

矩形薄板弹性弯曲问题的一般解析解法*

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摘 要

本文对求解矩形薄板弹性弯曲问题采用先建立微分方程的一般解, 然后根据问题的边界条件确定积分常数, 这样求解比采用迭加法求解要简单容易。

一、基本方程的解

如图1所示, 矩形薄板弹性弯曲的基本方程为^[1]

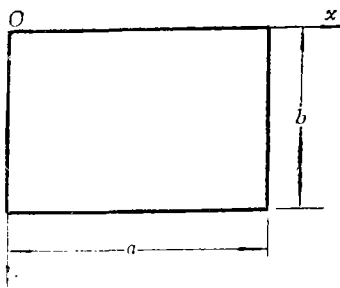


图 1

$$\frac{\partial^4 w}{\partial x^4} + 2 \frac{\partial^4 w}{\partial x^2 \partial y^2} + \frac{\partial^4 w}{\partial y^4} = \frac{q}{D} \quad (1.1)$$

当四边为简支时可取双正弦级数解

$$w = \sum_m \sum_n A_{mn} \sin \alpha x \sin \beta y \quad (1.2)$$

式中

$$A_{mn} = \frac{4 \int_0^a \int_0^b q \sin \alpha x \sin \beta y dx dy}{D ab (\alpha^2 + \beta^2)^2} \quad (1.3)$$

$$\alpha = \frac{m\pi}{a} \quad (m=1, 2, \dots, \infty) \quad (1.4)$$

$$\beta = \frac{n\pi}{b} \quad (n=1, 2, \dots, \infty) \quad (1.5)$$

当两对边为简支时可得单正弦级数解

$$w = \sum_m (A_m \cosh \alpha y + B_m \sinh \alpha y + C_m \alpha y \sinh \alpha y + D_m \alpha y \cosh \alpha y) \sin \alpha x \quad (1.6)$$

等式(1.1)也可取其他形式的解: 余弦级数, 多项式或其他函数。对于各种不同边界条件的问题, 虽然可以采用迭加法^[2,3], 但求解过程十分复杂。

本文建议先建立方程(1.1)的一般解, 然后根据边界条件确定积分常数, 并取为

$$w = \sum_m [A_m \sinh \alpha (b-y) + B_m \sinh \alpha y + C_m \alpha y \cosh \alpha (b-y) + D_m \alpha y \cosh \alpha y] \sin \alpha x / \sinh \alpha b \\ + \sum_n [E_n \sinh \beta (a-x) + F_n \sinh \beta x + G_n \beta x \cosh \beta (a-x) + H_n \beta x \cosh \beta x] \sin \beta y / \sinh \beta a$$

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$$\begin{aligned}
 &+ a_{00} + a_{10} \frac{x}{a} + a_{01} \frac{y}{b} + a_{11} \frac{xy}{ab} + a_{20} \frac{x^2}{a^2} + a_{02} \frac{y^2}{b^2} \\
 &+ a_{21} \frac{x^2 y}{a^2 b} + a_{12} \frac{xy^2}{ab^2} + a_{30} \frac{x^3}{a^3} + a_{03} \frac{y^3}{b^3} + a_{31} \frac{x^3 y}{a^3 b} + a_{13} \frac{xy^3}{ab^3} + w_0
 \end{aligned} \quad (1.7)$$

w_0 为等式(1.1)的任一特解, 本文取等式(1.2)。

将等式(1.6)和等式(1.7)的第一部分比较有两点不同, 一是在等式(1.7)中多了一除数 $\sinh ab$, 这可使积分常数的系数均变化在 $[-1, +1]$ 中而不致变成很大的数; 二是改用 $\sinh \alpha(b-y)$ 来代替 $\cosh \alpha y$ 避免了 αy 很大时积分常数 A_m 和 B_m 接近相同。

等式(1.7)的第一部分可满足 $y=0$ 和 $y=b$ 两个边为任意边界条件, 第二部分可满足 $x=0$ 和 $x=a$ 两个边为任意边界条件。此外必须补充一多项式来满足角点的边界条件, 其中前四项可满足四个角点的挠度条件, 后八项可满足四个角点每两边的弯矩条件。采用等式(1.2)作特解虽然收敛差, 但可通过数学演算来改善收敛速度。

