

二维流面上的流动问题的速度图方法*

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(郭兴明推荐)

摘要: 对于一些特殊的流动,尤其是平面上的位势流动,速度图方法有其显著的优点.对于理想流体来说,流面总是存在的,在流面上,流动的速度向量总是在其切空间里.通过引入流函数和势函数,采用张量分析作为工具,给出了二维曲流面上位势流动的速度图方法,得到了流函数满足的速度图方程,为一些特殊的流动问题提供了一类分析方法.并且,对于得到的二维速度图方程,得到了相应的特征方程和特征根,从而可以对方程的类型进行分类.最后,给出了一些特殊流动的实例.

关键词: 速度图方法; 位势流; 流面; 流函数; 位势函数

中图分类号: O183;O175;O35 **文献标志码:** A

DOI: 10.3879/j.issn.1000-0887.2010.03.009

引 言

众所周知,传统的速度图方法在空气动力学研究中发挥了重要的作用.然而,该方法仅仅被应用在二维的平面无粘流动问题中,可见文献[1-3].在本文中,我们使用流面的概念:一个 R^3 中的二维的流形,如果流动的速度向量总是在其切空间里,称这个流形为流动的流面,可以证明这种流面总是存在的,见文献[4-6].在流面上,是否也可以建立相应的速度图方法呢?这是本文的主要动机和目的.通过本文,我们给出了二维流形上的速度图方法,并且得到了速度图方程的特征方程和特征根,从而可以对方程进行分类.对于二维平面流动,这些结果和经典结论是一致的.

本文的组织结构如下:在第1节中我们基于二维流形引入三维空间的半测地坐标系,并得到该坐标系下的可压缩粘性流动的 Navier-Stokes 方程.在第2节中,基于前面的 Navier-Stokes 方程的表示,我们引入流函数,通过速度图变换得到了流函数满足的二阶方程,并给出了该方程对应的特征方程和特征根,从而可以对速度图方程进行分类.最后,我们在第3节中给出了一些特殊流动下的结果.

1 半测地坐标系下的 Navier-Stokes 方程

在本节中,我们将给出基于二维流面的半测地坐标系下的关于 Navier-Stokes 方程的一些

* 收稿日期: 2009-07-15; 修订日期: 2010-02-02

基金项目: 国家自然科学基金资助项目(10971165;10771167;10926080)

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结果,主要结论来自于文献[4-7].

1.1 基于二维流面的半测地坐标系

记 S 是一个二维流形,而 P 是三维空间中 S 附近的一点, O 是原点,我们知道 P 点可以表示为

$$\mathbf{R} = \vec{OP} = \mathbf{r} + \xi \mathbf{n}, \text{ 以及 } \mathbf{r} = \vec{OP}_o, P_o P = \xi \mathbf{n},$$

其中, P_o 是点 P 在 S 上的投影, \mathbf{n} 是 $P_o P$ 方向上的单位向量. 当 (x^1, x^2) 是 S 上的一个 Gauss 曲线坐标系时,点 P 可以唯一地表示为 (x^1, x^2, ξ) . 在文献[8]中, Il'in 证明了当 $\mathbf{r}: R^2 \supset S \rightarrow R^3$ 是一个 C^3 映照时,存在从 S 上的 \mathbf{r} 到其邻域 Ω_ε 的正则延拓 \mathbf{R} :

$$\mathbf{R}(x, \xi) = \mathbf{r}(x) + \xi \mathbf{n}(x), \quad \forall (x, \xi) \in \Omega^\varepsilon,$$

其中 \mathbf{R} 是从 Ω^ε 到 $R(\Omega^\varepsilon)$ 上的 C^1 映照,而且3个向量 $\mathbf{e}_\alpha = \partial \mathbf{R} / \partial x^\alpha, \alpha = 1, 2, \mathbf{e}_3 = \partial \mathbf{R} / \partial \xi$ 在 Ω^ε 内是处处线性无关的. 因此 (x, ξ) 可以看做是 S 附近一点 P 在 R^3 中的坐标表示,被称为 S 邻域的半测地坐标.

在本文中,拉丁字母 i, j, k, \dots 等在 $\{1, 2, 3\}$ 中取值,而希腊字母 $\alpha, \beta, \gamma, \dots$ 等在 $\{1, 2\}$ 中取值. 另外,对重复的指标使用 Einstein 求和约定.

流形 S 上的第一、二和三基本型 $\{a_{\alpha\beta}, b_{\alpha\beta}, c_{\alpha\beta}\}$ 定义为

$$\begin{cases} a_{\alpha\beta} = \mathbf{r}_\alpha \cdot \mathbf{r}_\beta, b_{\alpha\beta} = \mathbf{n} \cdot \mathbf{r}_{\alpha\beta} = -(\mathbf{n}_\alpha \cdot \mathbf{r}_\beta + \mathbf{r}_\alpha \cdot \mathbf{n}_\beta) / 2, \\ c_{\alpha\beta} = \mathbf{n}_\alpha \cdot \mathbf{n}_\beta = a^{\lambda\sigma} b_{\alpha\lambda} b_{\beta\sigma}, a^{\alpha\beta} a_{\beta\gamma} = \delta_\gamma^\alpha, \\ \hat{b}^{\alpha\beta} b_{\beta\lambda} = \delta_\lambda^\alpha, \hat{c}^{\alpha\beta} c_{\beta\lambda} = \delta_\lambda^\alpha, b^{\alpha\beta} = a^{\alpha\lambda} a^{\beta\sigma} b_{\lambda\sigma}, c^{\alpha\beta} = a^{\alpha\lambda} a^{\beta\sigma} c_{\lambda\sigma}, \end{cases} \quad (1)$$

其中 $\hat{b}^{\alpha\beta}, \hat{c}^{\alpha\beta}$ 分别为 $a_{\alpha\beta}, b_{\alpha\beta}$ 的逆矩阵元素. S 的平均曲率 H 和 Gauss 曲率 K 分别为

$$H = \frac{1}{2} a^{\alpha\beta} b_{\alpha\beta}, K = \frac{\det(b_{\alpha\beta})}{\det(a_{\alpha\beta})}.$$

很容易验证下面两个常用的关系式成立^[5]:

$$K a_{\alpha\beta} - 2H b_{\alpha\beta} + c_{\alpha\beta} = 0, a^{\alpha\beta} - 2H \hat{b}^{\alpha\beta} + K \hat{c}^{\alpha\beta} = 0. \quad (2)$$

同时我们还需要用到 S 上的行列式张量 $\varepsilon^{\alpha\beta}, \varepsilon_{\alpha\beta}$, 定义为

$$\varepsilon_{\alpha\beta} = \begin{cases} \sqrt{a}, \\ -\sqrt{a}, \\ 0, \end{cases} \quad \varepsilon^{\alpha\beta} = \begin{cases} 1/\sqrt{a}, & (\alpha, \beta) \text{ 是 } (1, 2) \text{ 的偶排列,} \\ -1/\sqrt{a}, & (\alpha, \beta) \text{ 是 } (1, 2) \text{ 的奇排列,} \\ 0, & \text{其它情形.} \end{cases} \quad (3)$$

此外,我们还需要下面的引理^[5]:

