(r, \theta) \frac{\partial^2 W}{\partial \theta^2} + D(r, \theta) \frac{\partial W}{\partial r} + E(r, \theta) \frac{\partial W}{\partial \theta} \right] = 0 \quad (1.2')$$

本文只考察  $N_r > 0$ ,  $N_r N_\theta - N_{r\theta}^2 > 0$  的情形,即作用于中面内的径向力,环向力都是拉力,并且剪力是充分小。这时  $A > 0$ ,  $AC - B^2 > 0$ , 退化方程(令  $\varepsilon = 0$  所得的方程)是椭圆型的。

### 1. 外部解

先应用正则摄动方法求其外部解,即在边缘的  $\varepsilon$  邻域的外部区域有意义的解。假设挠度函数关于  $\varepsilon$  的 Taylor 展开式是

$$W(r, \theta; \varepsilon) = \sum_{n=0}^{\infty} \varepsilon^n W_n(r, \theta) \quad (1.5)$$

代入方程(1.2'),令  $\varepsilon$  的各次幂的系数为零,得到关于  $W_n$ , ( $n=0, 1, \dots$ ) 的递推方程:

$$F[W_0] \equiv A \frac{\partial^2 W_0}{\partial r^2} + 2B \frac{\partial^2 W_0}{\partial r \partial \theta} + C \frac{\partial^2 W_0}{\partial \theta^2} + D \frac{\partial W_0}{\partial r} + E \frac{\partial W_0}{\partial \theta} = -q \quad (1.6)$$

$$F[W_n] = \Delta \Delta W_{n-2} \quad (n=1, 2, \dots) \quad (1.7)$$

在上式以及以后的计算中,都将带负下标的量取作零。方程(1.6)和(1.7)都是二阶线性椭圆型方程,一般不存在满足全部边界条件(1.3)–(1.4)的解,因此根据递推方程所得的展开式在边界上与原边值问题有间断,即存在着边界层。下面再应用参考文献[8]的方法构造边界层中的校正项(简称为边界层项)。

### 2. 边界层项

先在内缘  $r=b$  的邻域构造边界层项。在  $r=b$  的邻域引进两变量  $\xi$  和  $\eta$ :

$$\xi = \frac{u(r, \theta)}{\varepsilon}, \quad \eta = r \quad (1.8)$$

将关于  $r$  的偏导数换成关于变量  $\xi$  和  $\eta$  的偏导数:

$$\begin{aligned} \frac{\partial}{\partial r} &= \frac{\partial \xi}{\partial r} \frac{\partial}{\partial \xi} + \frac{\partial \eta}{\partial r} \frac{\partial}{\partial \eta} = \varepsilon^{-1}(\delta_{1,0} + \varepsilon \delta_{1,1}), \\ \frac{\partial^2}{\partial r^2} &= \varepsilon^{-2}(\delta_{2,0} + \varepsilon \delta_{2,1} + \varepsilon^2 \delta_{2,2}) \\ \frac{\partial^3}{\partial r^3} &= \varepsilon^{-3}(\delta_{3,0} + \varepsilon \delta_{3,1} + \varepsilon^2 \delta_{3,2} + \varepsilon^3 \delta_{3,3}) \\ \frac{\partial^4}{\partial r^4} &= \varepsilon^{-4}(\delta_{4,0} + \varepsilon \delta_{4,1} + \varepsilon^2 \delta_{4,2} + \varepsilon^3 \delta_{4,3} + \varepsilon^4 \delta_{4,4}) \\ \frac{\partial^2}{\partial r \partial \theta} &= \frac{\partial \xi}{\partial r} \frac{\partial^2}{\partial \xi \partial \theta} + \frac{\partial \eta}{\partial r} \frac{\partial^2}{\partial \eta \partial \theta} = \varepsilon^{-1}(\delta_{1,0,\theta} + \varepsilon \delta_{1,1,\theta}) \\ &\dots\dots\dots \end{aligned}$$

式中:

$$\begin{aligned} \delta_{1,0} &= u_r \frac{\partial}{\partial \xi}, \quad \delta_{1,1} = \frac{\partial}{\partial \eta} \\ \delta_{2,0} &= u_r^2 \frac{\partial^2}{\partial \xi^2}, \quad \delta_{2,1} = 2u_r \frac{\partial^2}{\partial \xi \partial \eta} + u_{rr} \frac{\partial}{\partial \xi}, \quad \delta_{2,2} = \frac{\partial^2}{\partial \eta^2} \\ \delta_{3,0} &= u_r^3 \frac{\partial^3}{\partial \xi^3}, \quad \delta_{3,1} = 3u_r^2 \frac{\partial^3}{\partial \xi^2 \partial \eta} + 3u_r u_{rr} \frac{\partial^2}{\partial \xi^2}, \\ \delta_{3,2} &= 3u_r \frac{\partial^3}{\partial \xi \partial \eta^2} + 3u_{rr} \frac{\partial^2}{\partial \xi \partial \eta} + u_{rrr} \frac{\partial}{\partial \xi}, \quad \delta_{3,3} = \frac{\partial^3}{\partial \eta^3} \\ \delta_{4,0} &= u_r^4 \frac{\partial^4}{\partial \xi^4}, \quad \delta_{4,1} = 4u_r^3 \frac{\partial^4}{\partial \xi^3 \partial \eta} + 6u_r^2 u_{rr} \frac{\partial^3}{\partial \xi^3}, \quad \delta_{4,2} = 6u_r^2 \frac{\partial^4}{\partial \xi^2 \partial \eta^2} \\ &\quad + 12u_r u_{rr} \frac{\partial^3}{\partial \xi^2 \partial \eta} + 4u_r u_{rrr} \frac{\partial^2}{\partial \xi^2} + 3u_r^2 \frac{\partial^2}{\partial \xi^2}, \quad \delta_{4,3} = 4u_r \frac{\partial^4}{\partial \xi \partial \eta^3} \\ &\quad + 6u_{rr} \frac{\partial^3}{\partial \xi \partial \eta^2} + 4u_{rrr} \frac{\partial^2}{\partial \xi \partial \eta} + u_{rrrr} \frac{\partial}{\partial \xi}, \quad \delta_{4,4} = \frac{\partial^4}{\partial \eta^4} \\ \delta_{1,0,\theta} &= u_r \frac{\partial^2}{\partial \xi \partial \theta} = \delta_{1,0} \frac{\partial}{\partial \theta}, \quad \delta_{1,1,\theta} = \frac{\partial^2}{\partial \eta \partial \theta} = \delta_{1,1} \frac{\partial}{\partial \theta} \end{aligned}$$

将  $\xi, \eta$  和  $\theta$  看成是三个独立的自变量, 将(1.2')所对应的齐次方程(令  $q \equiv 0$  所得的方程) 变换成

$$\varepsilon^{-2}(K_0 + \varepsilon K_1 + \varepsilon^2 K_2 + \varepsilon^3 K_3 + \varepsilon^4 K_4)[W] = 0. \tag{1.9}$$