二、边界条件

等式(1.7)共有 $4m+4n+12$ 个积分常数, 这可由边界条件来确定。其中每个边有二个边界条件: 即挠度或等效剪力, 斜度或弯矩均应分别等于边界的已知值。在每个边界条件所建立的方程式中将非正弦函数均展成正弦级数, 根据正交性可得到 $4m+4n$ 个方程式。另外每个角有三个角点条件: 即挠度或反力, 角的两边的斜度或弯矩应分别等于相应的已知值, 故又有 4×3 个方程式。因此可以求解全部积分常数。等式(1.7)中的函数可展成如下的正弦级数

$$1 = \sum_m \frac{2(1 - \cos m\pi)}{m\pi} \sin \alpha x \quad (2.1)$$

$$\frac{x}{a} = - \sum_m \frac{2 \cos m\pi}{m\pi} \sin \alpha x \quad (2.2)$$

$$\frac{x^2}{a^2} = - \sum_m \left[\frac{2 \cos m\pi}{m\pi} + \frac{4(1 - \cos m\pi)}{(m\pi)^3} \right] \sin \alpha x \quad (2.3)$$

$$\frac{x^3}{a^3} = - \sum_m \left[\frac{2 \cos m\pi}{m\pi} - \frac{12 \cos m\pi}{(m\pi)^3} \right] \sin \alpha x \quad (2.4)$$

$$\frac{\sinh \beta(a-x)}{\sinh \beta a} = \sum_m \frac{2\alpha}{a(\alpha^2 + \beta^2)} \sin \alpha x \quad (2.5)$$

$$\frac{\sinh \beta x}{\sinh \beta a} = - \sum_m \frac{2\alpha \cos m\pi}{a(\alpha^2 + \beta^2)} \sin \alpha x \quad (2.6)$$

$$\beta x \frac{\cosh \beta(a-x)}{\sinh \beta a} = \sum_m \left(\frac{2\beta^2}{\alpha^2 + \beta^2} - \frac{\beta \alpha \cos m\pi}{\sinh \beta a} \right) \frac{2\alpha}{a(\alpha^2 + \beta^2)} \sin \alpha x \quad (2.7)$$

$$\beta x \frac{\cosh \beta x}{\sinh \beta a} = \sum_m \left(\frac{2\beta^2}{\alpha^2 + \beta^2} - \beta \alpha \coth \beta a \right) \frac{2\alpha \cos m\pi}{a(\alpha^2 + \beta^2)} \sin \alpha x \quad (2.8)$$

三、例

以两相邻边固定两相邻边自由的矩形板为例, 如图2所示。边界条件和角点条件是

$$(w)_{x=0} = 0 \quad (3.1)$$

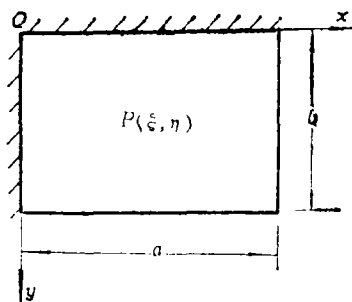


图 2

$$\left(\frac{\partial w}{\partial x}\right)_{x=0} = 0 \quad (3.2)$$

$$(M_x)_{x=a} = -D \left(\frac{\partial^2 w}{\partial x^2} + \nu \frac{\partial^2 w}{\partial y^2}\right)_{x=a} = 0 \quad (3.3)$$

$$(V_x)_{x=a} = -D \left[\frac{\partial^3 w}{\partial x^3} + (2-\nu) \frac{\partial^3 w}{\partial x \partial y^2}\right]_{x=a} = 0 \quad (3.4)$$

$$(w)_{y=0} = 0 \quad (3.5)$$

$$\left(\frac{\partial w}{\partial y}\right)_{y=0} = 0 \quad (3.6)$$

$$(M_y)_{y=b} = -D \left(\frac{\partial^2 w}{\partial y^2} + \nu \frac{\partial^2 w}{\partial x^2}\right)_{y=b} = 0 \quad (3.7)$$

