

感应磁场对竖直对称管道中 Johnson-Segman 流体蠕动流的影响*

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摘要: 研究了热传导和感应磁场, 对 Johnson-Segman 流体蠕动流的影响. 目的是研究感应磁场对非 Newton 流体蠕动流的影响. 在长波和低 Reynolds 数假设下, 被简化为一组二维的 Johnson-Segman 流体的流动方程. 采用常规的摄动方法, 求得流函数、磁力函数和轴向压力梯度的解. 对不同的参数, 绘出了压力增量、温度、感应磁场、压力梯度和流函数表达式的简图并给出解释.

关键词: 感应磁场; 竖直的对称管道; Johnson-Segman 流体; 磁流体动力学 (MHD)

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引 言

不同种类流体蠕动流的研究有着特殊的地位, 因而有着广阔的应用, 例如尿液从肾脏通过输尿管到膀胱的输运、食糜在胃肠脏器中的输运、某些保暖物的移动, 等. 在 Laham^[1] 最早的研究之后, 已有不少研究, 将蠕动流看作 Newton 流体和非 Newton 流体加以研究^[2-5].

磁流体动力学 (MHD) 对蠕动流问题的影响, 已应用于生理流体学, 例如血液的流动、血泵机, 以及关于蠕动磁流体动力学压缩机操作的理论研究. Nadeem 和 Akbar^[6] 就传热和传质的环状通路中, 径向变化的磁流体动力学对蠕动流的影响进行了研究. Srinivas 和 Kothandapani^[7] 就磁流体动力学蠕动流沿壁面流过多孔空间时, 调查了传热传质的影响. Mekheimer 和 Elhahond^[8] 对竖直的环状通道, 在零 Reynolds 数和长波的近似下, 讨论了传热和磁场对 Newton 流体蠕动流的影响. Ebaid^[9] 在圆柱形管道内, 用 Adomian 分解法, 就粘度可变生物流体的磁流体动力学蠕动流, 进行了新数值解的研究. Mekheimer^[10] 在一个狭长管道内, 研究了感应磁场对耦合应力流体蠕动流的影响. Srivastava 和 Agrawal^[11] 研究了磁流体动力学对血液流动的影响. 该课题更新的研究, 见文献 [12-17].

本文的主要目的是, 研究感应磁场对竖直管道中 Johnson-Segman 流体蠕动流的影响. 本文安排如下: 第 1 节介绍数学公式; 第 2 节就小 Weissenberg 数时, 构建流函数、磁力函数和轴

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向压力梯度的解;第 3 节通过图形分析了该问题的物理特点.

1 数学公式

在一均匀宽度为 n 的二维竖直管道内,考虑不可压缩、导电 Johnson-Segelman 流体的蠕流. 由于我们考虑的管道是均匀的,管壁上保持温度为 T_0 . 由于管道中心对称,温度的变化趋于为 0. 外部横向作用的均匀磁场强度为常数 H_0 . 感应磁场为 $\mathbf{H}(h_x(X, Y, t), H_0 + h_y(X, Y, t), 0)$, 则考虑的总磁场强度为 $\mathbf{H}^+(h_x(X, Y, t), H_0 + h_y(X, Y, t), 0)$. 考虑到管道是绝缘的,壁面的几何变形定义为

$$h(X, t) = n + b \sin\left[\frac{2\pi}{\lambda}(X - ct)\right], \quad (1)$$

其中 b 为波幅, λ 为波长, n 为管道宽度, c 为传播速度, t 为时间, X 为波传播方向. 如下给出 Johnson-Segelman 流体磁流体动力学流动的控制方程组:

Maxwell 方程^[10]

$$\tilde{\nabla} \cdot \mathbf{H} = 0, \quad \tilde{\nabla} \cdot \mathbf{E} = 0, \quad (2)$$

$$\tilde{\nabla} \times \mathbf{H} = \mathbf{J}, \quad \mathbf{J} = \sigma_1(\mathbf{E} + \mathbf{v} \times \mathbf{H}), \quad (3)$$

$$\tilde{\nabla} \times \mathbf{E} = -\epsilon \frac{\mathbf{H}}{t}, \quad (4)$$

其中 \mathbf{E} 为感应电场强度, \mathbf{J} 为电流密度, ϵ 为磁导率, σ_1 为电导率;

连续性方程为

$$\tilde{\nabla} \cdot \mathbf{V} = 0, \quad (5)$$

运动方程为

$$\left[\frac{\mathbf{V}}{t} + (\mathbf{V} \cdot \tilde{\nabla}) \mathbf{V} \right] = \text{div} \left[-\tilde{\nabla} \left(\frac{1}{2} \epsilon (\mathbf{H}^+)^2 \right) - \epsilon (\mathbf{H}^+ \cdot \tilde{\nabla}) \mathbf{H}^+ + \rho g(T - T_0) \right], \quad (6)$$

这里, Johnson-Segelman 流体^[10]的 Cauchy 应力张量与流体运动的关系为

$$\mathbf{T} = -PI + \mathbf{T}, \quad (7)$$

其中, $-PI$ 为球面应力, 由于约束的不可压缩性,

$$\mathbf{T} = 2\mathbf{D} + \mathbf{S}, \quad (8)$$

$$\mathbf{S} + m \left[\frac{d\mathbf{S}}{dt} + \mathbf{S}(\mathbf{W} - a\mathbf{D}) + (\mathbf{W} - a\mathbf{D})^T \mathbf{S} \right] = 2\mathbf{D}, \quad (9)$$