式中

$$\begin{aligned} K_0 &\equiv u_r^4 \frac{\partial^4}{\partial \xi^4} - Au_r^2 \frac{\partial^2}{\partial \xi^2} \\ K_1 &\equiv 4u_r^3 \frac{\partial^4}{\partial \xi^3 \partial \eta} + \left( 6u_r^2 u_{rr} + \frac{2}{\eta} u_r^3 \right) \frac{\partial^3}{\partial \xi^3} - 2Au_r \frac{\partial^2}{\partial \xi \partial \eta} - 2Bu_r \frac{\partial^2}{\partial \xi \partial \theta} \\ &\quad - (Au_{rr} + Du_r) \frac{\partial}{\partial \xi} \end{aligned}$$

$$\begin{aligned}
K_2 &\equiv 6u_r^2 \frac{\partial^4}{\partial \xi^2 \partial \eta^2} + \left( 12u_r u_{rr} + \frac{6}{\eta} u_r^2 \right) \frac{\partial^3}{\partial \xi^2 \partial \eta} + \left( 4u_r u_{rrr} - \frac{u_r^2}{\eta^2} + 3u_r^2 + \frac{6}{\eta} u_r u_{rr} \right) \frac{\partial^2}{\partial \xi^2} \\
&\quad + \frac{2}{\eta^2} u_r^2 \frac{\partial^4}{\partial \xi^2 \partial \theta^2} - A \frac{\partial^2}{\partial \eta^2} - 2B \frac{\partial^2}{\partial \eta \partial \theta} - C \frac{\partial^2}{\partial \theta^2} - D \frac{\partial}{\partial \eta} - E \frac{\partial}{\partial \theta} \\
K_3 &\equiv 4u_r \frac{\partial^4}{\partial \xi \partial \eta^3} + \left( 6u_{rr} + \frac{6}{\eta} u_r \right) \frac{\partial^3}{\partial \xi \partial \eta^2} + \left( 4u_{rrr} + \frac{6}{\eta} u_{rr} - \frac{2}{\eta^2} u_r \right) \frac{\partial^2}{\partial \xi \partial \eta} \\
&\quad + \frac{4u_r}{\eta^2} \frac{\partial^4}{\partial \xi \partial \eta \partial \theta^2} + \left( \frac{2u_{rr}}{\eta^2} - \frac{2u_r}{\eta^3} \right) \frac{\partial^3}{\partial \xi \partial \theta^2} + \left( u_{rrrr} - \frac{u_{rr}}{\eta^2} + \frac{2}{\eta} u_{rrr} + \frac{u_r}{\eta^3} \right) \frac{\partial}{\partial \xi} \\
K_4 &\equiv \frac{\partial^4}{\partial \eta^4} + \frac{2}{\eta} \frac{\partial^3}{\partial \eta^3} + \frac{2}{\eta^2} \frac{\partial^4}{\partial \eta^2 \partial \theta^2} - \frac{1}{\eta^2} \frac{\partial^2}{\partial \eta^2} - \frac{2}{\eta^3} \frac{\partial^3}{\partial \eta \partial \theta^2} + \frac{1}{\eta^3} \frac{\partial}{\partial \eta} \\
&\quad + \frac{1}{\eta^4} \frac{\partial^4}{\partial \theta^4} + \frac{4}{\eta^4} \frac{\partial^2}{\partial \theta^2}
\end{aligned}$$

假设内缘  $r=b$  邻域的边界层项具有下面形式的展开式:

$$V^{(b)}(\xi, \eta, \theta; \epsilon) = \sum_{n=0}^{\infty} \epsilon^{n+1} v_n^{(b)}(\xi, \eta, \theta) \quad (1.10)$$

代入方程 (1.9), 并令  $\epsilon$  的各次幂的系数为零, 得到关于  $v_n^{(b)}$  ( $n=0, 1, \dots$ ) 的递推方程:

$$K_0[v_0^{(b)}] \equiv u_r^2 \frac{\partial^4 v_0^{(b)}}{\partial \xi^4} - A u_r^2 \frac{\partial^2 v_0^{(b)}}{\partial \xi^2} = 0 \quad (1.11)$$

$$K_0[v_n^{(b)}] = - \sum_{s=1}^4 K_s[v_{n-s}^{(b)}], \quad (n=1, 2, \dots) \quad (1.12)$$

在方程 (1.11) 中, 若取  $u_r = A^{1/2}$ , 即取

$$u(\eta, \theta) = \int_b^\eta \sqrt{A(t, \theta)} dt > 0 \quad (1.13)$$

则得到常系数方程:

$$\frac{\partial^4 v_0^{(b)}}{\partial \xi^4} - \frac{\partial^2 v_0^{(b)}}{\partial \xi^2} = 0 \quad (1.14)$$

容易求得当  $\xi \rightarrow \infty$  时, 依指数函数规律趋于零的解 (称这种解具有“边界层项性质”) 为

$$v_0^{(b)} = C_0^{(b)}(\eta, \theta) \exp(-\xi) = C_0^{(b)}(r, \theta) \exp\left(-\epsilon^{-1} \int_b^\eta \sqrt{A(t, \theta)} dt\right). \quad (1.15)$$

式中  $C_0^{(b)}(\eta, \theta)$  是  $\eta$  和  $\theta$  的任意函数, 将由下面导出的关于  $C_0^{(b)}$  的一阶线性偏微分方程和以后导出的边界条件确定。

在递推方程 (1.12) 中令  $n=1$ , 得到关于  $v_1^{(b)}$  的偏微分方程:

$$K_0[v_1^{(b)}] = -K_1[v_0^{(b)}] \quad (1.16)$$

令上式的右端为零, 得到关于  $C_0^{(b)}$  的一阶线性偏微分方程:

$$2A \frac{\partial C_0^{(b)}}{\partial \eta} - 2B \frac{\partial C_0^{(b)}}{\partial \theta} + \left( \frac{5}{2} A_r + \frac{2A}{\eta_0} - D \right) C_0^{(b)} = 0 \quad (1.17)$$

这时  $v_1^{(b)}$  的偏微分方程 (1.16) 化为齐次方程:

$$\frac{\partial^4 v_1^{(b)}}{\partial \xi^4} - \frac{\partial^2 v_1^{(b)}}{\partial \xi^2} = 0$$

可以求得具有边界层性质的解为

$$v_1^{(b)} = C_1^{(b)}(\eta, \theta) \exp(-\xi) = C_1^{(b)}(r, \theta) \exp\left(-\varepsilon^{-1} \int_b^r \sqrt{A(t, \theta)} dt\right) \quad (1.18)$$

一般地, 假设已经求得  $v_i^{(b)}$  ( $i=0, 1, \dots, n-1$ ) 和

$$v_n^{(b)} = C_n^{(b)}(\eta, \theta) \exp(-\xi) = C_n^{(b)}(r, \theta) \exp\left(-\varepsilon^{-1} \int_b^r \sqrt{A(t, \theta)} dt\right)$$

式中  $C_n^{(b)}$  是尚未确定的任意函数, 再在递推方程 (1.12) 中取  $n$  为  $n+1$ , 得到关于  $v_{n+1}^{(b)}$  的偏微分方程:

$$K_0[v_{n+1}^{(b)}] = - \sum_{s=1}^4 K_s[v_{n+1-s}^{(b)}] \quad (1.19)$$

再令上式的右端为零, 则得到确定  $C_n^{(b)}$  的一阶线性偏微分方程:

$$K_1[v_n^{(b)}] = - \sum_{s=2}^4 K_s[v_{n+1-s}^{(b)}], \text{ 即}$$

$$2A \frac{\partial C_n^{(b)}}{\partial \eta} - 2B \frac{\partial C_n^{(b)}}{\partial \theta} + \left( \frac{5}{2} A_r + \frac{2}{\eta} A - D \right) C_n^{(b)} = A^{-\frac{1}{2}} (G_2[C_n^{(b)_1}] + G_3[C_n^{(b)_2}] + G_4[C_n^{(b)_3}]) \quad (1.20)$$