引理 1 在半测地坐标系下, R^3 上的度量张量、Christoffel 符号、协变导数、散度和旋度可以用 S 上的 $\{a_{\alpha\beta}, b_{\alpha\beta}, c_{\alpha\beta}\}$ 分别表示为

$$\begin{cases} g_{\alpha\beta} = a_{\alpha\beta} - 2\xi b_{\alpha\beta} + \xi^2 c_{\alpha\beta}, g_{3\alpha} = g_{\alpha 3} = 0, g_{33} = 1, \\ g^{\alpha\beta} = \theta^{-2} G^{\alpha\beta}, g^{3\alpha} = g^{\alpha 3} = 0, g^{33} = 1, \\ g = \det(g_{ij}) = \theta^2 a, a = \det(a_{\alpha\beta}), \end{cases} \quad (4)$$

$$\begin{cases} \Gamma_{\alpha\beta}^\gamma = \Gamma_{\alpha\beta}^{*\gamma} + \theta^{-1} R_{\alpha\beta}^\gamma, \Gamma_{\beta 3}^\alpha = \theta^{-1} I_\beta^\alpha, \Gamma_{\alpha\beta}^3 = J_{\alpha\beta}, \\ \Gamma_{\beta 3}^3 = \Gamma_{3\beta}^3 = \Gamma_{33}^\alpha = \Gamma_{33}^3 = 0, \end{cases} \quad (5)$$

$$\left\{ \begin{aligned} \nabla_\alpha u^\beta &= \overset{*}{\nabla}_\alpha u^\beta + \theta^{-1}(I_\alpha^\beta u^3 + R_{\alpha\lambda}^\beta u^\lambda), \quad \nabla_\alpha u^3 = \frac{\partial u^3}{\partial x^\alpha} + J_{\alpha\beta} u^\beta, \\ \nabla_3 u^3 &= \frac{\partial u^3}{\partial \xi}, \quad \nabla_3 u^\beta = \frac{\partial u^\beta}{\partial \xi} + \theta^{-1} I_\alpha^\beta u^\alpha, \\ \operatorname{div} \mathbf{u} &= \overset{*}{\operatorname{div}} \mathbf{u} + \frac{\partial u^3}{\partial \xi} + \theta^{-1} [2(-H + K\xi)u^3 + \\ &\quad u^\alpha(-2\overset{*}{\nabla}_\alpha H \xi + \overset{*}{\nabla}_\alpha K \xi^2)], \\ \operatorname{rot}(\mathbf{u}) &= (\operatorname{rot}(\mathbf{u}))^\alpha \mathbf{e}_\alpha + (\operatorname{rot}(\mathbf{u}))^3 \mathbf{n}, \\ (\operatorname{rot}(\mathbf{u}))^\alpha &= \theta^{-1} \varepsilon^{\alpha\beta} \left(\overset{*}{\nabla}_\beta u^3 - g_{\beta\lambda} \frac{\partial u^\lambda}{\partial \xi} \right), \\ (\operatorname{rot}(\mathbf{u}))^3 &= \varepsilon^{\beta\sigma} g_{\beta\lambda} [\theta^{-1} \overset{*}{\nabla}_\sigma u^\lambda + \theta^{-2} R_{\sigma\nu}^\lambda u^\nu], \end{aligned} \right. \quad (6)$$

其中, $\overset{*}{\Gamma}_{\alpha\beta}^\gamma, \overset{*}{\Delta}, \overset{*}{\operatorname{div}}, \overset{*}{\nabla}_\alpha$ 分别表示 S 上的 Christoffel 符号、Laplace 算子、散度算子和协变导数, 以及

$$\theta = 1 - 2H\xi + K\xi^2, \quad G^{\alpha\beta} = a^{\alpha\beta} - 2K\xi \hat{b}^{\alpha\beta} + \xi^2 K^2 \hat{c}^{\alpha\beta},$$

$$I_\beta^\alpha = -b_\beta^\alpha + K\xi \delta_\beta^\alpha, \quad J_{\alpha\beta} = b_{\alpha\beta} - \xi c_{\alpha\beta}, \quad R_{\beta\sigma}^\alpha = (2H\xi^2 - \xi) \overset{*}{\nabla}_\sigma b_\beta^\alpha - b_\mu^\alpha \overset{*}{\nabla}_\sigma b_\beta^\mu \xi^2.$$

特别地, 当 S 是一个流面时, $u^3 = 0$, 此时, 在流面 S (对应于 $\xi = 0$) 上有

$$\left\{ \begin{aligned} g_{\alpha\beta} &= a_{\alpha\beta}, \quad g_{\alpha 3} = g_{3\alpha} = 0, \quad g_{33} = 1, \quad g = a, \\ g^{\alpha\beta} &= a^{\alpha\beta}, \quad g^{\alpha 3} = g^{3\alpha} = 0, \quad g^{33} = 1, \\ \overset{*}{\Gamma}_{\alpha\beta}^\gamma &= \overset{*}{\Gamma}_{\alpha\beta}^\gamma, \quad \overset{*}{\Gamma}_{\beta 3}^\alpha = -b_\beta^\alpha, \quad \overset{*}{\Gamma}_{\alpha\beta}^3 = b_{\alpha\beta}, \quad \overset{*}{\Gamma}_{i3}^3 = \overset{*}{\Gamma}_{33}^i = 0, \end{aligned} \right. \quad (7)$$

$$\left\{ \begin{aligned} \nabla_\alpha u^\beta &= \overset{*}{\nabla}_\alpha u^\beta, \quad \nabla_3 u^\beta = \frac{\partial u^\beta}{\partial \xi} - b_\beta^\alpha u^\alpha, \quad \nabla_\alpha u^3 = \frac{\partial u^3}{\partial x^\alpha} + b_{\alpha\beta} u^\beta, \quad \nabla_3 u^3 = \frac{\partial u^3}{\partial \xi}, \\ \operatorname{div} \mathbf{u} &= \overset{*}{\operatorname{div}} \mathbf{u} + \frac{\partial u^3}{\partial \xi}, \quad (\operatorname{rot}(\mathbf{u}))^\alpha = -\varepsilon^{\alpha\beta} a_{\beta\lambda} \frac{\partial u^\lambda}{\partial \xi}, \quad (\operatorname{rot}(\mathbf{u}))^3 = \varepsilon^{\beta\sigma} a_{\beta\lambda} \overset{*}{\nabla}_\sigma u^\lambda, \end{aligned} \right. \quad (8)$$

$$\left\{ \begin{aligned} \Delta u^\alpha &= \overset{*}{\Delta} u^\alpha + \frac{\partial^2 u^\alpha}{\partial \xi^2} - 2(b_\beta^\alpha + H\delta_\beta^\alpha) \frac{\partial u^\beta}{\partial \xi} + K u^\alpha, \\ \Delta u^3 &= \frac{\partial^2 u^3}{\partial \xi^2} - 2H \frac{\partial u^3}{\partial \xi} + 2b_\lambda^\nu \overset{*}{\nabla}_\nu u^\lambda + 2u^\beta \overset{*}{\nabla}_\beta H, \\ \Delta T &= \overset{*}{\Delta} T + \frac{\partial^2 T}{\partial \xi^2} - H \frac{\partial T}{\partial \xi}, \end{aligned} \right. \quad (9)$$

这里我们用到了结论

$$\overset{*}{\Delta} u^3 \equiv a^{\alpha\beta} \overset{*}{\nabla}_\alpha \overset{*}{\nabla}_\beta u^3 = 0, \quad \overset{*}{\nabla}_\nu u^3 = 0, \quad \text{在 } S \text{ 上}, \quad (10)$$

这是由于在流面 S 上 $u^3 = 0$.