这里, \mathbf{V} 为速度, η 和 μ 为粘度, m 为松弛时间, a 为滑移参数, \mathbf{D} 和 \mathbf{W} 分别为速度梯度的对称部分和反对称部分:

$$\mathbf{D} = \frac{1}{2}(\mathbf{L} + \mathbf{L}^T), \quad (10)$$

$$\mathbf{W} = \frac{1}{2}(\mathbf{L} - \mathbf{L}^T), \quad (11)$$

式中 $\mathbf{L} = \text{grad}\mathbf{V}$.

没有耗散项时,能量方程定义为

$$c_p \left[\frac{T}{t} + U \frac{T}{X} + V \frac{T}{Y} \right] = k \left[\frac{\partial^2 T}{\partial X^2} + \frac{\partial^2 T}{\partial Y^2} \right] + Q_0, \quad (12)$$

其中 ρ 为密度, k 为导热系数, Q_0 为常数, 即热量吸收参数, c_p 为比定压热容.

联立方程 (2) ~ (4), 导得方程^[10]如下:

$$\frac{\mathbf{H}^+}{t} = \tilde{N} (\mathbf{V} \cdot \mathbf{H}^+) + \frac{1}{\tilde{N}} \tilde{N}^2 \mathbf{H}^+, \quad (13)$$

其中 $\tilde{N} = 1/(\nu_e)$ 为磁扩散系数.

引入波动坐标系 (x, y) , 以速度 c 远离固定坐标系 (X, Y) , 动坐标系和固定坐标系之间的变换为

$$x = X - ct, \quad y = Y, \quad u = U - c, \quad v = V.$$

定义

$$\left\{ \begin{aligned} x &= \frac{x}{n}, \quad y = \frac{y}{n}, \quad u = \frac{u}{c}, \quad v = \frac{v}{c}, \quad \tau = \frac{t}{cn}, \quad p = \frac{n^2 p}{c}, \quad t = \frac{ct}{n}, \quad h = \frac{h}{n}, \quad Re = \frac{cn}{\nu_e}, \\ &= \frac{1}{cn}, \quad \tau = \frac{t}{cn}, \quad P = P + \frac{1}{2} Re \frac{e(\mathbf{H}^+)^2}{c^2}, \quad Rm = \frac{cn}{\nu_e}, \quad S_1 = \frac{H_0}{c} \sqrt{\frac{e}{\nu_e}}, \\ &= \frac{T - T_0}{T_0}, \quad E_c = \frac{c^2}{CT_0}, \quad Pr = \frac{\nu_e C}{K}, \quad S = \frac{Sn}{c} = \frac{Q_0 n^2}{kT_0}, \quad Gr = \frac{g n^3 T_0}{2}. \end{aligned} \right. \quad (14)$$

利用上述无量纲量, 以流函数 $\psi(x, y)$ 和磁力函数 $\phi(x, y)$ 表示的磁流体动力学控制方程 (去掉上标横线, 并利用 $u = \psi_y / y, v = -\psi_x / x, h_x = \phi_y / y, h_y = -\phi_x / x$) 为

$$Re (\psi_{yy} - x \psi_{xy}) = -\frac{P}{x} \left(\frac{\psi}{x} \right) + \frac{1}{x} (S_{xx}) + \frac{1}{y} (S_{yy}) - Re S_1^2 \psi_{yy} - Re S_1^2 (\psi_{yy} - x \psi_{xy}) + Gr, \quad (15)$$

$$Re^3 (\psi_{xx} - y \psi_{xy}) = -\frac{P}{y} \left(\frac{\psi}{y} \right) + \frac{1}{x} (S_{xx}) + \frac{1}{y} (S_{yy}) + Re^2 S_1^2 \psi_{yy} - Re S_1^2 (\psi_{xx} - y \psi_{xy}), \quad (16)$$

$$\psi_y - (\psi_x - x \psi_y) + \frac{1}{Rm} (\psi_{yy} + \psi_{xx}) = E, \quad (17)$$

$$Re Pr \left(u \frac{\psi}{x} + v \frac{\psi}{y} \right) = \frac{1}{x^2} \frac{\psi^2}{x^2} + \frac{1}{y^2} \frac{\psi^2}{y^2}, \quad (18)$$

其中 W_e 为热源参数,

$$\left\{ \begin{aligned} S_{xx} &= W_e (1 + a) - \left(\frac{\psi}{y} \right)^2, \\ S_{yy} &= -W_e (1 - a) - \left(\frac{\psi}{x} \right)^2, \\ S_{xy} &= \frac{(\psi_x / x) (\psi_y / y)}{1 + W_e^2 (1 - a^2) (\psi_x^2 / x^2 + \psi_y^2 / y^2)} \end{aligned} \right. \quad (19)$$