式中

$$\begin{aligned} G_2 &\equiv 5A \frac{\partial^2}{\partial \eta^2} + \left( \frac{2}{\eta^2} A - C \right) \frac{\partial^2}{\partial \theta^2} + \left( 6A_r + \frac{6}{\eta} A - D \right) \frac{\partial}{\partial \eta} \\ &\quad + \left( \frac{-1}{4} A^{-1} A_r^2 + 2A_{rr} - \frac{1}{\eta^2} A + \frac{3}{\eta} A_r \right) - 2B \frac{\partial^2}{\partial \eta \partial \theta} - E \frac{\partial}{\partial \theta} \\ G_3 &\equiv -4A^{\frac{1}{2}} \frac{\partial^3}{\partial \eta^3} - \frac{4}{\eta^2} A^{\frac{1}{2}} \frac{\partial^3}{\partial \eta \partial \theta^2} - \left( 3A^{-\frac{1}{2}} A_r + \frac{6}{\eta} A^{\frac{1}{2}} \right) \frac{\partial^2}{\partial \eta^2} \\ &\quad + \left( A^{-\frac{3}{2}} A_r^2 - 2A^{-\frac{1}{2}} A_{rr} - \frac{3}{\eta} A^{-\frac{1}{2}} A_r + \frac{2}{\eta^2} A^{\frac{1}{2}} \right) \frac{\partial}{\partial \eta} - \left( \frac{1}{\eta^2} A^{-\frac{1}{2}} A_r - \frac{2}{\eta^3} A^{\frac{1}{2}} \right) \frac{\partial^2}{\partial \theta^2} \\ &\quad + \left( \frac{-3}{8} A^{-\frac{5}{2}} A_r^3 + \frac{3}{4} A^{-\frac{3}{2}} A_r A_{rr} - \frac{1}{2} A^{-\frac{1}{2}} A_{rrr} + \frac{1}{2\eta^2} A^{-\frac{1}{2}} A_r \right. \\ &\quad \left. + \frac{1}{2\eta} A^{-\frac{3}{2}} A_r^2 - \frac{1}{\eta} A^{-\frac{1}{2}} A_{rr} - \frac{1}{\eta^3} A^{\frac{1}{2}} \right) \end{aligned}$$

$$G_4 \equiv K_4$$

再根据后面导出的关于  $C_n^{(b)}$  的初值条件可以解出  $C_n^{(b)}$ , 再代入 (1.18) 式就完全确定  $v_n^{(b)}$ 。这时方程 (1.19) 化为齐次方程:

$$\frac{\partial^4 v_{n+1}^{(b)}}{\partial \xi^4} - \frac{\partial^2 v_{n+1}^{(b)}}{\partial \xi^2} = 0$$

又可求得

$$v_{n+1}^{(b)} = C_{n+1}^{(b)}(\eta, \theta) \exp(-\xi) = C_{n+1}^{(b)}(r, \theta) \exp\left(-\varepsilon^{-1} \int_b^r \sqrt{A(t, \theta)} dt\right)$$

其中  $C_{n+1}^{(b)}$  是待定函数等等。建立了逐步求  $v_n^{(b)}$ , ( $n=0, 1, \dots$ ) 的递推过程。

可以应用同样的方法在外缘  $r=1$  的邻域构造边界层项。引进两变量  $\tilde{\xi}$  和  $\tilde{\eta}$ :

$$\tilde{\xi} = \frac{\tilde{u}(r, \theta)}{\varepsilon}, \quad \tilde{\eta} = r \quad (1.21)$$

式中

$$\tilde{u}(r, \theta) = \int_r^1 \sqrt{A(t, \theta)} dt \quad (1.22)$$

假设边界层项具有展开式:

$$V^{(b)} = \sum_{n=0}^{\infty} \varepsilon^{n+1} v_n^{(b)}(\tilde{\xi}, \tilde{\eta}, \theta) \quad (1.23)$$

代入方程(1.2'), 令  $\varepsilon^n$ , ( $n=0, 1, \dots$ ) 的系数为零, 得到同样形式的递推方程:

$$\tilde{K}_0[v_0^{(b)}] \equiv \tilde{u}_r^4 \frac{\partial^4 v_0^{(b)}}{\partial \tilde{\xi}^4} - A \tilde{u}_r^2 \frac{\partial^2 v_0^{(b)}}{\partial \tilde{\xi}^2} = 0 \quad (1.24)$$

$$\tilde{K}_0[v_n^{(b)}] = - \sum_{s=1}^4 \tilde{K}_s[v_{n-s}^{(b)}], \quad (n=0, 1, \dots) \quad (1.25)$$

式中  $\tilde{u}_r = -A^{\frac{1}{2}}$ ,  $\tilde{K}_s$ , ( $s=0, 1, 2, 3, 4$ ) 与  $K_s$  的表达式相同只是将  $\xi, \eta$  和  $u$  相应地换成  $\tilde{\xi}, \tilde{\eta}$  和  $\tilde{u}$ 。经过同样的运算知道

$$v_n^{(b)} = C_n^{(b)}(\tilde{\eta}, \theta) \exp(-\tilde{\xi}) = C_n^{(b)}(r, \theta) \exp\left(-\varepsilon^{-1} \int_r^1 \sqrt{A(t, \theta)} dt\right) \quad (1.26)$$

$$(n=0, 1, 2, \dots)$$

只是  $C_n^{(b)}$ , ( $n=0, 1, 2, \dots$ ) 确定于下面的一阶线性偏微分方程:

$$2A \frac{\partial C_0^{(b)}}{\partial \tilde{\eta}} - 2B \frac{\partial C_0^{(b)}}{\partial \theta} + \left(\frac{5}{2} A_r + \frac{2}{\tilde{\eta}} A - D\right) C_0^{(b)} = 0 \quad (1.27)$$

$$\begin{aligned}
& 2A \frac{\partial C_n^{(1)}}{\partial \tilde{\eta}} - 2B \frac{\partial C_n^{(1)}}{\partial \theta} + \left( \frac{5}{2} A_r + \frac{2}{\tilde{\eta}} A - D \right) C_n^{(1)} \\
& = -A^{-\frac{1}{2}} (\tilde{G}_2 [C_{n-1}^{(1)}] + \tilde{G}_3 [C_{n-2}^{(1)}] + \tilde{G}_4 [C_{n-3}^{(1)}]), \\
& (n=1, 2, \dots)
\end{aligned} \tag{1.28}$$

式中  $\tilde{G}_2$ ,  $\tilde{G}_3$  和  $\tilde{G}_4$  分别与  $G_2$ ,  $-G_3$  和  $G_4$  的表达式相同只是将  $\eta$  换成  $\tilde{\eta}$ .

假设边值问题(1.2)–(1.4)的解具有展开式:

$$\begin{aligned}
W(r, \theta; \varepsilon) &= \sum_{n=0}^N \varepsilon^n W_n(r, \theta) + \sum_{n=0}^N \varepsilon^{n+1} v_n^{(b)}(\xi, \eta, \theta) + \sum_{n=0}^N \varepsilon^{n+1} v_n^{(1)}(\tilde{\xi}, \tilde{\eta}, \theta) \\
&+ Z_N,
\end{aligned} \tag{1.29}$$

式中  $W_n$ ,  $v_n^{(b)}$  和  $v_n^{(1)}$  分别由递推方程(1.6)(1.7)(1.11)(1.12)(1.24)(1.25)确定.  $Z_N$  表示余项, 易知  $L_\varepsilon[Z_N] = O(\varepsilon^{N+1})$

下面再确定  $W_n$ ,  $v_n^{(b)}$  (或  $C_n^{(b)}$ ),  $v_n^{(1)}$  (或  $C_n^{(1)}$ ), ( $n=0, 1, \dots, N$ ) 的边界条件, 使余项  $Z_N$  在边界上成立:

$$Z_N \Big|_{r=b} = O(\varepsilon^{N+1}), \quad \frac{\partial Z_N}{\partial r} \Big|_{r=b} = O(\varepsilon^{N+1})$$