$$(V_y)_{y=b} = -D \left[\frac{\partial^3 w}{\partial y^3} + (2-\nu) \frac{\partial^3 w}{\partial x^2 \partial y}\right]_{y=b} = 0 \quad (3.8)$$

$$w_{(0,0)} = 0 \quad (3.9)$$

$$\left(\frac{\partial w}{\partial x}\right)_{(0,0)} = 0 \quad (3.10)$$

$$\left(\frac{\partial w}{\partial y}\right)_{(0,0)} = 0 \quad (3.11)$$

$$w_{(a,0)} = 0 \quad (3.12)$$

$$\left(\frac{\partial w}{\partial y}\right)_{(a,0)} = 0 \quad (3.13)$$

$$M_{x(a,0)} = -D \left(\frac{\partial^2 w}{\partial x^2} + \nu \frac{\partial^2 w}{\partial y^2}\right)_{(a,0)} = 0 \quad (3.14)$$

$$w_{(0,b)} = 0 \quad (3.15)$$

$$\left(\frac{\partial w}{\partial x}\right)_{(0,b)} = 0 \quad (3.16)$$

$$M_{y(0,b)} = -D \left(\frac{\partial^2 w}{\partial y^2} + \nu \frac{\partial^2 w}{\partial x^2}\right)_{(0,b)} = 0 \quad (3.17)$$

$$R_{(a,b)} = 2D(1-\nu) \left(\frac{\partial^2 w}{\partial x \partial y}\right)_{(a,b)} = 0 \quad (3.18)$$

$$M_{x(a,b)} = -D \left(\frac{\partial^2 w}{\partial x^2} + \nu \frac{\partial^2 w}{\partial y^2}\right)_{(a,b)} = 0 \quad (3.19)$$

$$M_{y(a,b)} = -D \left(\frac{\partial^2 w}{\partial y^2} + \nu \frac{\partial^2 w}{\partial x^2}\right)_{(a,b)} = 0 \quad (3.20)$$

将等式(1.2)代入等式(1.1)然后代入以上各式并应用到等式(2.1)~(2.8)。首先由等式(3.9), (3.12)和(3.15)可得

$$a_{00} = 0, \quad a_{10} = -a_{20} - a_{30}, \quad a_{01} = -a_{02} - a_{03} \quad (3.21)$$

应用上式则由等式(3.5)和(3.10)可得

$$A_m - a_{20} \frac{4(1 - \cos m\pi)}{(m\pi)^3} + a_{30} \frac{12 \cos m\pi}{(m\pi)^3} = 0 \quad (3.22)$$

$$\sum_m A_m m\pi - a_{20} - a_{30} = 0 \quad (3.23)$$

将 x 和 x^2 展成余弦级数可以求得

$$\sum_m \frac{1}{(m\pi)^2} = \frac{1}{6}, \quad \sum_m \frac{\cos m\pi}{(m\pi)^2} = -\frac{1}{12} \quad (3.24)$$

将等式(3.22)乘以 $m\pi$ 然后进行求和,并应用到以上二式即可得到等式(3.23)。故等式(3.10)并不是独立的角点条件,这是由于沿 x 轴 $w=0$,必然有 $\partial w/\partial x=0$,这可用 $(\partial^2 w/\partial x^2)_{(0,0)}=0$ 的条件来代替,由此可得

$$a_{20}=0$$

同样用 $(\partial^2 w/\partial y^2)_{(0,0)}=0$ 来代替等式(3.11)可得

$$a_{02}=0$$

由等式(3.14), (3.17), (3.19)和(3.20)可得

$$a_{30} = -a_{12} \frac{\nu}{3} \frac{a^2}{b^2}, \quad a_{03} = -a_{21} \frac{\nu}{3} \frac{b^2}{a^2}, \quad a_{31} = a_{12} \frac{\nu}{3} \frac{a^2}{b^2} - \frac{a_{21}}{3}, \quad a_{13} = a_{21} \frac{\nu}{3} \frac{b^2}{a^2} - \frac{a_{12}}{3}$$