相应的边界条件为

$$\psi = 0, \quad \frac{\psi}{y^2} = 0, \quad \psi = 0, \quad y = 0 \quad (20a)$$

$$\psi = F, \quad \frac{\psi}{y} = -1, \quad \psi = h = 1 + \sin(2x); \quad (20b)$$

$$\frac{\psi}{y} = 0, \quad \psi = 0, \quad \psi = 0, \quad y = h; \quad (20c)$$

$$\frac{\psi}{y} = 0, \quad \psi = 0, \quad \psi = 0, \quad y = h. \quad (20d)$$

在长波的假定下, 1 以及低 Reynolds 数时, 略去 1 项以及高于 1 阶的项, 方程 (15) 至 (19) 取如下形式:

$$\left(\frac{\partial}{\partial x} + \frac{\partial}{\partial y} \right) \frac{P}{x} = \frac{S_{xy}}{y} + \frac{3}{x^3} + Re S_1^2 \frac{\partial^2}{\partial y^2} + Gr, \quad (21)$$

$$-\frac{P}{y} = 0 \quad (22)$$

$$\frac{\partial^2}{\partial y^2} = Rm \left(E - \frac{\partial}{\partial y} \right), \quad (23)$$

$$\frac{\partial^2}{\partial y^2} + \frac{\partial}{\partial y} = 0. \quad (24)$$

由方程 (21) 和 (22) 消去压力, 可得

$$\frac{\partial^2}{\partial y^2} \left[\left[\left(\frac{\partial}{\partial x} + \frac{\partial}{\partial y} \right) \frac{\partial^2}{\partial y^2} + W_e^2 (1 - a^2) \left(\frac{\partial^2}{\partial y^2} \right)^2 \right] \left[\left[1 + W_e^2 (1 - a^2) \left(\frac{\partial^2}{\partial y^2} \right)^2 \right] \right] + Re^2 \frac{\partial^2}{\partial y^2} + Gr \frac{\partial}{\partial y} = 0 \quad (25)$$

$$\frac{\partial^2}{\partial y^2} = Rm \left(E - \frac{\partial}{\partial y} \right). \quad (26)$$

借助方程 (26), 方程 (25) 变为

$$\frac{\partial^2}{\partial y^2} \left[\frac{\partial^2}{\partial y^2} + \frac{W_e^2 (1 - a^2)}{\partial y^2} \left(\frac{\partial^2}{\partial y^2} \right)^2 \right] + M_1^2 \frac{\partial}{\partial y} \left(E - \frac{\partial}{\partial y} \right) + \frac{\partial}{\partial y} Gr = C_1, \quad (27)$$

其中 C_1 为常数, $M_1^2 = Rm R e S_b^2$, $M^2 = M_1^2 / (\partial + \partial)$.

2 摄动解

由温度方程 (24) 及边界条件 (20c), 有

$$= -\frac{1}{2}(y^2 - h^2). \quad (28)$$

为了得到解方程 (28), 我们使用常规的摄动方法, 以 W_e^2 为摄动参数. 对小 Weissenberg 数, 流函数、磁力函数和轴向压力梯度的解可写为

$$\begin{aligned} &= a_5 \sinh(My) + a_3 y^3 + a_4 y - \frac{a_6}{M^2} y + W_e^2 \left[a_{24} \cosh(My) + a_{25} \sinh(My) + \right. \\ & a_{15} y^3 \sinh(My) + a_{16} y^2 \sinh(My) + a_{17} y \sinh(My) + \\ & a_{18} \sinh(My) + a_{19} \sinh(3My) + a_{20} y \cosh(2My) + \\ & \left. a_{21} \cosh(2My) + a_{22} y^3 + a_{23} y - \frac{1}{M^2} (a_{26} y + a_{27}) \right], \quad (29) \end{aligned}$$

$$\begin{aligned} &= a_{28} \cosh(My) + a_{29} y^4 + a_{30} y^2 + a_{31} + W_e^2 (a_{32} y^3 \cosh(My) + \\ & a_{33} y^2 \cosh(My) + a_{34} y^2 \sinh(My) + a_{35} y \cosh(My) + a_{36} y \sinh(My) + \\ & a_{37} \cosh(My) + a_{38} \sinh(My) + a_{39} \cosh(3My) + a_{40} \cosh(2My) + \\ & a_{41} \sinh(2My) + a_{42} y \sinh(2My) + a_{43} y^4 + a_{44} y^2 + a_{46} y + a_{47}), \quad (30) \end{aligned}$$

$$\begin{aligned} \frac{dP}{dx} &= M^2 \left[1 + a_4 + 3a_3 h^2 + \frac{(F + h + 2a_3 h^3) M \cosh(Mh)}{\sinh(Mh) - Mh \cosh(Mh)} \right] + \\ & W_e^2 \left[M^2 (-3a_{17} + 2a_{16} h + 3a_{16} h^2 - 8a_{21} M) + \right. \end{aligned}$$

$$\left. \begin{aligned} & (4a_{17} + (9a_{21} + 3a_{20}h + 2a_{23}h + 2a_{22}h^3)M) \cosh(Mh) - \\ & (a_{17} + 2a_{16}h + 3a_{15}h^2) \cosh(2Mh) - (a_{21} + a_{20}h)M \cosh(3Mh) \\ & (a_{20} - 2a_{23} - 6a_{22}h^2) \sinh(Mh) + 4a_{19}M \sinh(2Mh) - a_{20} \sinh(3Mh) - \\ & \frac{2a_{19}M \sinh(4Mh)}{2Mh \cosh(Mh) - 2\sinh(Mh)} \end{aligned} \right\}. \quad (31)$$