将(1.29)式代入边值条件(1.3)(1.4), 考虑到  $v_n^{(b)}$  ( $v_n^{(1)}$ ) ( $n=0, 1, \dots, N$ ) 在  $r=1$  ( $r=b$ ) 具有边界层项性质, 在边界  $r=b$  ( $r=1$ ) 上当  $\varepsilon \rightarrow 0$  时渐近于零, 得到关系式:

$$\sum_{n=0}^N \varepsilon^n W_n \Big|_{r=b} + \sum_{n=0}^N \varepsilon^{n+1} C_n^{(b)}(\eta, \theta) \exp(-\xi) \Big|_{\substack{\xi=0 \\ \eta=b}} + Z_N \Big|_{r=b} = f_0(\theta) \tag{1.30}$$

$$\begin{aligned}
& \sum_{n=0}^N \varepsilon^n \frac{\partial W_n}{\partial r} \Big|_{r=b} + \sum_{n=0}^N \varepsilon^{n+1} \left( \varepsilon^{-1} A^{\frac{1}{2}} \frac{\partial}{\partial \xi} + \frac{\partial}{\partial \eta} \right) C_n^{(b)}(\eta, \theta) \exp(-\xi) \Big|_{\substack{\xi=0 \\ \eta=b}} \\
& + \frac{\partial Z_N}{\partial r} \Big|_{r=b} = g_0(\theta)
\end{aligned} \tag{1.31}$$

$$\sum_{n=0}^N \varepsilon^n W_n \Big|_{r=1} + \sum_{n=0}^N \varepsilon^{n+1} C_n^{(1)}(\tilde{\eta}, \theta) \exp(-\tilde{\xi}) \Big|_{\substack{\tilde{\xi}=0 \\ \tilde{\eta}=1}} + Z_N \Big|_{r=1} = f_1(\theta), \tag{1.32}$$

$$\begin{aligned}
& \sum_{n=0}^N \varepsilon^n \frac{\partial W_n}{\partial r} \Big|_{r=1} + \sum_{n=0}^N \varepsilon^{n+1} \left( -\varepsilon^{-1} A^{\frac{1}{2}} \frac{\partial}{\partial \tilde{\xi}} + \frac{\partial}{\partial \tilde{\eta}} \right) \\
& \cdot C_n^{(1)}(\tilde{\eta}, \theta) \exp(-\tilde{\xi}) \Big|_{\substack{\tilde{\xi}=0 \\ \tilde{\eta}=1}} + \frac{\partial Z_N}{\partial r} \Big|_{r=1} = g_1(\theta)
\end{aligned} \tag{1.33}$$

令  $\varepsilon^n$  ( $n=0, 1, \dots, N$ ) 的系数为零, 则得到关于  $W_n$ ,  $C_n^{(b)}$ ,  $C_n^{(1)}$  ( $n=0, 1, \dots, N$ ) 的边值条件,

$$W_0|_{r=b} = f_0(\theta), \quad W_n|_{r=1} = f_1(\theta) \quad (1.34)$$

$$\left. \frac{\partial W_0}{\partial r} \right|_{r=b} - A^{\frac{1}{2}} C_0^{(b)} \Big|_{\eta=b} = g_0(\theta), \quad \left. \frac{\partial W_0}{\partial r} \right|_{r=1} + A^{\frac{1}{2}} C_0^{(1)} \Big|_{\eta=1} = g_1(\theta) \quad (1.35)$$

$$W_n|_{r=b} + C_{n-1}^{(b)} \Big|_{\eta=b} = 0, \quad W_n|_{r=1} + C_{n-1}^{(1)} \Big|_{\eta=1} = 0 \quad (1.36)$$

$$\left. \begin{aligned} \frac{\partial W_n}{\partial r} \Big|_{r=b} + \left( -A^{\frac{1}{2}} C_n^{(b)} + \frac{\partial C_{n-1}^{(b)}}{\partial \eta} \right) \Big|_{\eta=b} &= 0, \\ \frac{\partial W_n}{\partial r} \Big|_{r=1} + \left( A^{\frac{1}{2}} C_n^{(1)} + \frac{\partial C_{n-1}^{(1)}}{\partial \eta} \right) \Big|_{\eta=1} &= 0 \end{aligned} \right\} \quad (1.37)$$

$$(n=1, 2, \dots, N)$$

根据递推方程和边值条件(1.30)–(1.33)可以逐步地求出展开式(1.29)中的  $W_n, v_n^{(b)}, v_n^{(1)}$ , ( $n=0, 1, \dots, N$ ).

首先看出, 展开式(1.29)中的首项  $W_0$  应是退化边值问题 (二阶椭圆型方程的狄立克雷问题):

$$\begin{aligned} F[W_0] \equiv & A(r, \theta) \frac{\partial^2 W_0}{\partial r^2} + 2B(r, \theta) \frac{\partial^2 W_0}{\partial r \partial \theta} + C(r, \theta) \frac{\partial^2 W_0}{\partial \theta^2} \\ & + D(r, \theta) \frac{\partial W_0}{\partial r} + E(r, \theta) \frac{\partial W_0}{\partial \theta} = -q \end{aligned} \quad (1.38)$$

$$W_0|_{r=b} = f_0(\theta), \quad W_0|_{r=1} = f_1(\theta) \quad (1.39)$$

的解, 即薄膜理论的解。求得  $W_0$  后, 从关于  $C_0^{(b)}$  的一阶线性偏微分方程(1.17)和(1.35)式左侧的边界条件:

$$C_0^{(b)}(\eta, \theta) \Big|_{\eta=b} = -A^{\frac{-1}{2}}(b, \theta) \left( g_0(\theta) - \frac{\partial W_0(b, \theta)}{\partial r} \right) \quad (1.40)$$

可以确定出  $C_0^{(b)}$ , 再代入(1.15)式就求得  $v_0^{(b)}$ ; 从关于  $C_0^{(1)}$  的方程(1.27)和(1.35)式右侧的边界条件:

$$C_0^{(1)}(\eta, \theta) \Big|_{\eta=1} = A^{\frac{-1}{2}}(1, \theta) \left( g_1(\theta) - \frac{\partial W_0(1, \theta)}{\partial r} \right) \quad (1.41)$$

可以确定出  $C_0^{(1)}$ , 再代入(1.26) (取  $n=0$ ) 就求得  $v_0^{(1)}$ . 求得  $W_0, v_0^{(b)}$  和  $v_0^{(1)}$  后, 再代入(1.7)、(1.36) (取  $n=1$ ) 又得到关于  $W_1$  的边值问题:

$$F[W_1] = 0 \quad (1.42)$$

$$W_1 \Big|_{r=b} = -C_0^{(b)}(b, \theta), \quad W_1 \Big|_{r=1} = -C_0^{(1)}(1, \theta) \quad (1.43)$$

求得  $W_1$  后, 从关于  $C_1^{(b)}$  的方程 (1.20) (取  $n=1$ ) 和 (1.37) 式 (取  $n=1$ ) 左侧的边界条件可以确定出  $C_1^{(b)}$ , 再代入 (1.18) 式就求得  $v_1^{(b)}$ , 从关于  $C_1^{(1)}$  的方程 (1.28) (取  $n=1$ ) 和 (1.37) 式 (取  $n=1$ ) 右侧的边界条件可以确定出  $C_1^{(1)}$ , 再代入(1.26) 式 (取  $n=1$ ) 就求得  $v_1^{(1)}$ . 这样继续下去可以逐步地求得  $W_n, v_n^{(b)}, v_n^{(1)}$ , ( $n=0, 1, \dots, N$ ), 最后确定出  $W(r, \theta; \varepsilon)$ .