另外我们还会用到流面 S 上的旋度算子

$$\operatorname{rot}(\mathbf{u}) = (\operatorname{rot}(\mathbf{u}))^3 |_S = \varepsilon^{\beta\sigma} a_{\beta\lambda} \overset{*}{\nabla}_\sigma u^\lambda = \varepsilon_{\alpha\beta} \overset{*}{\nabla}^\alpha u^\beta = \varepsilon^{\alpha\beta} \overset{*}{\nabla}_\alpha u_\beta. \quad (11)$$

1.2 半测地坐标系下的 Navier-Stokes 方程

我们考虑定常的可压缩粘性流动问题. 当采用以角速度大小 ω 绕 z 轴旋转的非惯性坐标系时, 控制方程可以表示为

$$\begin{cases} \operatorname{div}(\rho \mathbf{u}) = 0, & \text{连续性方程,} \\ -\mu \Delta \mathbf{u} + \rho(\mathbf{u} \cdot \nabla) \mathbf{u} + \nabla \left(p - \frac{\mu}{3} \operatorname{div} \mathbf{u} \right) + 2\rho \boldsymbol{\omega} \times \mathbf{u} = \\ \quad \rho \boldsymbol{\omega} \times (\boldsymbol{\omega} \times \mathbf{R}) + \mathbf{f}, & \text{动量方程,} \\ \operatorname{div}(\rho E \mathbf{u}) + p \operatorname{div} \mathbf{u} - \operatorname{div}(\kappa \operatorname{grad} T) - \Phi = 0, & \text{能量方程,} \\ p = p(\rho, T), & \text{状态方程,} \end{cases} \quad (12)$$

其中, $\mathbf{u}, \rho, p, E = C_v T, C_v, T, \kappa, \nu = \mu/\rho, 2\rho \boldsymbol{\omega} \times \mathbf{u}, \mathbf{F} = \mathbf{f}/\rho + \boldsymbol{\omega} \times (\boldsymbol{\omega} \times \mathbf{R})$ 分别为流体相对旋转坐标系的相对速度、密度、压力、单位体积下的内能、比热容、温度、热传导系数、动力粘性常数、Coriolis 力、单位质量下的外力和离心力, $\boldsymbol{\omega}$ 为角速度向量, 应力张量 $\boldsymbol{\sigma}$ 和耗散函数 Φ 分别定义为

$$\sigma^{ij} = g^{ij} \left(-p - \frac{2}{3} \mu \operatorname{div} \mathbf{u} \right) + 2\mu e^{ij}(\mathbf{u}), \quad e^{ij}(\mathbf{u}) = \frac{1}{2} (\nabla^i u^j + \nabla^j u^i), \quad (13)$$

$$\Phi = 2\mu e^{ij}(\mathbf{u}) e_{ij}(\mathbf{u}) - \frac{2}{3} \mu (\operatorname{div} \mathbf{u})^2. \quad (14)$$

有些情形下,我们会用如下的熵方程代替前面的能量方程

$$\frac{ds}{dt} = \frac{1}{|\mathbf{u}|^2 T} \left(\frac{\kappa}{\rho} \Delta T + \frac{\Phi}{\rho} \right), \quad (15)$$

其中 $s = R \lg(T^{\gamma/(\gamma-1)}/p)$ 表示单位质量的熵, $|\mathbf{u}|^2 = g_{ij} u^i u^j$.

由引理 1 我们可知

定理 1 在流面 $S(\xi = 0, u^3 = 0)$ 上, Navier-Stokes 方程(12)和(15)可以表示为

$$\begin{aligned} & -\mu \left(\Delta u^\alpha + \frac{\partial^2 u^\alpha}{\partial \xi^2} - 2(H \delta_\lambda^\alpha + b_\lambda^\alpha) \frac{\partial u^\lambda}{\partial \xi} + K u^\alpha \right) + \rho u^\beta \nabla_\beta^* u^\alpha + \\ & a^{\alpha\beta} \nabla_\beta^* \left(p - \frac{\mu}{3} \operatorname{div} \mathbf{u} \right) - 2\rho a^{\alpha\beta} \varepsilon_{\beta\lambda} u^\lambda \omega^3 = F^\alpha, \end{aligned} \quad (16a)$$

$$\begin{aligned} & -\mu \left(\frac{\partial^2 u^3}{\partial \xi^2} - 2H \frac{\partial u^3}{\partial \xi} \right) + \frac{\partial}{\partial \xi} \left(p - \frac{\mu}{3} \operatorname{div} \mathbf{u} \right) \Big|_{\xi=0} - 2\rho \varepsilon_{\alpha\beta} \omega^\alpha u^\beta - \\ & 2\mu \left(\frac{4}{3} u^\alpha \nabla_\beta^* H + b_\beta^\alpha \nabla_\alpha^* u^\beta \right) + \rho b_{\alpha\beta} u^\alpha u^\beta = F^3, \end{aligned} \quad (16b)$$

$$\operatorname{div}(\rho \mathbf{u}) + \frac{\partial(\rho \mathbf{u})^3}{\partial \xi} = 0, \quad (16c)$$

$$(\mathbf{u} \cdot \nabla) s = \frac{1}{|\mathbf{u}|^2 T \rho} \left(\kappa \left(\Delta T + \frac{\partial^2 T}{\partial \xi^2} - 2H \frac{\partial T}{\partial \xi} \right) + \Phi_0 \right), \quad (16d)$$

其中 ω^3 为角速度向量在半测地坐标系下的第 3 分量,

$$\Phi_0 = 2\mu a^{\alpha\lambda} a^{\beta\sigma} e_{\alpha\beta}^* e_{\lambda\sigma}^* + \frac{1}{2} \mu a_{\alpha\beta} \frac{\partial u^\alpha}{\partial \xi} \frac{\partial u^\beta}{\partial \xi} - \frac{2}{3} \mu \left(\operatorname{div} \mathbf{u} + \frac{\partial u^3}{\partial \xi} \right)^2.$$

关于曲面上算子的交换性质,我们有下面的结论(参见文献[5]).

引理 2

$$\operatorname{rot}(\Delta \mathbf{u} + K \mathbf{u}) = \Delta \operatorname{rot} \mathbf{u}; \quad \operatorname{rot}((\mathbf{u} \cdot \nabla) \mathbf{u}) = (\mathbf{u} \cdot \nabla) \operatorname{rot} \mathbf{u} + \varepsilon_{\alpha\beta}^* \nabla^\alpha u^\lambda \nabla_\lambda u^\beta. \quad (17)$$

利用在 S 上 $\sigma^{33} = -\tau H$, 并定义函数 b 为

$$u^\alpha \frac{\partial \ln b}{\partial x^\alpha} = \frac{\partial u^3}{\partial x^3}, \quad \text{在 } S \text{ 上.} \quad (18)$$

注1 b 的物理意义是相邻流面之间的相对厚度^[4-5].