轴向感应磁场强度表达式可借助 $h_x = \quad / y$ 得到

$$\begin{aligned} h_x = & a_{28}M \sinh(My) + 4a_{29}y^3 + 2a_{30}y + W_e^2 (3a_{32}y^2 \cosh(My) \\ & a_{32}My^3 \sinh(My) + 2a_{33}y \cosh(My) + a_{33}My^2 \sinh(My) + 2a_{34}y \sinh(My) + \\ & a_{34}y^2 \cosh(My) + a_{35} \cosh(My) + a_{35}My \sinh(My) + a_{36} \sinh(My) + \\ & a_{36}My \cosh(My) + a_{37}M \sinh(My) + a_{38}M \cosh(My) + 3a_{39}M \sinh(3My) + \\ & 2a_{40}M \sinh(2My) + 2a_{41}M \cosh(2My) + a_{42} \sinh(2My) + \\ & 2a_{42}My \cosh(2My) + 4a_{43}y^3 + 2a_{44}y + a_{46}). \end{aligned} \quad (32)$$

在固定坐标系中, 任意轴向位置的流量为

$$Q = \int_{h_2}^{h_1} (u + 1) dy = \int_{h_2}^{h_1} u dy + \int_{h_2}^{h_1} dy = q + h. \quad (33)$$

蠕动波在 1 个周期 ($T = \quad / c$) 内平均体积流量比定义为

$$Q = \frac{1}{T} \int_0^T Q dt = \frac{1}{T} \int_0^T (q + h) dt = q + 1. \quad (34)$$

压力增量的无量纲表达式定义为

$$P = \int_0^1 \left(\frac{dP}{dx} \right) dx. \quad (35)$$

4 种被考虑的无量纲波形表达式如下:

1) 正弦波

$$h(x) = 1 + \sin(2x);$$

2) 三角形波

$$h(x) = 1 + \left[\frac{8}{3} \sum_{n=1} \frac{(-1)^{n+1}}{(2n-1)} \sin(2(2n-1)x) \right];$$

3) 梯形波

$$h(x) = 1 + \left[\frac{32}{2} \sum_{n=1} \frac{\sin(\sqrt{8})(2n-1)}{(2n-1)^2} \sin(2(2n-1)x) \right];$$

4) 多个正弦波

$$h(x) = 1 + \sin(2mx).$$

3 图形结果和讨论

本节给出解的图形结果. 利用数学软件, 数值地计算压力增量的表达式. 压力增量、温度、浓度、磁力函数和流函数的结果示于图 1 至图 7.

图 1(a) 示出不同 Weissenberg 数 W_e 时, 压力增量 P 随体积流量比 Q 的变化, 其他参数为 $\beta = 0.2$, $Gr = 1$, $\gamma = 0.1$, $a = 0.1$, $\delta = 0.1$, $\epsilon = 0.2$, $M = 0.5$, $E = 0.5$. 图 1(b) 示出不同 M 时, 压力增量 P 随体积流量比 Q 的变化, 其他参数为 $\beta = 0.3$, $Gr = 0.5$, $\gamma = 0.8$, $a = 0.1$, $\delta = 0.2$, $\epsilon = 0.2$, $W_e = 0.3$, $E = 0.4$. 图 1(c) 示出不同 β 值时, 压力增量 P 随体积流量比 Q

的变化,其他参数为 $\beta = 0.9, Gr = 2, B = 0.1, a = 0.5, G = 0.2, M = 0.3, We = 0.3, E = 0.4$. 从图形可以看出,压力增量和体积流量比都呈反比例关系. 意味着,体积流量比小时,压力增量更大,体积流量比大时,压力增量更小. 图 1(a)的区域 $-1 \leq Q < 0$ 以及图 1(b)和(c)的区域 $-1 \leq Q \leq 1.3$ 管壁的蠕动起着泵的作用. 在图 1的其他区域,增长了泵的作用. 从图 1中还可以看到,压力增量随着 We 和 β 的增大而减小,但随着 M 的增大而增大.

当 $x = 0.2$ 和 $\beta = 0.2$ 时,温度分布曲线示于图 2. 可以看出,随着 B 的增大,温度分布曲线上升.