将以上各等式代入等式(3.21)和(3.22)可得

$$a_{10} = a_{12} \frac{\nu}{3} \frac{a^2}{b^2}, \quad a_{01} = a_{21} \frac{\nu}{3} \frac{b^2}{a^2}$$

$$A_m = a_{12} \frac{4\nu \cos m\pi}{(m\pi)^3} \frac{a^2}{b^2}$$

同样由等式(3.1)得

$$E_n = a_{21} \frac{4\nu \cos n\pi}{(n\pi)^3} \frac{b^2}{a^2}$$

应用以上各式则由等式(3.3)和(3.7)得

$$F_n = -G_n \frac{\beta a}{\sinh \beta a} - H_n \left(\beta a \coth \beta a + \frac{2}{1-\nu} \right)$$

$$B_m = -C_m \frac{ab}{\sinh ab} - D_m \left(ab \coth ab + \frac{2}{1-\nu} \right)$$

由等式(3.13)和(3.16)得

$$a_{12} = a_{21} + \frac{3}{1-\nu} \sum_n (D_n - H_n) n\pi \quad (3.25)$$

$$a_{11} = \frac{2}{1-\nu} \sum_m D_m m\pi - a_{21} \frac{\nu}{3} \frac{b^2}{a^2} - a_{12} \left(\frac{2}{3} + \frac{\nu}{3} \frac{a^2}{b^2} \right)$$

由等式(3.2), (3.4), (3.6), (3.8)和(3.18),并应用到以下二式

$$\sum_m \frac{1}{\alpha^2 + \beta^2} = \frac{a}{2\beta} \left(\coth \beta a - \frac{1}{\beta a} \right)$$

$$\sum_m \frac{\cos m\pi}{\beta^2(\alpha^2 + \beta^2)} = \frac{a}{2\beta^3} \left(\frac{1}{\beta a} - \frac{1}{\sinh \beta a} - \frac{\beta a}{6} \right)$$

(将 $\sinh \beta x$ 和 $\cosh \beta x$ 展成余弦级数,并应用到等式(3.24)可以求得以上二式),最后可得

$$\begin{aligned} & \sum_m \left[C_m \beta - D_m \frac{(\alpha^2 + \nu\beta^2) \cos n\pi}{(1-\nu)\beta} \right] \frac{4\alpha^3}{b(\alpha^2 + \beta^2)^2} \\ & + \left[G_n \left(\coth \beta a - \frac{\beta a}{\sinh^2 \beta a} \right) - \frac{H_n}{\sinh \beta a} \left(\beta a \coth \beta a + \frac{1+\nu}{1-\nu} \right) \right] \beta \end{aligned}$$

$$-\left[\frac{a_{12}}{(n\pi)^2}\left(\frac{1-\nu}{\beta a} + \frac{\nu}{\sinh\beta a}\right) + a_{21}\frac{\nu\cos n\pi}{\beta^2 a^2}\left(\coth\beta a - \frac{1}{\beta a}\right)\right]\frac{4}{b} + \sum_m A_{mn}\alpha = 0 \quad (3.26)$$

$$\begin{aligned} & \sum_m \{C_m[\alpha^2 + (2-\nu)\beta^2] + D_m(1-\nu)\beta^2\cos m\pi\} \frac{4\alpha^3\beta\cos m\pi}{b(\alpha^2 + \beta^2)^2} \\ & - \left\{ \frac{G_n}{\sinh\beta a} [(1-\nu)\beta a\coth\beta a + 1 + \nu] + H_n [(3+\nu)\coth\beta a \right. \\ & \left. + (1-\nu)\frac{\beta a}{\sinh^2\beta a}] \right\} \beta^3 - \left[\frac{a_{12}}{b^2} \left(\nu\coth\beta a + \frac{2-\nu}{\beta a} \right) + a_{21}\frac{\cos n\pi}{a^2} \left(\frac{1-\nu}{\beta a} \right. \right. \\ & \left. \left. + \frac{\nu}{\sinh\beta a} \right) \right] \frac{4(1-\nu)}{b} + \sum_m A_{mn}\alpha[\alpha^2 + (2-\nu)\beta^2]\cos m\pi = 0 \end{aligned} \quad (3.27)$$