对于余项  $Z_N$  成立

$$L_\varepsilon[Z_N] = O(\varepsilon^{N+1}), \quad Z_N \Big|_{r=b} = O(\varepsilon^{N+1}), \quad \frac{\partial Z_N}{\partial r} \Big|_{r=b} = O(\varepsilon^{N+1})$$

根据 [9] 或 [10] 的结果知

$$[Z_N]_j = O(\varepsilon^{N+1-j}), \quad (j=0, 1, \dots, N)$$

$$\text{式中 } [Z_N]_j \equiv S_{\mu\rho} |D^j Z_N|, \quad |D^j Z_N| = \sum_{\rho=0}^j \left| \frac{\partial^\rho Z_N}{\partial r^{j-\rho} \partial \theta^\rho} \right|$$

例 1: 设一半径为  $r_1$  的圆形板, 在板的中心含有一半径为  $r_0$  的刚性物, 又在板的中面上作用有均匀的径向和环向的拉力:  $N_r = N_\theta = N$  (常数),  $N_{r\theta} = 0$ , 当板所含的刚性物绕直径转过小的转角  $\alpha$  时, 试求板的挠度。(1968年, W.E. Alzheimer 和 R.T. Davis 曾应用匹配方法求得了一阶近似式。参看 [6] 或 [11])。

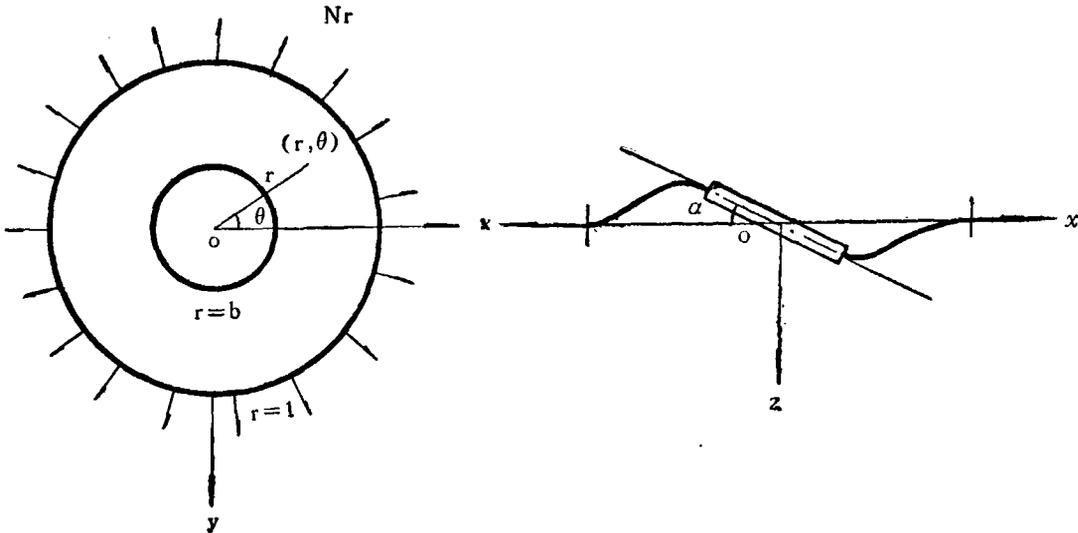


图 1 变形前板的俯视图

图 2 板的变形图

写出板的 (无量纲) 挠度方程和边界条件:

$$\varepsilon^2 \Delta \Delta W - \Delta W = 0 \tag{1.44}$$

$$W \Big|_{r=b} = b \alpha \cos \theta, \quad \frac{\partial W}{\partial r} \Big|_{r=b} = \alpha \cos \theta \tag{1.45}$$

$$W \Big|_{r=1} = 0, \quad \frac{\partial W}{\partial r} \Big|_{r=1} = 0 \tag{1.46}$$

为了与 [6] 的结果比较, 这里采用了新的小参数  $\varepsilon^2 = \frac{h^3}{12(1-\nu^2)r_1^3 n} = \frac{D}{r_1^2 N}$  式中

$n = \frac{N}{r_1 E}$ . 这时  $A=1, B=0, C=\frac{1}{r^2}, D=\frac{1}{r}, E=0$  展开式 (1.29) 中的首项  $W_0$  确定于下面的退化边值问题:

$$\frac{\partial^2 W_0}{\partial r^2} + \frac{1}{r} \frac{\partial W_0}{\partial r} + \frac{1}{r^2} \frac{\partial^2 W_0}{\partial \theta^2} = 0$$

$$W_0|_{r=b} = b\alpha \cos \theta, \quad W_0|_{r=1} = 0$$

假设  $W_0 = u(r) \cos \theta$  代入上式, 得到关于  $u(r)$  边值问题:

$$\frac{d^2 u}{dr^2} + \frac{1}{r} \frac{du}{dr} - \frac{1}{r^2} u = 0, \quad u(b) = b\alpha, \quad u(1) = 0$$

解得  $u(r) = \frac{b^2 \alpha}{1-b^2} \left( \frac{1}{r} - r \right)$ , 所以

$$W_0 = \frac{b^2 \alpha}{1-b^2} \left( \frac{1}{r} - r \right) \cos \theta$$

又关于  $C_0^{(b)}$  的方程 (1.17) 和边界条件 (1.40) 具有形式:

$$2 \frac{\partial C_0^{(b)}}{\partial \eta} + \frac{1}{\eta} C_0^{(b)} = 0, \quad C_0^{(b)}(\eta, \theta) \Big|_{\eta=b} = -\frac{2\alpha}{1-b^2} \cos \theta$$

解得  $C_0^{(b)} = \frac{-2\alpha \sqrt{b}}{1-b^2 \sqrt{\eta}} \cos \theta$ , 所以

$$v_0^{(b)} = \left[ \frac{-2\alpha \sqrt{b}}{1-b^2 \sqrt{r}} \exp\left(-\frac{r-b}{\varepsilon}\right) \right] \cos \theta$$

关于  $C_0^{(1)}$  的方程 (1.27) 和边界条件 (1.41) 具有形式:

$$2 \frac{\partial C_0^{(1)}}{\partial \tilde{\eta}} + \frac{1}{\tilde{\eta}} C_0^{(1)} = 0, \quad C_0^{(1)}(\tilde{\eta}, \theta) \Big|_{\tilde{\eta}=1} = \frac{2b^2 \alpha}{1-b^2} \cos \theta$$

解得  $C_0^{(1)} = \frac{2b^2 \alpha}{1-b^2} \frac{1}{\sqrt{\tilde{\eta}}} \cos \theta$ , 所以

$$v_0^{(1)} = \left[ \frac{2b^2 \alpha}{1-b^2} \frac{1}{\sqrt{r}} \exp\left(-\frac{1-r}{\varepsilon}\right) \right] \cos \theta$$

又关于  $W_1$  的边值问题 (1.42)–(1.43) 具有形式:

$$\frac{\partial^2 W_1}{\partial r^2} + \frac{1}{r} \frac{\partial W_1}{\partial r} + \frac{1}{r^2} \frac{\partial^2 W_1}{\partial \theta^2} = 0$$

$$W_1 \Big|_{r=b} = \frac{2\alpha}{1-b^2} \cos \theta, \quad W_1 \Big|_{r=1} = -\frac{2b^2 \alpha}{1-b^2} \cos \theta$$