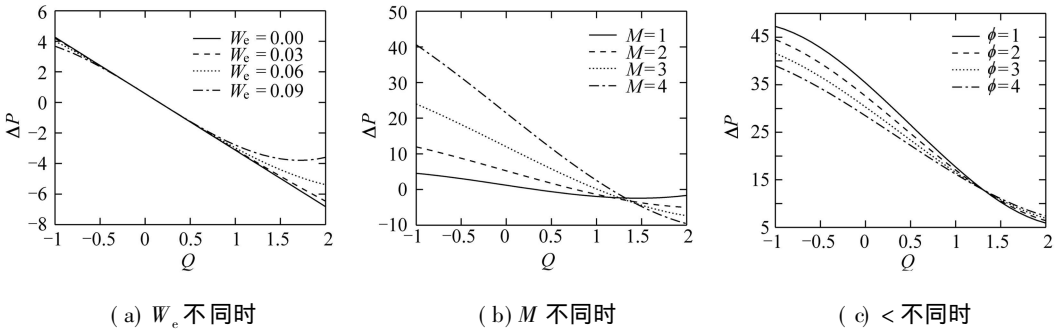


图 1 不同 We, M 和 β 时,压力增量 ΔP 随流量比 Q 的变化

图 3(a) 示出了不同 Weissenberg 数 We 时,轴向感应磁场强度 h_x 随着空间变量 y 的变化,其他参数为 $L = 0.2, Gr = 1, B = 0.1, a = 0.1, G = 0.1, \beta = 0.2, M = 0.5, E = 0.5, Rm = 0.5$. 图 3(b) 示出不同磁 Reynolds 数 Rm 时,轴向感应磁场强度 h_x 随着空间变量 y 的变化,其他参数 $L = 0.2, Gr = 1, B = 0.1, a = 0.1, G = 0.1, \beta = 0.2, M = 0.5, E = 0.5, We = 0.1$. 从图中可以看出,随着 Rm, We 的增大,管道上半部中的 h_x 也增大,而管道下半部中的 h_x 反而减小.

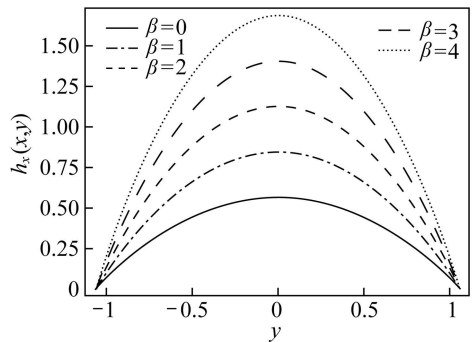


图 2 温度分布曲线

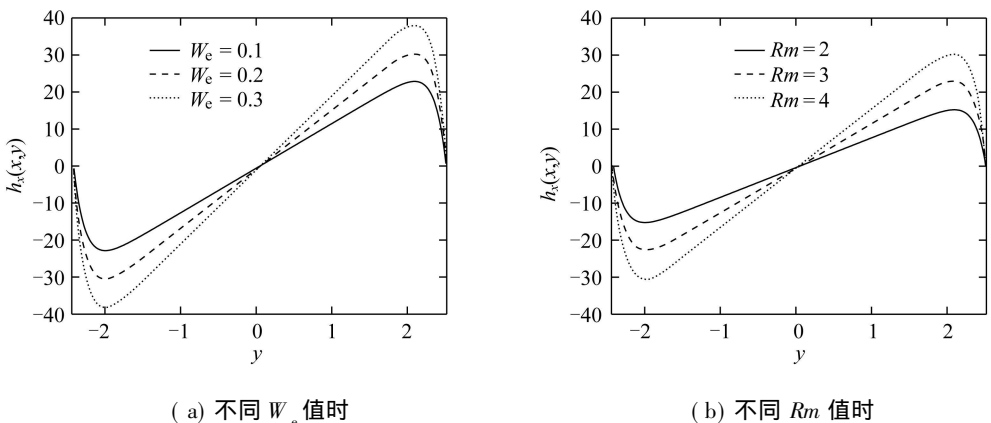
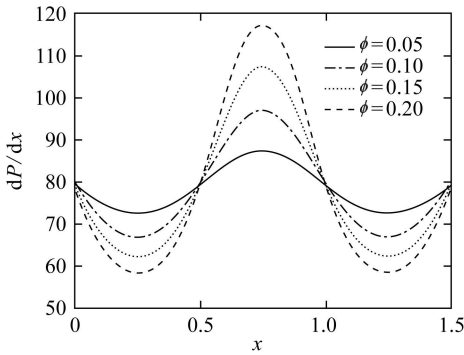


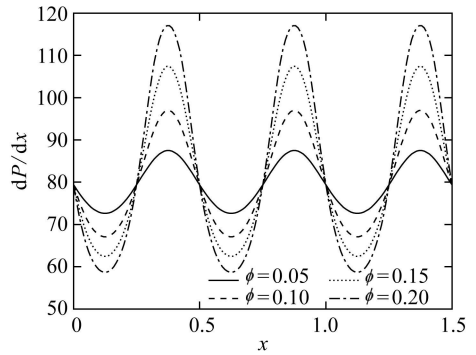
图 3 不同 We 和 Rm 时,轴向感应磁场强度 $h_x(x,y)$ 随 y 的变化

不同波型时,压力梯度的性质示于图 4 其中 $L = 0.3, Gr = 1, B = 0.1, a = 0.1, G = 0$

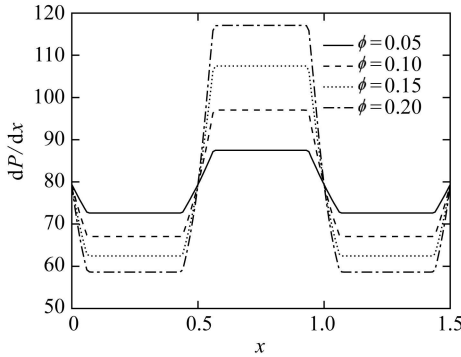
2 (= - 1 M = 0 5 E = 0 5 W_e = 0 3. 由图 4 可以看出, 在区间 x I [0 0 5] 和 x I [1 1 1 5] 中, 压力梯度小, 而在区间 x I [0 5] 中, 压力梯度大. 还可以看出, 压力梯度随着 < 的增大而增大.