最终我们可得

定理2 流面 S 上的 Navier-Stokes 方程(16)可以表示为

$$-\mu \overset{*}{\Delta} \overset{*}{\text{rot}} \mathbf{u} + \rho (\mathbf{u} \cdot \overset{*}{\nabla}) \overset{*}{\text{rot}} \mathbf{u} + \rho \varepsilon_{\alpha\beta} \overset{*}{\nabla}^\alpha u^\lambda \overset{*}{\nabla}_\lambda u^\beta + \varepsilon_{\alpha\beta} (\mathbf{u} \cdot \overset{*}{\nabla}) u^\beta \overset{*}{\nabla}^\alpha \rho + 2 \overset{*}{\nabla}_\lambda (\rho \omega^3 u^\lambda) = \overset{*}{\text{rot}} \left(F - \mu \frac{\partial^2 u^\alpha}{\partial \xi^2} + 2(H\delta_\lambda^\alpha + b_\lambda^\alpha) \frac{\partial u^\lambda}{\partial \xi} \right), \quad (19a)$$

$$\mu \left(\frac{\partial^2 u^3}{\partial \xi^2} + \left(2H + \frac{\partial \ln \rho}{\partial \xi} \right) \frac{\partial u^3}{\partial \xi} \right) = F^3 - \tau \frac{\partial H}{\partial \xi} - \rho b_{\alpha\beta} u^\alpha u^\beta + 2\rho \varepsilon_{\alpha\beta} \omega^\alpha u^\beta + 2\mu (u^\beta \overset{*}{\nabla}_\beta H + b_\beta^\alpha \overset{*}{\nabla}_\alpha u^\beta) - \frac{\partial u^\alpha}{\partial \xi} \overset{*}{\nabla}_\alpha \ln \rho - u^\alpha \overset{*}{\nabla}_\alpha \frac{\partial \ln \rho}{\partial \xi}, \quad (19b)$$

$$\text{div}(\mathbf{b}\rho\mathbf{u}) = 0, \quad (19c)$$

$$-\kappa \left(\overset{*}{\Delta} T + \frac{\partial^2 T}{\partial \xi^2} - 2H \frac{\partial T}{\partial \xi} \right) + C_\nu \rho u^\alpha \overset{*}{\nabla}_\alpha T + p \left(\text{div} \mathbf{u} + \frac{\partial u^3}{\partial \xi} \right) - 2\mu \overset{*}{e}^{\alpha\beta}(\mathbf{u}) \overset{*}{e}_{\alpha\beta}(\mathbf{u}) - \frac{1}{2} \mu a^{\alpha\beta} \frac{\partial u^\alpha}{\partial \xi} \frac{\partial u^\beta}{\partial \xi} + \frac{2}{3} \mu \left(\text{div} \mathbf{u} + \frac{\partial u^3}{\partial \xi} \right)^2 = 0. \quad (19d)$$

2 速度图方法和流函数满足的速度图方程

在本节中对于位势流动,我们定义流面 S 上的流函数 Ψ 和位势函数 Φ , 并得出了流函数满足的方程.

2.1 流面上的流函数和位势函数

由(19c)式,我们可以定义满足以下关系的流函数

$$\mathbf{b}\rho\mathbf{u}^\beta = \varepsilon^{\beta\alpha} \overset{*}{\nabla}_\alpha \Psi, \quad \overset{*}{\nabla}_\alpha \Psi = \mathbf{b}\rho \varepsilon_{\beta\alpha} u^\beta, \quad (20)$$

其中 $\varepsilon_{\beta\alpha}$ 为 S 上的行列式张量,定义见(3)式.

另外,如果流动是位势流动,可以定义位势函数 Φ :

$$\mathbf{u} = \text{grad} \Phi \text{ 或 } u_i = \frac{\partial \Phi}{\partial x^i}, \quad u^i = g^{ij} \frac{\partial \Phi}{\partial x^j}.$$

由于 S 是流面,可知在 S 上, $u^3 = u_3 = 0$, 因此

$$u_\alpha = \frac{\partial \Phi}{\partial x^\alpha}, \quad u^\alpha = a^{\alpha\beta} u_\beta = a^{\alpha\beta} \frac{\partial \Phi}{\partial x^\beta}. \quad (21)$$

S 上的速度向量、流函数和位势函数有下面的关系式:

$$u^\alpha = a^{\alpha\beta} \overset{*}{\nabla}_\beta \Phi, \quad \overset{*}{\nabla}_\alpha \Phi = a_{\alpha\beta} u^\beta; \quad u^\alpha = \frac{1}{\mathbf{b}\rho} \varepsilon^{\alpha\beta} \overset{*}{\nabla}_\beta \Psi, \quad \overset{*}{\nabla}_\alpha \Psi = \mathbf{b}\rho \varepsilon_{\beta\alpha} u^\beta. \quad (22)$$

2.2 流函数满足的速度图方程

首先引入速度图变量 (V, Θ) , 其中 V 是速度向量 \mathbf{u} 的模, Θ 是速度向量 \mathbf{u} 与流面上第一基向量 \mathbf{e}_1 的夹角, 即

$$V = \sqrt{a_{\alpha\beta} u^\alpha u^\beta}, \quad V \cos \Theta = \sqrt{a_{11}} u^1.$$

改变换的行列式为 $\hat{J} = \partial(V, \Theta) / \partial(x^1, x^2)$.

我们先给出本文的主要定理如下:

定理3 设速度图变换 Jacobi 行列式 \hat{J} 非奇异, 那么流面上流函数 Ψ 满足速度图方程:

$$A_{\Theta\Theta} \frac{\partial^2 \Psi}{\partial V^2} + A_{V\Theta} \frac{\partial^2 \Psi}{\partial \Theta^2} - (A_{V\Theta} + A_{\Theta V}) \frac{\partial^2 \Psi}{\partial V \partial \Theta} + \left(\frac{A_{\Theta\Theta}}{\partial V} - \frac{\partial A_{V\Theta}}{\partial \Theta} \right) \frac{\partial \Psi}{\partial V} + \left(\frac{A_{V\Theta}}{\partial \Theta} - \frac{\partial A_{\Theta V}}{\partial V} \right) \frac{\partial \Psi}{\partial \Theta} = 0, \quad (23)$$

其系数在后面的(33)式中定义,即

$$A_{\xi\eta} = \frac{1}{Q\sqrt{a}} \varepsilon_{\alpha\beta} \frac{\partial}{\partial \xi} (D_\rho u^\beta) \frac{\partial}{\partial \eta} (D_1 \varepsilon_\gamma^{\cdot\alpha} u^\gamma), \quad \xi, \eta = V \text{ 或 } \Theta,$$

以及 $D = b\rho\sqrt{a}V^2$, $D_1 = \frac{\sqrt{a}}{D}$, $D_\rho = D_1 b\rho = \frac{1}{V^2}$.

为证明定理3,我们需要用到下面的几个引理.

引理3 流面 S 上的流函数和位势函数 (Ψ, Φ) 在 Gauss 坐标系 $x = (x^1, x^2)$ 下满足方程

$$\frac{\partial x^\sigma}{\partial u^\beta} = \frac{1}{b\rho V^2} (b\rho \delta_\alpha^\sigma \Phi_\beta + \varepsilon_\alpha^{\cdot\sigma} \Psi_\beta) u^\alpha. \quad (24)$$

证明 由(22)式有

$$\begin{cases} \mathbf{d}\Phi = \nabla_\alpha \Phi \mathbf{d}x^\alpha = a_{\alpha\beta} u^\beta \mathbf{d}x^\alpha, \\ \mathbf{d}\Psi = \nabla_\alpha \Psi \mathbf{d}x^\alpha = b\rho \varepsilon_{\beta\alpha} u^\beta \mathbf{d}x^\alpha. \end{cases} \quad (25)$$

该方程组的系数矩阵对应的行列式为

$$D = \begin{vmatrix} a_{1\beta} u^\beta & a_{2\beta} u^\beta \\ b\rho \varepsilon_{\beta 1} u^\beta & b\rho \varepsilon_{\beta 2} u^\beta \end{vmatrix} = b\rho \varepsilon_{12} a_{\alpha\beta} u^\alpha u^\beta = b\rho \sqrt{a} V^2,$$