假设  $W_1 = u_1(r) \cos \theta$ , 代入上式, 得到  $u_1$  的边值问题

$$\frac{d^2 u_1}{dr^2} + \frac{1}{r} \frac{du_1}{dr} - \frac{1}{r^2} u_1 = 0, \quad u_1(b) = \frac{2\alpha}{1-b^2}, \quad u_1(1) = -\frac{2b^2 \alpha}{1-b^2}$$

解得  $u_1 = \frac{2ab}{(1-b^2)^2} \left[ \frac{1+b^3}{r} - (1+b)r \right]$ , 所以

$$W_1 = \frac{2ab}{(1-b^2)^2} \left[ \frac{1+b^3}{r} - (1+b)r \right] \cos \theta$$

将  $W_0, v_0^{(b)}, v_0^{(1)}$ , 和  $W_1$  代入 (1.29) 式, 得到挠度函数的一阶渐近近似式:

$$W(r, \theta, \varepsilon) = \left\{ \frac{b^2 \alpha}{1-b^2} \left( \frac{1}{r} - r \right) + \varepsilon \frac{2ab}{(1-b^2)^2} \left[ \frac{1+b^3}{r} - (1+b)r \right] + \varepsilon \frac{-2\alpha}{1-b^2} \frac{\sqrt{b}}{\sqrt{r}} e^{-\frac{r-b}{\varepsilon}} \right. \\ \left. + \varepsilon \frac{2b^2 \alpha}{1-b^2} \frac{1}{\sqrt{r}} e^{-\frac{1-r}{\varepsilon}} \right\} \cos \theta + O(\varepsilon^2)$$

与 [6] 或 [11] 应用匹配法求得的结果相同, 只是边界层项相差一高阶无穷小量。

例 2: 仍考察上面的例子, 只是假设  $N_r = N_\theta = N(r)$ , 和  $N_{r\theta} = 0$ 。将挠度方程 (1.44) 改写成

$$\varepsilon^2 \Delta \Delta W - n(r) \Delta W = 0$$

式中  $\varepsilon^2 = \frac{h^3}{12(1-\nu^2)r_1^3}$ ,  $n(r) = \frac{N(r)}{r_1 E}$ 。与方程 (1.2') 比较,  $A = n(r)$ ,  $B = 0$ ,

$C = \frac{n(r)}{r^2}$ ,  $D = \frac{n(r)}{r}$ ,  $E = 0$ , 同例 1 一样地可以求得

$$W_0 = \frac{b^2 \alpha}{1-b^2} \left( \frac{1}{r} - r \right) \cos \theta$$

$C_0^{(b)}$  确定于下面的方程和边界条件:

$$2n(\eta) \frac{\partial C_0^{(b)}}{\partial \eta} + \left( \frac{5}{2} n'(\eta) + \frac{n(\eta)}{\eta} \right) C_0^{(b)} = 0,$$

$$C_0^{(b)} \Big|_{\eta=b} = -n^{\frac{-1}{2}}(b) \frac{2\alpha}{1-b^2} \cos \theta$$

解得  $C_0^{(b)} = \frac{-2\alpha}{1-b^2} n^{\frac{3}{2}}(b) \frac{\sqrt{b}}{\sqrt{\eta}} n^{\frac{-5}{4}}(\eta) \cos \theta$ , 所以

$$v_0^{(b)} = \left[ \frac{-2\alpha}{1-b^2} n^{\frac{3}{2}}(b) \frac{\sqrt{b}}{\sqrt{r}} n^{\frac{-5}{4}}(r) \exp\left(-\varepsilon^{-1} \int_b^r \sqrt{n(t)} dt\right) \right] \cos \theta$$

又  $C_0^{(1)}$  确定于方程和边界条件:

$$2n(\tilde{\eta}) \frac{\partial C_0^{(1)}}{\partial \tilde{\eta}} + \left( \frac{5}{2} n'(\tilde{\eta}) + \frac{n(\tilde{\eta})}{\tilde{\eta}} \right) C_0^{(1)} = 0,$$

$$C_0^{(1)} \Big|_{\tilde{\eta}=1} = \frac{2b^2 \alpha}{1-b^2} n^{\frac{-1}{2}}(1) \cos \theta$$

解得  $C_0^{(1)} = \frac{2b^2 \alpha}{1-b^2} n^{\frac{3}{2}}(1) \frac{1}{\sqrt{\tilde{\eta}}} n^{\frac{-5}{4}}(\tilde{\eta}) \cos \theta$ , 所以

$$v_0^{(1)} = \left[ \frac{2b^2 \alpha}{1-b^2} n^{\frac{3}{2}}(1) \frac{1}{\sqrt{r}} n^{\frac{-5}{4}}(r) \exp\left(-\varepsilon^{-1} \int_1^r \sqrt{n(t)} dt\right) \right] \cos \theta$$

这时  $W_1$  确定于边值问题:

$$\frac{\partial^2 W_1}{\partial r^2} + \frac{1}{r} \frac{\partial W_1}{\partial r} + \frac{1}{r^2} \frac{\partial^2 W_1}{\partial \theta^2} = 0$$

$$W_1 \Big|_{r=b} = \frac{2a}{1-b^2} n^{-\frac{1}{2}}(b) \cos \theta, \quad W_1 \Big|_{r=1} = \frac{-2b^2 a}{1-b^2} n^{-\frac{1}{2}}(1) \cos \theta$$

解得

$$W_1 = \frac{2ba}{(1-b^2)^2} \left\{ \left[ n^{-\frac{1}{2}}(b) + b^3 n^{-\frac{1}{2}}(1) \right] \frac{1}{r} - \left[ n^{-\frac{1}{2}}(b) + b n^{-\frac{1}{2}}(1) \right] r \right\} \cos \theta$$

所以

$$\begin{aligned} W(r, \theta; \varepsilon) = & \left\{ \frac{b^2 a}{1-b^2} \left( \frac{1}{r} - r \right) + \varepsilon \frac{2ba}{(1-b^2)^2} \right. \\ & \cdot \left[ \left( n^{-\frac{1}{2}}(b) + b^3 n^{-\frac{1}{2}}(1) \right) \frac{1}{r} - \left( n^{-\frac{1}{2}}(b) + b n^{-\frac{1}{2}}(1) \right) r \right] \\ & + \varepsilon \frac{-2a}{1-b^2} n^{\frac{3}{4}}(b) \frac{\sqrt{b}}{\sqrt{r}} n^{-\frac{5}{4}}(r) \exp\left(-\varepsilon^{-1} \int_b^r \sqrt{n(t)} dt\right) \\ & + \varepsilon \frac{2b^2 a}{1-b^2} n^{\frac{3}{4}}(1) \frac{1}{\sqrt{r}} n^{-\frac{5}{4}}(r) \exp\left(-\varepsilon^{-1} \int_r^1 \sqrt{n(t)} dt\right) \left. \right\} \\ & \cdot \cos \theta + O(\varepsilon^2) \end{aligned}$$

从上式可以看出板的挠度随着 $n(r)$ 的增大而减小, 当 $n(r) \rightarrow \infty$ 时, 趋于薄膜理论的解。

[注1]: 若 $W_0, W_1, \dots$ 不能显式地解出, 则可以应用近似方法(例如 Галеркин 方法)或数值方法(例如差分方法)求出它们的近似解, 再完成上面的运算。

[注2]: 若在边界例如 $r=1$ 上, 不是给出第一类边界条件而是给出其它类型的边界条件, 例如

$$W|_{r=1} = f_1(\theta), \quad \left[ \frac{\partial^2 W}{\partial r^2} + \nu \left( \frac{1}{r} \frac{\partial W}{\partial r} + \frac{1}{r^2} \frac{\partial^2 W}{\partial \theta^2} \right) \right] \Big|_{r=1} = g_1(\theta) \quad (1.47)$$