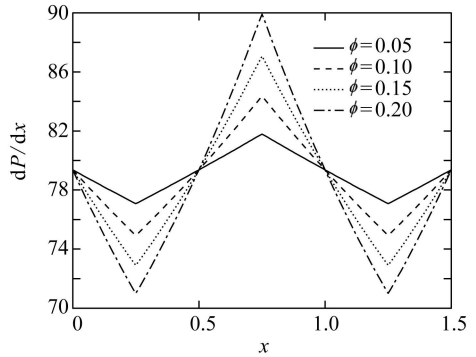
(a) 正弦波



(b) 多个正弦波

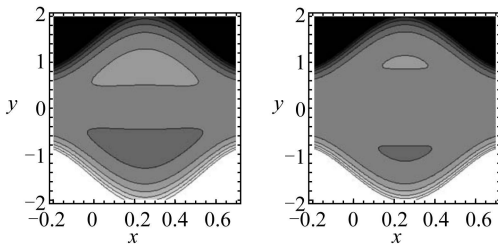


(c) 梯形波

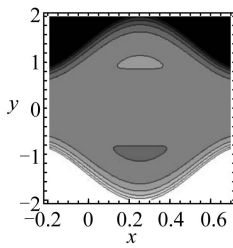


(d) 三角形波

图 4 不同波型时压力梯度的变化

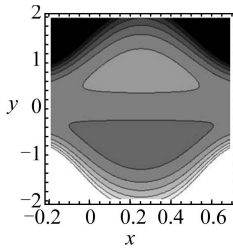


(a) M = 2

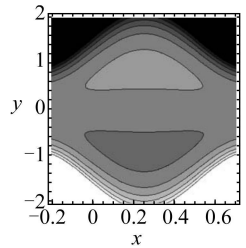


(b) M = 3

图 5 不同 M 时的流线图



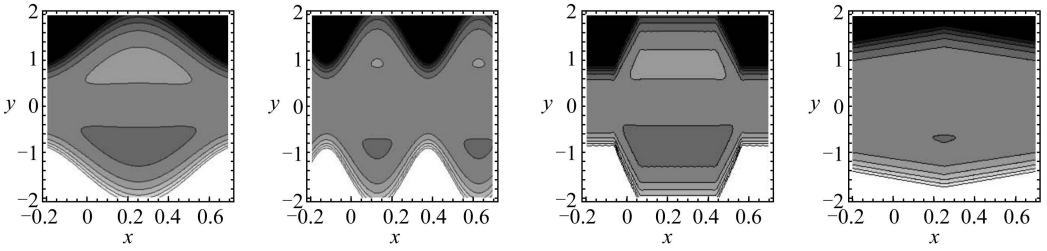
(a) W_e = 0 1



(b) W_e = 0 2

图 6 不同 W_e 时的流线图

图 5~ 7 给出了流线的 /俘获 0 现象. 图 5 中的 M = 2 和 3, L = 0 3 Gr = 0 6 B = 0 8 a = 0 1 G = 0 2 < = P/6 W_e = 0 1 E = 0 4 Q = 1 时, 随着 M 的增大, /俘获 0 的团块 (指闭合流线所围的面积)) 校者注) 反而变小. 图 6 中的 W_e = 0 1 和 0 2 L = 0 3 Gr = 0 6 B = 0 8 a = 0 1 G = 0 2 < = P/6 M = 2 E = 0 4 Q = 1 时, 随着 W_e 的增大, /俘获 0 的团块也变小了. 图 7 绘出了不同波型时的流线图. 由图可以看出, 三角形波 /俘获 0 团块的大小小于其他类型的波.



(a) 正弦波

(b) 多个正弦波

(c) 梯形波

(d) 三角形波

图 7 不同波型时的流线图

4 结 论

在一个具有感应磁流体力学的 Johnson-Segahan 流体中, 给出了蠕动流和热传导的研究实例. 利用长波假定来简化控制方程. 采用常规的摄动法, 求得该方程的流函数、磁力函数和轴向压力梯度. 完成的分析要点如下:

- 1) 压力增量随着 M 的增大而增大, 随着 α 和 W_e 的增大反而减小;
- 2) W_e 和 α 对压力增量的影响, 性质上是类似的;
- 3) W_e 和 Rm 对轴向感应磁场的影响也类似;
- 4) 温度分布曲线随着 B 的增大而升高;
- 5) 与梯形波和正弦波相比, 三角形波的 streamline / 俘获 0 的团块体尺寸最小;
- 6) 压力梯度随着 α 的增大而增大.