其中 $V^2 = a_{\alpha\beta} u^\alpha u^\beta = |\mathbf{u}|^2$, 从而有

$$\mathbf{d}x^1 = \frac{1}{D} \begin{vmatrix} \mathbf{d}\Phi & a_{2\beta} u^\beta \\ \mathbf{d}\Psi & b\rho \varepsilon_{\beta 2} u^\beta \end{vmatrix} = \frac{1}{D} (b\rho \varepsilon_{\beta 2} u^\beta \mathbf{d}\Phi - a_{2\beta} u^\beta \mathbf{d}\Psi), \quad (26a)$$

$$\mathbf{d}x^2 = \frac{1}{D} \begin{vmatrix} a_{1\beta} u^\beta & \mathbf{d}\Phi \\ b\rho \varepsilon_{\beta 1} u^\beta & \mathbf{d}\Psi \end{vmatrix} = \frac{1}{D} (a_{1\beta} u^\beta \mathbf{d}\Psi - b\rho \varepsilon_{\beta 1} u^\beta \mathbf{d}\Phi). \quad (26b)$$

另外将 Φ 和 Ψ 看作 u^1 和 u^2 的函数,并定义

$$\Phi_\alpha = \frac{\partial \Phi}{\partial u^\alpha}, \quad \Psi_\alpha = \frac{\partial \Psi}{\partial u^\alpha},$$

我们有

$$\begin{cases} \mathbf{d}x^1 = -\frac{1}{D} (b\rho \varepsilon_{2\alpha} \Phi_\beta + a_{2\alpha} \Psi_\beta) u^\alpha \mathbf{d}u^\beta, \\ \mathbf{d}x^2 = \frac{1}{D} (b\rho \varepsilon_{1\alpha} \Phi_\beta + a_{1\alpha} \Psi_\beta) u^\alpha \mathbf{d}u^\beta. \end{cases} \quad (27)$$

利用 $\varepsilon_{\alpha\beta}$ 和 $\varepsilon^{\alpha\beta}$, 则有

$$\mathbf{d}x^\sigma = (\sqrt{a}/D) (b\rho \delta_\alpha^\sigma \Phi_\beta + a_{\lambda\alpha} \varepsilon^{\lambda\sigma} \Psi_\beta) u^\alpha \mathbf{d}u^\beta.$$

定义循环张量 $\varepsilon_\alpha^{\cdot\sigma} = a_{\alpha\lambda} \varepsilon^{\lambda\sigma}$, 最终可得

$$\frac{\partial x^\sigma}{\partial u^\beta} = \frac{1}{b\rho V^2} (b\rho \delta_\alpha^\sigma \Phi_\beta + \varepsilon_\alpha^{\cdot\sigma} \Psi_\beta) u^\alpha.$$

证毕. □

引理4 由(20)式所定义的流函数 Ψ 满足方程

$$\frac{\partial}{\partial u^\alpha} \left(m^{\alpha\beta} \frac{\partial}{\partial u^\beta} \Psi \right) = 0, \quad (28)$$

其中

$$m^{\alpha\beta} = \frac{\sqrt{a}}{D_2} \varepsilon^{\alpha\lambda} \varepsilon^{\beta\sigma} \varepsilon_{\nu\mu} \frac{\partial}{\partial u^\lambda} (D_\rho u^\nu) \frac{\partial}{\partial u^\sigma} (D_1 \varepsilon_\gamma^{\cdot\nu} u^\gamma).$$

证明 从引理 3 的结果和二阶导数的可交换性

$$\frac{\partial^2 x^\sigma}{\partial u^\beta \partial u^\lambda} = \frac{\partial^2 x^\sigma}{\partial u^\lambda \partial u^\beta},$$

可得

$$\frac{\partial}{\partial u^\lambda} (D_1 b \rho \delta_\alpha^\sigma u^\alpha \Phi_\beta + D_1 \varepsilon_\alpha^{\cdot\sigma} u^\alpha \Psi_\beta) = \frac{\partial}{\partial u^\beta} (D_1 b \rho \delta_\alpha^\sigma u^\alpha \Phi_\lambda + D_1 \varepsilon_\alpha^{\cdot\sigma} u^\alpha \Psi_\lambda),$$

即

$$\begin{aligned} & \frac{\partial}{\partial u^\lambda} (D_1 b \rho \delta_\alpha^\sigma u^\alpha) \Phi_\beta - \frac{\partial}{\partial u^\beta} (D_1 b \rho \delta_\alpha^\sigma u^\alpha) \Phi_\lambda = \\ & \frac{\partial}{\partial u^\beta} (D_1 \varepsilon_\alpha^{\cdot\sigma} u^\alpha) \Psi_\lambda - \frac{\partial}{\partial u^\lambda} (D_1 \varepsilon_\alpha^{\cdot\sigma} u^\alpha) \Psi_\beta \end{aligned}$$

或

$$\frac{\partial}{\partial u^2} (D_1 b \rho u^\sigma) \Phi_1 - \frac{\partial}{\partial u^1} (D_1 b \rho u^\sigma) \Phi_2 = \frac{\partial}{\partial u^1} (D_1 \varepsilon_\alpha^{\cdot\sigma} u^\alpha) \Psi_2 - \frac{\partial}{\partial u^2} (D_1 \varepsilon_\alpha^{\cdot\sigma} u^\alpha) \Psi_1. \quad (29)$$

记 $D_\rho = D_1 b \rho = 1/V^2$ 并令

$$\begin{aligned} D_2 = & \begin{vmatrix} \frac{\partial}{\partial u^2} (D_\rho u^1) & -\frac{\partial}{\partial u^1} (D_\rho u^1) \\ \frac{\partial}{\partial u^2} (D_\rho u^2) & -\frac{\partial}{\partial u^1} (D_\rho u^2) \end{vmatrix} = \\ & \frac{\partial}{\partial u^1} (D_\rho u^1) \frac{\partial}{\partial u^2} (D_\rho u^2) - \frac{\partial}{\partial u^1} (D_\rho u^2) \frac{\partial}{\partial u^2} (D_\rho u^1). \end{aligned} \quad (30)$$

则由(29)式,我们可以用 Ψ_α 来表示 Φ_α :

$$\begin{aligned} \Phi_1 = & \frac{1}{D_2} \left(\left[\frac{\partial}{\partial u^1} (D_\rho u^2) \frac{\partial}{\partial u^2} (D_1 \varepsilon_\alpha^{\cdot 1} u^\alpha) - \frac{\partial}{\partial u^1} (D_\rho u^1) \frac{\partial}{\partial u^2} (D_1 \varepsilon_\alpha^{\cdot 2} u^\alpha) \right] \Psi_1 + \right. \\ & \left. \left[\frac{\partial}{\partial u^1} (D_\rho u^1) \frac{\partial}{\partial u^1} (D_1 \varepsilon_\alpha^{\cdot 2} u^\alpha) - \frac{\partial}{\partial u^1} (D_\rho u^2) \frac{\partial}{\partial u^1} (D_1 \varepsilon_\alpha^{\cdot 1} u^\alpha) \right] \Psi_2 \right), \\ \Phi_2 = & \frac{1}{D_2} \left(\left[\frac{\partial}{\partial u^2} (D_\rho u^2) \frac{\partial}{\partial u^2} (D_1 \varepsilon_\alpha^{\cdot 1} u^\alpha) - \frac{\partial}{\partial u^2} (D_\rho u^1) \frac{\partial}{\partial u^2} (D_1 \varepsilon_\alpha^{\cdot 2} u^\alpha) \right] \Psi_1 + \right. \\ & \left. \left[\frac{\partial}{\partial u^2} (D_\rho u^1) \frac{\partial}{\partial u^1} (D_1 \varepsilon_\alpha^{\cdot 2} u^\alpha) - \frac{\partial}{\partial u^2} (D_\rho u^2) \frac{\partial}{\partial u^1} (D_1 \varepsilon_\alpha^{\cdot 1} u^\alpha) \right] \Psi_2 \right). \end{aligned}$$