这时应将挠度函数的展开式假设成

$$W(r, \theta; \varepsilon) = \sum_{n=0}^N \varepsilon^n W_n(r, \theta) + \sum_{n=0}^N \varepsilon^{n+1} v_n^{(b)}(\xi, \eta, \theta) + \sum_{n=0}^N \varepsilon^{n+2} v_n^{(1)}(\tilde{\xi}, \tilde{\eta}, \theta) \quad (1.48)$$

代入边界条件(1.47), 代替关系式(1.32)、(1.33)有

$$\begin{aligned} & \sum_{n=0}^N \varepsilon^n W_n|_{r=1} + \sum_{n=0}^N \varepsilon^{n+2} C_n^{(1)}(\tilde{\eta}, \theta) \exp(-\tilde{\xi}) \Big|_{\substack{\tilde{\xi}=0 \\ \tilde{\eta}=1}} + Z_N|_{r=1} = f_1(\theta) \\ & \sum_{n=0}^N \varepsilon^n \left[ \frac{\partial^2 W_n}{\partial r^2} + \nu \left( \frac{1}{r} \frac{\partial W_n}{\partial r} + \frac{1}{r^2} \frac{\partial^2 W_n}{\partial \theta^2} \right) \right] \Big|_{r=1} + \sum_{n=0}^N \varepsilon^{n+2} \left[ \varepsilon^{-2} A \frac{\partial}{\partial \tilde{\xi}} \right. \end{aligned}$$

$$\begin{aligned}
 & + \varepsilon^{-1} \left( -2 A^{\frac{1}{2}} \frac{\partial^2}{\partial \tilde{\xi} \partial \tilde{\eta}} - \frac{1}{2} A^{-\frac{1}{2}} A_r \frac{\partial}{\partial \tilde{\xi}} \right) + \frac{\partial^2}{\partial \tilde{\eta}^2} \Big] \\
 & \cdot C_n^{(1)}(\tilde{\eta}, \theta) \exp(-\tilde{\xi}) \Big|_{\tilde{\xi}=\tilde{\eta}} + \nu \sum_{n=0}^N \varepsilon^{n+2} \left( -\varepsilon^{-1} A^{\frac{1}{2}} \frac{\partial}{\partial \tilde{\xi}} + \frac{\partial}{\partial \tilde{\eta}} \right) \\
 & \cdot C_n^{(1)}(\tilde{\eta}, \theta) \exp(-\tilde{\xi}) \Big|_{\tilde{\xi}=\tilde{\eta}} + \nu \sum_{n=0}^N \varepsilon^{n+2} \frac{\partial^2}{\partial \theta^2} C_n^{(1)}(\tilde{\eta}, \theta) \\
 & \exp(-\tilde{\xi}) \Big|_{\tilde{\xi}=\tilde{\eta}} + \left[ \frac{\partial^2 Z_N}{\partial r^2} + \nu \left( \frac{1}{r} \frac{\partial Z_N}{\partial r} + \frac{1}{r^2} \frac{\partial^2 Z_N}{\partial \theta^2} \right) \right] \Big|_{r=1} \\
 & = g_1(\theta)
 \end{aligned}$$

令  $\varepsilon^n$ , ( $n=0, 1, \dots, N$ ) 的系数为零, 代替(1.34)–(1.37)式右侧的边界条件有

$$\begin{aligned}
 & W_0 \Big|_{r=1} = f_1(\theta) \\
 & \left[ \frac{\partial^2 W_0}{\partial r^2} + \nu \left( \frac{1}{r} \frac{\partial W_0}{\partial r} + \frac{1}{r^2} \frac{\partial^2 W_0}{\partial \theta^2} \right) \right] \Big|_{r=1} + A C_0^{(1)} \Big|_{\tilde{\eta}=1} = g_1(\theta) \\
 & W_n \Big|_{r=1} + C_{n-2}^{(1)} \Big|_{\tilde{\eta}=1} = 0 \\
 & \left[ \frac{\partial^2 W_n}{\partial r^2} + \nu \left( \frac{1}{r} \frac{\partial W_n}{\partial r} + \frac{1}{r^2} \frac{\partial^2 W_n}{\partial \theta^2} \right) \right] \Big|_{r=1} - A C_n^{(1)} \Big|_{\tilde{\eta}=1} \\
 & + \left[ 2 A^{\frac{1}{2}} \frac{\partial C_{n-1}^{(1)}}{\partial \tilde{\eta}} + \frac{1}{2} A^{-\frac{1}{2}} A_r C_{n-1}^{(1)} + \frac{\partial^2 C_{n-2}^{(1)}}{\partial \tilde{\eta}^2} \right. \\
 & \left. + \nu \left( A^{\frac{1}{2}} C_{n-1}^{(1)} + \frac{\partial C_{n-2}^{(1)}}{\partial \tilde{\eta}} + \frac{\partial^2 C_{n-2}^{(1)}}{\partial \theta^2} \right) \right] \Big|_{\tilde{\eta}=0} = 0 \\
 & (n=1, 2, \dots, N)
 \end{aligned}$$

其它运算相同。

## 二、圆形薄板

上面所提出的摄动方法, 也适用于圆形薄板和其它一切具有光滑边界的薄板。考察下面的例子:

例 3: 设一半径为  $r_1$  的圆板, 除作用有依赖于  $r$  的侧向载荷外(以  $q(r)$  表示载荷强度)还在中面内作用有依赖于  $r$  的径向力和环向力:  $N_r = N_\theta = N(r)$ ,  $N_{r\theta} = 0$  试分别求板在夹支和筒支条件下的挠度。

先考察夹支的情形。由于对称性, 板的(无量纲)挠度方程和边界条件具有形式

$$\varepsilon^2 \left( \frac{d^4 W}{dr^4} + \frac{2}{r} \frac{d^3 W}{dr^3} - \frac{1}{r^2} \frac{d^2 W}{dr^2} + \frac{1}{r^3} \frac{dW}{dr} \right) - n(r) \left( \frac{d^2 W}{dr^2} + \frac{1}{r} \frac{dW}{dr} \right) = q(r) \quad (2.1)$$

$$W \Big|_{r=1} = 0, \quad \frac{dW}{dr} \Big|_{r=1} = 0; \quad \text{在 } r=0, \quad W \text{ 和 } \frac{dW}{dr} \text{ 是有界.} \quad (2.2)$$

式中  $\varepsilon^2 = \frac{h^3}{12(1-\nu^2)r_1^3}$ . 将方程 (2.1) 与方程 (1.2) 相比较,  $A=n(r)$ ,  $B=0$ ,  $D = \frac{n(r)}{r}$  和所有对  $\theta$  的导数项为零. 代替 (1.29) 式应假设

$$W(r, \theta; \varepsilon) = \sum_{n=0}^N \varepsilon^n W_n(r, \theta) + \sum_{n=0}^N \varepsilon^{n+1} v_n(\xi, \eta, \theta) + Z_N \quad (2.3)$$

式中  $\xi = \varepsilon^{-1} \int_0^1 \sqrt{n(t)} dt$ ,  $\eta = r$ . 这时  $W_0$  确定于下面形式的退化边值问题:

$$\frac{d^2 W_0}{dr^2} + \frac{1}{r} \frac{dW_0}{dr} = \frac{-q(r)}{n(r)}$$

$W_0 \Big|_{r=1} = 0$ , 在  $r=0$ ,  $W_0$  是有界,

解得

$$W_0 = k_1 \ln r + \int_1^r t^{-1} \int_1^t \frac{-q(s)}{n(s)} s ds dt \quad (2.4)$$