$$\begin{aligned} & \sum_n \left[G_n\alpha - H_n \frac{(\nu\alpha^2 + \beta^2)\cos m\pi}{(1-\nu)\alpha} \right] \frac{4\beta^3}{a(\alpha^2 + \beta^2)^2} + \left[C_m \left(\coth ab - \frac{ab}{\sinh^2 ab} \right) \right. \\ & \left. - \frac{D_m}{\sinh ab} \left(ab\coth ab + \frac{1+\nu}{1-\nu} \right) \right] \alpha - \left[\frac{a_{21}}{(m\pi)^2} \left(\frac{1-\nu}{ab} + \frac{\nu}{\sinh ab} \right) \right. \\ & \left. + a_{12}\frac{\nu\cos m\pi}{a^2 b^2} \left(\coth ab - \frac{1}{ab} \right) \right] \frac{4}{a} + \sum_n A_{mn}\beta = 0 \end{aligned} \quad (3.28)$$

$$\begin{aligned} & \sum_n \{G_n[\beta^2 + (2-\nu)\alpha^2] + H_n(1-\nu)\alpha^2\cos m\pi\} \frac{4\alpha\beta^3\cos m\pi}{a(\alpha^2 + \beta^2)^2} \\ & - \left\{ \frac{C_m}{\sinh ab} [(1-\nu)ab\coth ab + 1 + \nu] + D_n \left[(3+\nu)\coth ab + (1-\nu)\frac{ab}{\sinh^2 ab} \right] \right\} \alpha^3 \\ & - \left[\frac{a_{21}}{a^2} \left(\nu\coth ab + \frac{2-\nu}{ab} \right) + a_{12}\frac{\cos m\pi}{b^2} \left(\frac{1-\nu}{ab} + \frac{\nu}{\sinh ab} \right) \right] \frac{4(1-\nu)}{a} \\ & + \sum_n A_{mn}[(2-\nu)\alpha^2 + \beta^2]\beta\cos m\pi = 0 \end{aligned} \quad (3.29)$$

$$\begin{aligned} & \sum_m C_m(ab\coth ab - 1) \frac{\alpha^2\cos m\pi}{\sinh ab} + \sum_n D_n \alpha \left[\left(\frac{1+\nu}{1-\nu}\coth ab + \frac{ab}{\sinh^2 ab} \right) \alpha\cos m\pi \right. \\ & \left. - \frac{1}{b(1-\nu)} \right] + \sum_n G_n(\beta a\coth\beta a - 1) \frac{\beta^2\cos n\pi}{\sinh\beta a} + \sum_n H_n \beta \left[\left(\frac{1+\nu}{1-\nu}\coth\beta a + \right. \right. \\ & \left. \left. + \frac{\beta a}{\sinh^2\beta a} \right) \beta\cos n\pi - \frac{1}{a(1-\nu)} \right] + \frac{a_{12}}{ab} \left[\sum_n \frac{4\nu}{ab\sinh ab} - \frac{2}{3} \left(1 + \nu\frac{a^2}{b^2} \right) \right] \\ & + \frac{a_{21}}{ab} \left[\sum_n \frac{4\nu}{\beta a\sinh\beta a} - \frac{2}{3} \left(1 + \nu\frac{b^2}{a^2} \right) \right] - \sum_m \sum_n A_{mn}\alpha\beta\cos m\pi\cos n\pi = 0 \end{aligned} \quad (3.30)$$

由等式(3.25)~(3.30)可解得 C_m , D_m , G_n , H_n , a_{21} 和 a_{12} 。

四、集中载荷

当板上有一集中载荷 P 作用在 $x=\xi$, $y=\eta$, 由等式(1.3)得

$$A_{mn} = \frac{4P \sin \alpha \xi \sin \beta \eta}{Dab(\alpha^2 + \beta^2)^2}$$