从而根据 $\Phi_{12} = \Phi_{21}$, 有

$$\frac{\partial}{\partial u^\alpha} \left(m^{\alpha\beta} \frac{\partial}{\partial u^\beta} \Psi \right) = 0,$$

其中

$$m^{\alpha\beta} = \frac{\sqrt{a}}{D_2} \varepsilon^{\alpha\lambda} \varepsilon^{\beta\sigma} \varepsilon_{\nu\mu} \frac{\partial}{\partial u^\lambda} (D_\rho u^\mu) \frac{\partial}{\partial u^\sigma} (D_1 \varepsilon_\gamma^{\cdot\nu} u^\gamma). \quad \square \quad (31)$$

定理 3 的证明 由速度图变换公式, (30) 式可改写为

$$D_2 = \frac{\partial(D_\rho u^1, D_\rho u^2)}{\partial(u^1, u^2)} = J \frac{\partial(D_\rho u^1, D_\rho u^2)}{\partial(V, \Theta)} = JQ,$$

其中

$$J = \frac{\partial(V, \Theta)}{\partial(u^1, u^2)}, \quad Q = \frac{\partial(D_\rho u^1, D_\rho u^2)}{\partial(V, \Theta)}.$$

从而, (31) 式转化为

$$m^{\alpha\beta} = \frac{a}{J} \varepsilon^{\alpha\lambda} \varepsilon^{\beta\sigma} \left(A_{V\lambda} \frac{\partial V}{\partial u^\lambda} \frac{\partial V}{\partial u^\sigma} + A_{V\Theta} \frac{\partial V}{\partial u^\lambda} \frac{\partial \Theta}{\partial u^\sigma} + A_{\Theta V} \frac{\partial \Theta}{\partial u^\lambda} \frac{\partial V}{\partial u^\sigma} + A_{\Theta\Theta} \frac{\partial \Theta}{\partial u^\lambda} \frac{\partial \Theta}{\partial u^\sigma} \right), \quad (32)$$

其中

$$A_{\xi\eta} = \frac{1}{Q\sqrt{a}} \varepsilon^{\alpha\beta} \frac{\partial}{\partial \xi} (D_\rho u^\beta) \frac{\partial}{\partial \eta} (D_1 \varepsilon_\gamma^{\alpha} u^\gamma), \quad \xi, \eta = V \text{ 或 } \Theta. \quad (33)$$

而(28)式变为

$$A \frac{\partial^2 \Psi}{\partial V^2} + B \frac{\partial^2 \Psi}{\partial V \partial \Theta} + C \frac{\partial^2 \Psi}{\partial \Theta^2} + E \frac{\partial \Psi}{\partial V} + F \frac{\partial \Psi}{\partial \Theta} = 0, \quad (34)$$

其中

$$\begin{cases} A = m^{\alpha\beta} \frac{\partial V}{\partial u^\alpha} \frac{\partial V}{\partial u^\beta}, & B = m^{\alpha\beta} \left(\frac{\partial V}{\partial u^\alpha} \frac{\partial \Theta}{\partial u^\beta} + \frac{\partial \Theta}{\partial u^\alpha} \frac{\partial V}{\partial u^\beta} \right), & C = m^{\alpha\beta} \frac{\partial \Theta}{\partial u^\alpha} \frac{\partial \Theta}{\partial u^\beta}, \\ E = \frac{\partial}{\partial V} \left(m^{\alpha\beta} \frac{\partial V}{\partial u^\beta} \right) \frac{\partial V}{\partial u^\alpha} + \frac{\partial}{\partial \Theta} \left(m^{\alpha\beta} \frac{\partial V}{\partial u^\beta} \right) \frac{\partial \Theta}{\partial u^\alpha}, \\ F = \frac{\partial}{\partial V} \left(m^{\alpha\beta} \frac{\partial \Theta}{\partial u^\beta} \right) \frac{\partial V}{\partial u^\alpha} + \frac{\partial}{\partial \Theta} \left(m^{\alpha\beta} \frac{\partial \Theta}{\partial u^\beta} \right) \frac{\partial \Theta}{\partial u^\alpha}. \end{cases} \quad (35)$$

易证

$$\begin{cases} \sqrt{a} \varepsilon^{\alpha\beta} \frac{\partial V}{\partial u^\alpha} \frac{\partial V}{\partial u^\beta} = 0, & \sqrt{a} \varepsilon^{\alpha\beta} \frac{\partial V}{\partial u^\alpha} \frac{\partial \Theta}{\partial u^\beta} = J, & \sqrt{a} \varepsilon^{\alpha\beta} \frac{\partial \Theta}{\partial u^\alpha} \frac{\partial V}{\partial u^\beta} = -J, \\ \sqrt{a} \varepsilon^{\alpha\beta} \frac{\partial \Theta}{\partial u^\alpha} \frac{\partial \Theta}{\partial u^\beta} = 0, & \frac{\partial}{\partial u^\alpha} (\sqrt{a} \varepsilon^{\alpha\lambda} \frac{\partial V}{\partial u^\lambda}) = 0, & \frac{\partial}{\partial u^\alpha} (\sqrt{a} \varepsilon^{\alpha\lambda} \frac{\partial \Theta}{\partial u^\lambda}) = 0. \end{cases} \quad (36)$$

通过计算可知

$$\begin{cases} m^{\alpha\beta} \frac{\partial V}{\partial u^\beta} = \sqrt{a} \varepsilon^{\alpha\lambda} \left(A_{V\Theta} \frac{\partial V}{\partial u^\lambda} + A_{\Theta\Theta} \frac{\partial \Theta}{\partial u^\lambda} \right), \\ m^{\alpha\beta} \frac{\partial \Theta}{\partial u^\beta} = -\sqrt{a} \varepsilon^{\alpha\lambda} \left(A_{V\lambda} \frac{\partial V}{\partial u^\lambda} + A_{\Theta V} \frac{\partial \Theta}{\partial u^\lambda} \right), \end{cases} \quad (37)$$

从而

$$\begin{cases} A = JA_{\Theta\Theta}, & B = -J(A_{\Theta V} + A_{V\Theta}), & C = JA_{V\lambda}, \\ E = J \left(\frac{\partial A_{\Theta\Theta}}{\partial V} - \frac{\partial A_{V\Theta}}{\partial \Theta} \right), & F = J \left(\frac{\partial A_{V\lambda}}{\partial \Theta} - \frac{\partial A_{\Theta V}}{\partial V} \right). \end{cases} \quad (38)$$

(34) 式为

$$A_{\Theta\Theta} \frac{\partial^2 \Psi}{\partial V^2} - (A_{V\Theta} + A_{\Theta V}) \frac{\partial^2 \Psi}{\partial V \partial \Theta} + A_{V\lambda} \frac{\partial^2 \Psi}{\partial \Theta^2} + \left(\frac{\partial A_{\Theta\Theta}}{\partial V} - \frac{\partial A_{V\Theta}}{\partial \Theta} \right) \frac{\partial \Psi}{\partial V} + \left(\frac{\partial A_{V\lambda}}{\partial \Theta} - \frac{\partial A_{\Theta V}}{\partial V} \right) \frac{\partial \Psi}{\partial \Theta} = 0.$$

证毕. □

以下的定理将对定理 3 中得到的二阶速度图方程进行分类.