附录 A

$$\begin{aligned}
 a_1 &= \frac{BGrL}{2(L+G)}, \quad a_2 = -\frac{GrL}{(L+G)} - M^2E - \frac{h^2_B hGrL}{2(L+G)}, \quad a_3 = -\frac{a_1}{3M^2}, \quad a_4 = -\frac{a_1^2}{3M^4} - \frac{a_2}{M^2} \\
 a_5 &= \frac{F+h+2a_3h^3}{\sinh(Mh) - Mh \cosh(Mh)}, \quad a_6 = M^2(1+a_4+3a_3h^2+a_5M \cosh(Mh)), \\
 a_7 &= a_5^3 M^6, \quad a_8 = (6a_3)^3, \quad a_9 = 18a_3^2 M^4 a_3, \quad a_{10} = 108a_5 a_3^2 M^2 a, \quad a_{11} = -\frac{(a^2-1)Ga_7}{L+G}, \\
 a_{12} &= -\frac{(a^2-1)a_8}{L+G}, \quad a_{13} = -\frac{(a^2-1)Ga_9}{L+G}, \quad a_{14} = -\frac{(a^2-1)Ga_{10}}{L+G}, \\
 a_{15} &= \frac{a_{14}}{6M}, \quad a_{16} = -\frac{a_{14}}{4M^2}, \quad a_{17} = -\frac{3a_{11}}{8M} + \frac{a_{14}}{4M^3}, \quad a_{18} = \frac{3a_{11}}{16M^2} - \frac{a_{14}}{32M^4}, \\
 a_{19} &= \frac{a_{11}}{32M^2}, \quad a_{20} = \frac{a_{13}}{6M^2}, \quad a_{21} = -\frac{2a_{13}}{9M^3}, \quad a_{22} = -\frac{a_{12}}{M^2}, \quad a_{23} = \frac{a_{13}}{2M^2} - \frac{6a_{12}}{M^4}, \\
 a_{24} &= -\frac{2(a_{17}+2a_{21}M)}{M}, \\
 a_{25} &= (2a_{17}+3a_{21}M-2a_{22}h^3M - (2a_{17}+4a_{21}M+h(a_{10}-h(a_{17}+h(a_{16}+a_{13}h))))M^2) \cosh(Mh) + M(a_{21} \cosh(2Mh) - 3a_{19}Mh + \cosh(3Mh) + (a_{10}+h(2a_{17}-h(a_{16}+2a_{15}h)+4a_{21}M))) \sinh(Mh) - 2h(a_{21}+a_{20}h) @ \\
 &M \sinh(3Mh)) / (M(Mh \cosh(Mh) - \sinh(Mh))), \\
 a_{26} &= (M^2(-3a_{17}+2a_{16}h+3a_{16}h^2-8a_{21}M) + (4a_{17}+(9a_{21}+3a_{20}h+2a_{23}h+2a_{22}h^3)M) \cosh(Mh) - (a_{17}+2a_{16}h+3a_{15}h^2) \cosh(2Mh) - (a_{21}+a_{20}h) @ \\
 &M \cosh(3Mh) + (a_{20}-2a_{23}-6a_{22}h^2) \sinh(Mh) + 4a_{19}M \sinh(2Mh) -
 \end{aligned}$$

$$\begin{aligned}
& a_{20} \sinh(3Mh) - 2a_{19}M \sinh(4Mh) / (2Mh \cosh(Mh) - 2\sinh(Mh)), \\
a_{27} = & -M(2a_{17} + 3a_{21}M), \quad a_{28} = -\frac{Rma_5}{M}, \quad a_{29} = -\frac{Rma_3}{4}, \quad a_{30} = \frac{ERm}{2} - \frac{Rma_4}{2} + \frac{Rma_6}{M^2}, \\
a_{31} = & -(a_{28} \cosh(Mh) + a_{29}h^4 + a_{30}h^2), \quad a_{32} = -\frac{a_{15}Rm}{M}, \quad a_{33} = -\frac{a_{16}Rm}{M}, \quad a_{34} = -\frac{3a_{15}Rm}{M^2}, \\
a_{35} = & -\frac{6a_{15}Rm}{M^3} - \frac{a_{17}Rm}{M}, \quad a_{36} = \frac{2a_{16}Rm}{M^2}, \quad a_{37} = -\frac{2a_{16}Rm}{M^3} - \frac{a_{18}Rm}{M} - \frac{a_{25}Rm}{M}, \\
a_{38} = & -\frac{a_{24}Rm}{M} + \frac{6a_{15}Rm}{M^4} + \frac{a_{17}Rm}{M^2}, \quad a_{39} = -\frac{a_{19}Rm}{3M}, \quad a_{40} = \frac{a_{20}Rm}{4M^2}, \quad a_{41} = -\frac{a_{21}Rm}{2M}, \\
a_{42} = & \frac{2a_{20}Rm}{4M}, \quad a_{43} = -\frac{a_{22}Rm}{4}, \quad a_{44} = -\frac{a_{23}Rm}{2} + \frac{a_{26}Rm}{2M^2}, \quad a_{45} = \frac{a_{27}Rm}{M^2}, \\
a_{46} = & -a_{35} - a_{38}M - 2a_{41}M, \\
a_{47} = & a_{35}h + a_{44}h^2 - a_{43}h^4 + a_{38}Mh + 2a_{41}Mh - a_{37} \cosh(Mh) - a_{38}h \cosh(Mh) - \\
& a_{33}h^2 \cosh(Mh) - a_{32}h^3 \cosh(Mh) - a_{40} \cosh(2Mh) - a_{39} \cosh(3Mh) - \\
& a_{38} \sin(Mh) - a_{36}h \sin(Mh) - a_{34}h^2 \sin(Mh) - a_{41} \sin(2Mh) - a_{42}h \sin(2Mh).
\end{aligned}$$