将上式代入等式(3.26)~(3.30)得

$$\sum_m A_{mn} \alpha = \frac{4P \sin \beta \eta}{Dab} \sum_m \frac{\alpha \sin \alpha \xi}{(\alpha^2 + \beta^2)^2} \quad (4.1)$$

$$\sum_n A_{mn} \beta = \frac{4P \sin \alpha \xi}{Dab} \sum_n \frac{\beta \sin \beta \eta}{(\alpha^2 + \beta^2)^2} \quad (4.2)$$

$$\begin{aligned} \sum_m A_{mn} \alpha [\alpha^2 + (2-\nu)\beta^2] \cos m\pi \\ = \frac{4P \sin \beta \eta}{Dab} \sum_m \frac{\alpha \sin \alpha \xi}{(\alpha^2 + \beta^2)^2} [\alpha^2 + (2-\nu)\beta^2] \cos m\pi \end{aligned} \quad (4.3)$$

$$\begin{aligned} \sum_n A_{mn} \beta [(2-\nu)\alpha^2 + \beta^2] \cos n\pi \\ = \frac{4P \sin \alpha \xi}{Dab} \sum_n \frac{\beta \sin \beta \eta}{(\alpha^2 + \beta^2)^2} [(2-\nu)\alpha^2 + \beta^2] \cos n\pi \end{aligned} \quad (4.4)$$

$$\begin{aligned} \sum_m \sum_n A_{mn} \alpha \beta \cos m\pi \cos n\pi \\ = \sum_n \frac{4P \beta \sin \beta \eta}{Dab} \cos n\pi \sum_m \frac{\alpha \sin \alpha \xi}{(\alpha^2 + \beta^2)^2} \cos m\pi \end{aligned} \quad (4.5)$$

由等式(2.5)~(2.8)可得

$$\begin{aligned} \sum_m \frac{\alpha \sin \alpha x}{(\alpha^2 + \beta^2)^2} &= \frac{a}{4\beta^2} \left[\beta x \frac{\cosh \beta(a-x)}{\sinh \beta a} - \beta a \frac{\sinh \beta x}{\sinh^2 \beta a} \right] \\ \sum_m \frac{\alpha \sin \alpha x}{(\alpha^2 + \beta^2)^2} \cos m\pi &= \frac{a}{4\beta^2} \left(\beta x \frac{\cosh \beta x}{\sinh \beta a} - \beta a \coth \beta a \frac{\sinh \beta x}{\sinh \beta a} \right) \\ \sum_m \frac{\alpha^3 \sin \alpha x}{(\alpha^2 + \beta^2)^2} \cos m\pi &= \frac{a}{4} \left[(\beta a \coth \beta a - 2) \frac{\sinh \beta x}{\sinh \beta a} - \beta x \frac{\cosh \beta x}{\sinh \beta a} \right] \end{aligned}$$

令 $x = \xi$ 代入以上各式然后代入等式(4.1)~(4.5)得

$$\sum_m A_{mn} \alpha = \frac{P \sin \beta \eta \sinh \beta \xi}{Dn\pi \sinh \beta a} \left[\xi \frac{\cosh \beta(a-\xi)}{\sinh \beta \xi} - \frac{a}{\sinh \beta a} \right] \quad (4.6)$$

$$\sum_n A_{mn} \beta = \frac{P \sin \alpha \xi \sinh \alpha \eta}{Dm\pi \sinh \alpha b} \left[\eta \frac{\cosh \alpha(b-\eta)}{\sinh \alpha \eta} - \frac{b}{\sinh \alpha b} \right] \quad (4.7)$$

$$\begin{aligned} \sum_m A_{mn} \alpha [\alpha^2 + (2-\nu)\beta^2] \cos m\pi \\ = \frac{P \sin \beta \eta \sinh \beta \xi}{Dbsinh \beta a} [(1-\nu)(\beta \xi \coth \beta \xi - \beta a \coth \beta a) - 2] \end{aligned} \quad (4.8)$$

$$\begin{aligned} \sum_n A_{mn} \beta [(2-\nu)\alpha^2 + \beta^2] \cos n\pi \\ = \frac{P \sin \alpha \xi \sinh \alpha \eta}{Dasinh \alpha b} [(1-\nu)(\alpha \eta \coth \alpha \eta - \alpha b \coth \alpha b) - 2] \end{aligned} \quad (4.9)$$

$$\begin{aligned} \sum_m \sum_n A_{mn} \alpha \beta \cos m\pi \cos n\pi \\ = \sum_n \frac{P \sin \beta \eta \sinh \beta \xi}{Dbsinh \beta a} (\xi \coth \beta \xi - a \coth \beta a) \cos n\pi \end{aligned} \quad (4.10)$$