式中  $k_1$  是任意常数, 根据  $W_0$  在  $r=0$  是有界的条件确定. 在均匀载荷和均匀中面力:  $q(r) = q$ ,  $n(r) = n$ , ( $q$  和  $n$  是常数) 的情形下, 有

$$W_0 = k_1 \ln r - \frac{qr^2}{4n} + \frac{q}{2n} \ln r + \frac{q}{4n} \quad (2.5)$$

取  $k_1 = \frac{-q}{2n}$ , 得  $W_0 = -\frac{qr^2}{4n} + \frac{q}{4n}$

又关于  $C_0^{(1)}$  的方程 (1.27) 和边界条件 (1.41) 具有形式:

$$2n(\eta) \frac{dC_0^{(1)}}{d\eta} + \left( \frac{5}{2} n'(\eta) + \frac{n(\eta)}{\eta} \right) C_0^{(1)} = 0, \quad C_0^{(1)} \Big|_{\eta=1} = \frac{-k_1}{\sqrt{n(1)}} \quad (2.6)$$

解得  $C_0^{(1)} = \frac{-k_1 n^{\frac{3}{2}}(1)}{\sqrt{\eta}} n^{-\frac{5}{4}}(\eta)$ , 所以边界层项  $v_0^{(1)}$  为

$$v_0^{(1)} = \frac{-k_1 n^{\frac{3}{2}}(1)}{\sqrt{r}} n^{-\frac{5}{4}}(r) \exp\left(-\varepsilon^{-1} \int_0^1 \sqrt{n(t)} dt\right)$$

为了消除它在边界层以外区域的影响, 再引进截断函数:

$$\psi(r) = \begin{cases} 1, & \text{当 } \frac{2}{3} \leq r \leq 1 \\ 0, & \text{当 } 0 \leq r \leq \frac{1}{3} \end{cases}$$

$$\tilde{v}_0^{(1)} = \psi(r) v_0^{(1)},$$

又关于  $W_1$  的边值问题 (1.42)–(1.43) 具有形式:

$$\frac{d^2 W_1}{dr^2} + \frac{1}{r} \frac{dW_1}{dr} = 0 \quad (2.7)$$

$$W_1|_{r=1} = k_1 n^{-\frac{1}{2}}(1), \text{ 在 } r=0, W_1 \text{ 是有界,} \quad (2.8)$$

解得  $W_1 = k_1 n^{-\frac{1}{2}}(1)$ . 所以挠度函数的一阶渐近近似式是

$$\begin{aligned} W(r, \theta; \varepsilon) = & W_0 + \varepsilon W_1 + \varepsilon \tilde{v}_0^{(1)} = k_1 \ln r + \int_r^1 t^{-1} \int_t^1 \frac{-q(s)}{n(s)} s ds dt + \varepsilon k_1 n^{-\frac{1}{2}}(1) \\ & + \varepsilon \psi(r) \frac{-k_1 n^{\frac{3}{2}}(1)}{\sqrt{r}} n^{-\frac{5}{4}}(r) \exp\left(-\varepsilon^{-1} \int_r^1 \sqrt{n(t)} dt\right) + O(\varepsilon^2) \end{aligned} \quad (2.9)$$

在均匀侧向载荷和均匀中面力的情形

$$W(r, \theta; \varepsilon) = \frac{(1-r^2)q}{4n} - \varepsilon \frac{q}{2n^{3/2}} + \varepsilon \psi(r) \frac{q}{2n^{3/2}} \frac{1}{\sqrt{r}} \exp\left(\frac{-\sqrt{n}(1-r)}{\varepsilon}\right) + O(\varepsilon^2) \quad (2.10)$$

在参考文献 [7] 的 94 节中考虑了均匀载荷和均匀中面力的情形, 它们的主要项是一致的.

对于边界简支的圆形板, 代替边界条件 (2.2) 有

$$W|_{r=1} = 0, \quad \left(\frac{d^2 W}{dr^2} + \frac{\nu}{r} \frac{dW}{dr}\right)\Big|_{r=1} = 0 \quad (2.11)$$

代替展开式 (2.3) 有

$$W(r, \theta; \varepsilon) = \sum_{n=0}^N \varepsilon^n W_n(r, \theta) + \sum_{n=0}^N \varepsilon^{n+2} v_n(\xi, \eta, \theta) + Z_N$$

式中  $W_0$  仍由 (2.4) 式给出,  $C_0^{(1)}$  仍确定于 (2.6) 中的一阶线性微分方程, 只是边界条件换成

$$C_0^{(1)}\Big|_{\eta=1} = -A^{-1} \left(\frac{d^2 W_0}{dr^2} + \frac{\nu}{r} \frac{dW_0}{dr}\right)\Big|_{r=1} = -\frac{(1-\nu)k_1}{n(1)} + \frac{q(1)}{n^2(1)}$$

解得  $C_0^{(1)} = \left[\frac{(1-\nu)k_1}{n(1)} + \frac{q(1)}{n^2(1)}\right] n^{\frac{5}{4}}(1) \frac{1}{\sqrt{\eta}} n^{-\frac{5}{4}}(\eta)$ , 所以

$$v_0 = \left[\frac{(1-\nu)k_1}{n(1)} + \frac{q(1)}{n^2(1)}\right] n^{\frac{5}{4}}(1) \frac{1}{\sqrt{r}} n^{-\frac{5}{4}}(r) \exp\left(-\varepsilon^{-1} \int_r^1 \sqrt{n(t)} dt\right)$$

令  $\tilde{v}_0 = \psi(r) v_0$ . 又  $W_1$  仍确定于方程 (2.7), 只是边界条件换成

$$W_1|_{r=1} = 0, \text{ 在 } r=0 \text{ 是有界}$$

解得

$$W_1 = 0$$

所以挠度函数的一阶近似式为

$$\begin{aligned} W(r, \theta; \varepsilon) &= W_0 + \varepsilon W_1 + \varepsilon \tilde{v}_0 + O(\varepsilon^2) \\ &= k_1 \ln r + \int_0^1 t^{-1} \int_0^1 \frac{-q(s)}{n(s)} s ds dt + \varepsilon \psi(r) \left[ -\frac{(1-\nu)k_1}{n(1)} + \frac{q(1)}{n^2(1)} \right] n^{\frac{5}{4}}(1) \\ &\quad + \frac{1}{\sqrt{r}} n^{-\frac{5}{4}}(r) \exp\left(-\varepsilon^{-1} \int_0^1 \sqrt{n(t)} dt\right) + O(\varepsilon^2) \end{aligned} \quad (2.12)$$

对于  $q(r)=q$ ,  $n(r)=n$ ,  $q$  和  $n$  是常数的情形,  $k_1 = \frac{-q}{2n}$  所以

$$W(r, \theta; \varepsilon) = -\frac{q(1-r^2)}{4n} + \varepsilon \psi(r) \frac{(1+\nu)q}{2n^2} \frac{1}{\sqrt{r}} \exp\left(-\frac{\sqrt{n}(1-r)}{\varepsilon}\right) + O(\varepsilon^2) \quad (2.13)$$

比较 (2.10) 式和 (2.13) 式可以看出, 在板的内部区域, 夹支板的挠度比简支板的挠度减小的量为  $\varepsilon \frac{q}{2n^{3/2}} = \frac{h^3 q}{24(1-\nu^2)r_1^3 n^{3/2}}$  准确到  $\varepsilon^2$  量级。

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## Some Applications of Perturbation Method in Thin Plate Bending Problems

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### Abstract

In this paper, problems of bending of thin plates under the combined action of lateral loading and in-plane forces are studied by means of perturbation method.