参考文献:

- [1] Latham T W. Fluid motion in a peristaltic pump[D]. M S Thesis Cambridge Massachusetts Institute of Technology, 1966.
- [2] Nadeem S, Akbar N S. Influence of heat transfer on a peristaltic flow of Johnson-Segalman fluid in a non-uniform tube[J]. Int Comm un Heat Mass Transfer, 2009, 36(10): 1050-1059.
- [3] Nadeem S, Akbar N S. Effects of heat transfer on the peristaltic transport of MHD Newtonian fluid with variable viscosity: application of Adomian decomposition method[J]. Comm un Non linear Sci Numer Sim ul, 2009, 14(11): 3844-3855.
- [4] Nadeem S, Akbar N S. Influence of heat transfer on a peristaltic transport of Herschel-Bulkley fluid in a non-uniform inclined tube[J]. Comm un Non linear Sci Numer Sim ul, 2009, 14(12): 4100-4113.
- [5] Nadeem S, Akbar N S, Hayat T, Malik M Y. On the influence of heat transfer in peristalsis with variable viscosity[J]. Int J Heat Mass Transfer, 2009, 52(21/22): 4722-4730.
- [6] Nadeem S, Akbar N S. Influence of radially varying MHD on the peristaltic flow in an annulus with heat and mass transfer[J]. Journal of the Taiwan Institute of Chemical Engineers. doi: 10.1016/j.jtice.2009.11.004.
- [7] Srinivas S, Kothandapani M. The influence of heat and mass transfer on MHD peristaltic flow through a porous space with compliant walls[J]. Appl Math Comp, 2009, 213(1): 197-208.
- [8] Mekheimer Kh S, Abd Elmaboud Y. The influence of heat transfer and magnetic field on peristaltic transport of a Newtonian fluid in a vertical annulus: application of an endoscope[J]. Phys Lett A, 2008, 372(10): 1657-1665.
- [9] Ebaid A. A new numerical solution for the MHD peristaltic flow of a biofluid with variable viscosity in circular cylindrical tube via Adomian decomposition method[J]. Phys A, 2008, 372(32): 5321-5328.
- [10] Mekheimer Kh S. Effect of the induced magnetic field on peristaltic flow of a couple stress fluid[J]. Phys Lett A, 2008, 372(23): 4271-4278.
- [11] Srivastava L M, Agrawal R P. Oscillating flow of a conducting fluid with suspension of spheri-

J Appl Mech, 1980, 47(1): 196-199.

- [12] Vajravelu K, Radhakrishnam acharya G, Radhakrishnamurty V. Peristaltic flow and heat transfer in a vertical porous annulus with long wave approximation[J]. Int J Non Linear Mech, 2007, 42(5): 754-759.
- [13] Vajravelu K, Sreenadh S, Ramesh Babu V. Peristaltic pumping of a Herschel-Bulkley fluid in a channel[J]. Appl Math Comput, 2005, 169(1): 726-735.
- [14] Vajravelu K, Sreenadh S, Ramesh Babu V. Peristaltic transport of a Herschel-Bulkley fluid in an inclined tube[J]. Int J Non-Linear Mech, 2005, 40(1): 83-90.
- [15] Elshahawy E F, Elhadabe N T, Elghazly E M, Ebaid A. Peristaltic transport in an asymmetric channel through a porous medium [J]. Appl Math Comput, 2006, 182(1): 140-150.
- [16] Ealshahed M, Haroun M H. Peristaltic transport of Johnson-Segman fluid under effect of a magnetic field[J]. Math Probl Eng, 2005, 6(8): 663-677.
- [17] Haroun M H. Non-linear peristaltic flow of a fourth grade fluid in an inclined asymmetric channel[J]. Computational Materials Science, 2007, 39(2): 324-333.

E f f e c t s o f I n d u c e d M a g n e t i c F i e l d o n t h e P e r i s t a l t i c
F l o w o f J o h n s o n - S e g a m a n F l u i d i n a V e r t i c a l
S y m m e t r i c C h a n n e l

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Abstract The influence of heat transfer and induced magnetic field on peristaltic flow of a Johnson-Segman fluid was studied. The purpose of the present investigation was to study the effects of induced magnetic field on the peristaltic flow of non-Newtonian fluid. The two-dimensional equations of Johnson-Segman fluid were simplified by assuming a long wave length and low Reynolds number. The obtained equations were solved for the stream function, magnetic force function, and axial pressure gradient by using a regular perturbation method. The expressions for the pressure rise, temperature, induced magnetic field, pressure gradient, and stream function were sketched for various embedded parameters and were interpreted.

Key words induced magnetic field, vertical symmetric channel, Johnson-Segman fluid, magnetohydrodynamics (MHD)