由等式(1.1)可得自由角点的挠度和固定边的弯矩为

$$w_{(a,b)} = \sum_m D_m \frac{2m\pi}{1-\nu} + a_{21} \frac{2}{3}$$

$$(M_y)_{y=0} = \left(\sum_m C_m \alpha^2 \sin \alpha x - a_{21} \frac{1-\nu}{b^2} \frac{x}{a} \right) 2D$$

为简单计，取矩形板 $a=b$ ，且集中载荷作用在 $(0,0)$ 和 (a,b) 的联线上，将有 $\xi=\eta$ ， $G_n=C_n$ ， $H_n=D_n$ ， $a_{12}=a_{21}$ 。根据等式(3.26)，(3.27)和(3.30)，取 $\nu=0.3$ ， ξ/a 分别等于 0.25, 0.5, 0.75, m 和 n 由1取至8和16时 $w_{(a,b)}$ 的结果 见表1。

表1 自由角点的挠度 (单位为 $10^{-6}Pa^2/D$)

m, n	ξ/a	0.25		0.5		0.75	
		8	608	1828	24854	33147	92441
16		1171	1750	27538	31534	106138	124083

表1中第一个数值是由等式(4.1)，(4.3)和(4.5)求得的，第二个数值是由等式(4.6)，(4.8)和(4.10)求得的。可以看出第一个数值由小变大而第二个数值由大变小并逐渐接近精确值，但第二个数值收敛性较好。

仅采用等式(4.6)，(4.8)和(4.10)， m 和 n 由1取至16, 23, 24, 25时的结果见表2。

表2 自由角点的挠度

m, n	ξ/a	0.25		0.5		0.75	
		16	1750		31574		124083
23		1603		29478		118080	
24		1697		30382		120090	
25		1611		29639		118553	

可以看出， m 和 n 取至偶数时是由大变小，取至奇数时是由小变大，并逐渐接近精确值。

采用等式(4.6)，(4.8)和(4.10)， m 和 n 由1取至24和25，取其平均值可得自由角点的挠度和沿固定边的弯矩，见表3。其中 $\xi/a=1$ 为集中力作用在自由角点，如令 $A_{mn}=0$ ，且在等式(2.18)中令 $R_{(a,b)}=P$ 时的结果。最后一列为文献[2]当 m 和 n 由1取至50的结果。

表3 挠度 (Pa^2/D)和弯矩(P)

ξ/a	0.25	0.50	0.75	1	1[2]
$w_{(a,b)}$	0.00165	0.03901	0.11932	0.29649	0.29787
$M_{y_{\max}}(x,0)$	-0.1888	-0.2496	-0.7707	-1.3825	-1.3131
$x/a(M_{y_{\max}})$	0.29	0.87	0.96	0.96	0.975
$M_{y(a,0)}$	0.0031	-0.0779	-0.3627	-0.7049	0

本文的一般解法和常用的迭加法原则上是相同的。文献[2]没有引用等式(1.7)中代数多项式的后八项，因而导致角点 $(a,0)$ 的弯矩 $M_y=0$ ，故未能满足角点条件 $(\partial w / \partial y)_{(a,0)}=0$ 。文献[3]虽然引用了全部代数多项式，但在满足角点条件 $(\partial w / \partial y)_{(a,0)}=0$ 的同时，取 $M_{x(a,0)}=1.1M_{y(a,0)}$ ，因而未能满足 $M_{x(a,0)}=0$ 的要求。

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A General Solution of Rectangular Thin Plates in Bending

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Abstract

In this paper a general solution of rectangular plates in bending is given. The integral constants are determined by means of boundary conditions. This method is simpler and easier than the method of superposition.