定理 4 速度图方程(23)对应的特征方程和特征根分别为

$$\lambda^2 - (A_{VV} + A_{\theta\theta})\lambda + A_{VV}A_{\theta\theta} - \frac{(A_{V\theta} + A_{\theta V})^2}{4} = 0$$

和

$$\lambda_{1,2} = \frac{A_{VV} + A_{\theta\theta} \pm \sqrt{(A_{VV} - A_{\theta\theta})^2 + (A_{V\theta} + A_{\theta V})^2}}{2}.$$

证明 方程(23)的特征矩阵为

$$\begin{pmatrix} A_{VV} & -\frac{A_{V\theta} + A_{\theta V}}{2} \\ -\frac{A_{V\theta} + A_{\theta V}}{2} & A_{\theta\theta} \end{pmatrix},$$

从而特征方程为

$$\begin{vmatrix} A_{VV} - \lambda & -\frac{A_{V\theta} + A_{\theta V}}{2} \\ -\frac{A_{V\theta} + A_{\theta V}}{2} & A_{\theta\theta} - \lambda \end{vmatrix} = (A_{VV} - \lambda)(A_{\theta\theta} - \lambda) - \frac{(A_{V\theta} + A_{\theta V})^2}{4} =$$

$$\lambda^2 - (A_{VV} + A_{\theta\theta})\lambda + A_{VV}A_{\theta\theta} - \frac{(A_{V\theta} + A_{\theta V})^2}{4} = 0.$$

相应的判别式为

$$\Delta = (A_{VV} + A_{\theta\theta})^2 - 4\left(A_{VV}A_{\theta\theta} - \frac{(A_{V\theta} + A_{\theta V})^2}{4}\right) =$$

$$(A_{VV} - A_{\theta\theta})^2 + (A_{V\theta} + A_{\theta V})^2 \geq 0.$$

从而可以得到结论,所有的特征根都是实数,其值分别为

$$\lambda_{1,2} = \frac{A_{VV} + A_{\theta\theta} \pm \sqrt{(A_{VV} - A_{\theta\theta})^2 + (A_{V\theta} + A_{\theta V})^2}}{2}. \quad \square$$

另外,我们有

$$\lambda_1\lambda_2 = A_{VV}A_{\theta\theta} - \frac{(A_{V\theta} + A_{\theta V})^2}{4}.$$

从二阶偏微分方程的经典理论可以得出,方程(23)当 $\lambda_1\lambda_2 > 0$ 时是椭圆的,当 $\lambda_1\lambda_2 < 0$ 时是双曲的. 而 $\{\lambda_1\lambda_2 = 0\}$ 是两种类型的分离线.

注 2 特别地,对于平面或柱面流动,我们知道 $\lambda_1\lambda_2 = V^2(1 - Ma^2)$,从而 $\lambda_1\lambda_2 = 0$ 当且仅当 Mach 数 $Ma = 1$.

一种特殊但最重要的情况, S 上的 Gauss 坐标系选为正交曲线坐标系时,即度量张量有如下的形式:

$$a_{12} = a_{21} = 0, a^{12} = a^{21} = 0, a^{11} = \frac{1}{a_{11}}, a^{22} = \frac{1}{a_{22}}, a = a_{11}a_{22}.$$

设速度 \mathbf{u} 的物理分量为 u, v , 我们有

$$u^1 = \frac{u}{\sqrt{a_{11}}}, u^2 = \frac{v}{\sqrt{a_{22}}}, u_1 = \sqrt{a_{11}}u, u_2 = \sqrt{a_{22}}v. \quad (39)$$

另一方面, 由于

$$u = V\cos\Theta, v = V\sin\Theta \text{ 及 } V^2 = u^2 + v^2,$$

因此

$$u_1 = \sqrt{a_{11}}V\cos\Theta, u_2 = \sqrt{a_{22}}V\sin\Theta, u^1 = \frac{V\cos\Theta}{\sqrt{a_{11}}}, u^2 = \frac{V\sin\Theta}{\sqrt{a_{22}}}. \quad (40)$$

注意到

$$\begin{cases} D_\rho = \frac{1}{V^2}, D_\rho u^1 = \frac{\cos\Theta}{V\sqrt{a_{11}}}, D_\rho u^2 = \frac{\sin\Theta}{V\sqrt{a_{22}}}, \\ D_1 \varepsilon_\alpha^{-1} u^\alpha = -\frac{u_2}{D} = -\frac{\sin\Theta}{b\rho V\sqrt{a_{11}}}, D_1 \varepsilon_\alpha^{-2} u^\alpha = \frac{u_1}{D} = \frac{\cos\Theta}{b\rho V\sqrt{a_{22}}}, \end{cases}$$

因此(33)式为

$$\begin{aligned} A_{\xi\eta} = & -\frac{1}{Q} \left[\frac{\partial}{\partial\xi} \left(\frac{\cos\Theta}{V\sqrt{a_{11}}} \right) \frac{\partial}{\partial\eta} \left(\frac{\cos\Theta}{b\rho V\sqrt{a_{22}}} \right) + \right. \\ & \left. \frac{\partial}{\partial\xi} \left(\frac{\sin\Theta}{V\sqrt{a_{22}}} \right) \frac{\partial}{\partial\eta} \left(\frac{\sin\Theta}{b\rho V\sqrt{a_{11}}} \right) \right], \quad \xi, \eta = V \text{ 或 } \Theta, \end{aligned} \quad (41)$$

其中

$$\begin{aligned} Q = & \frac{\partial(D_\rho u^1, D_\rho u^2)}{\partial(V, \Theta)} = \partial \left(\frac{\cos\Theta}{V\sqrt{a_{11}}}, \frac{\sin\Theta}{V\sqrt{a_{22}}} \right) / \partial(V, \Theta) = \\ & -\frac{1}{V^3\sqrt{a}} + \frac{\sin(2\Theta)}{2V^2\sqrt{a}} \left(\frac{\partial}{\partial V} \ln\sqrt{a_{11}} - \frac{\partial}{\partial\Theta} \ln\sqrt{a_{22}} - \frac{\partial}{\partial V} \ln\sqrt{a_{22}} - \frac{\partial}{\partial\Theta} \ln\sqrt{a_{11}} \right) + \\ & \frac{\sin(2\Theta)}{2V^3\sqrt{a}} \frac{\partial}{\partial\Theta} \ln\sqrt{a_{22}} - \frac{\cos^2\Theta}{V^2\sqrt{a}} \frac{\partial}{\partial V} \ln\sqrt{a_{11}} - \frac{\sin^2\Theta}{V^2\sqrt{a}} \frac{\partial}{\partial V} \ln\sqrt{a_{22}}. \end{aligned} \quad (42)$$

这说明速度图方程(34)仅依赖流面 S 的度量张量 $(a_{\alpha\beta})$ 。

3 一些特殊流动实例

我们考虑可压缩位势流动问题. 假设流体是理想气体, 我们知道有关系式

$$\left(\frac{\rho_0}{\rho} \right)^2 = 1 + \frac{V^2}{c_0^2} \text{ 及 } \rho^2 c^2 = \rho_0^2 c_0^2,$$

其中 c_0 和 ρ_0 分别为滞止音速和密度, c 为当地音速. 从而有

$$\frac{\partial\rho}{\partial V} = -\frac{\rho V}{c^2}, \frac{\partial\rho}{\partial\Theta} = 0. \quad (43)$$

例 1 平面流动情形, 在直角坐标系下我们有

$$a_{11} = a^{11} = a_{22} = a^{22} = 1, a = 1, b = 1.$$

从而由(41)和(42)式可以得出

$$\begin{cases} Q = -\frac{1}{V^3}, A_{Vv} = V^3 \left(\frac{1}{\rho V^4} - \frac{1}{V^3} \frac{\partial}{\partial V} \frac{1}{\rho} \right), \\ A_{\Theta\Theta} = \frac{V}{\rho}, A_{V\Theta} = -\frac{\partial}{\partial\Theta} \frac{1}{\rho}, A_{\Theta v} = 0. \end{cases} \quad (44)$$

另外,由(43)式

$$A_{Vv} = \frac{1 - Ma^2}{\rho V}, A_{v\theta} = 0, \quad (45)$$

其中 $Ma = V/c$ 为 Mach 数. 由(43)至(45)式,有

$$\frac{\partial A_{\theta\theta}}{\partial V} = \frac{1}{\rho} - \frac{V}{\rho^2} \frac{\partial \rho}{\partial V} = \frac{1 + Ma^2}{\rho}, \frac{\partial A_{Vv}}{\partial \Theta} = 0. \quad (46)$$

从而速度图方程(23)为

$$V^2 \frac{\partial^2 \psi}{\partial V^2} + (1 - Ma^2) \frac{\partial^2 \psi}{\partial \Theta^2} + V(1 + Ma^2) \frac{\partial \psi}{\partial V} = 0, \quad (47)$$

这和经典结果是一致的.

例 2 当流面 S 是半径为 $r = R_0$ 的圆柱面时,取 $\mathbf{y} = (r, \phi, z)$ 为 R^3 中的圆柱坐标系,度量张量为

$$(\tilde{g}_{ij}) = \begin{pmatrix} 1 & 0 & 0 \\ 0 & r^2 & 0 \\ 0 & 0 & 1 \end{pmatrix}.$$

在圆柱面上,取 $x^1 = \phi, x^2 = z$, 并根据公式

$$a_{\alpha\beta} = \tilde{g}_{ij} \frac{\partial y^i}{\partial x^\alpha} \frac{\partial y^j}{\partial x^\beta}, \quad (48)$$

我们知道在 S 上

$$a_{11} = R_0^2, a_{22} = 1, a_{12} = a_{21} = 0, a = R_0^2. \quad (49)$$

因此由(41)和(42)式有

$$Q = -\frac{1}{V^3 R_0}, b = 1,$$

$$A_{Vv} = V^3 R_0 \left[\frac{\partial}{\partial V} \left(\frac{\cos \Theta}{VR_0} \right) \frac{\partial}{\partial V} \left(\frac{\cos \Theta}{b\rho V} \right) + \frac{\partial}{\partial V} \left(\frac{\sin \Theta}{V} \right) \frac{\partial}{\partial V} \left(\frac{\sin \Theta}{b\rho VR_0} \right) \right] = \frac{1 - Ma^2}{\rho V},$$

$$A_{\theta\theta} = V^3 R_0 \left[\frac{\partial}{\partial \Theta} \left(\frac{\cos \Theta}{VR_0} \right) \frac{\partial}{\partial \Theta} \left(\frac{\cos \Theta}{b\rho V} \right) + \frac{\partial}{\partial \Theta} \left(\frac{\sin \Theta}{V} \right) \frac{\partial}{\partial \Theta} \left(\frac{\sin \Theta}{b\rho VR_0} \right) \right] = \frac{V}{\rho},$$

$$A_{v\theta} = A_{\theta v} = 0.$$

从而速度图方程和(46)式相同.

例 3 流面是半径为 $r = R_0$ 的球面,取 $\mathbf{y} = (r, \theta, \phi)$ 为 R^3 中的球极坐标系,其度量张量为

$$(\tilde{g}_{ij}) = \begin{pmatrix} 1 & 0 & 0 \\ 0 & r^2 & 0 \\ 0 & 0 & r^2 \cos^2 \theta \end{pmatrix}.$$

在球面 S 上,取球面坐标 $x^1 = \theta, x^2 = \phi$ ($\theta \in (-\pi/2, \pi/2], \phi \in (-\pi, \pi]$), 由关系式(48)有

$$a_{11} = R_0^2, a_{22} = R_0^2 \cos^2 \theta, a_{12} = a_{21} = 0, a = R_0^4 \cos^2 \theta. \quad (50)$$

从而由(41)和(42)式可以得到

$$Q = -\frac{1}{V^3 R_0^2 \cos \theta} \left(1 - \frac{1}{2} \sin(2\Theta) \frac{\partial}{\partial \Theta} \ln(\cos \theta) + V \sin^2 \Theta \frac{\partial}{\partial V} \ln(R_0 \cos \theta) \right), b = 1,$$

$$A_{Vv} = -\frac{1}{Q} \left[\frac{\partial}{\partial V} \left(\frac{\cos \Theta}{VR_0} \right) \frac{\partial}{\partial V} \left(\frac{\cos \Theta}{b\rho VR_0 \cos \theta} \right) + \frac{\partial}{\partial V} \left(\frac{\sin \Theta}{VR_0 \cos \theta} \right) \frac{\partial}{\partial V} \left(\frac{\sin \Theta}{b\rho VR_0} \right) \right] =$$

$$\begin{aligned}
& - \frac{1}{Q\rho V^4 R_0^2 \cos\theta} \left(1 - Ma^2 + V \frac{\partial}{\partial V} \ln(\cos\theta) - VMa^2 \sin^2\Theta \frac{\partial}{\partial V} \ln(\cos\theta) \right), \\
A_{\theta\theta} = & - \frac{1}{Q} \left[\frac{\partial}{\partial\Theta} \left(\frac{\cos\Theta}{VR_0} \right) \frac{\partial}{\partial\Theta} \left(\frac{\cos\Theta}{b\rho VR_0 \cos\theta} \right) + \frac{\partial}{\partial\Theta} \left(\frac{\sin\Theta}{VR_0 \cos\theta} \right) \frac{\partial}{\partial\Theta} \left(\frac{\sin\Theta}{b\rho VR_0} \right) \right] = \\
& - \frac{1}{Q\rho V^2 R_0^2 \cos\theta}, \\
A_{V\theta} = & - \frac{1}{Q} \left[\frac{\partial}{\partial V} \left(\frac{\cos\Theta}{VR_0} \right) \frac{\partial}{\partial\Theta} \left(\frac{\cos\Theta}{b\rho VR_0 \cos\theta} \right) + \frac{\partial}{\partial V} \left(\frac{\sin\Theta}{VR_0 \cos\theta} \right) \frac{\partial}{\partial\Theta} \left(\frac{\sin\Theta}{b\rho VR_0} \right) \right] = \\
& - \frac{1}{Q\rho V^3 R_0^2 \cos\theta} \left(\cos^2\Theta \frac{\partial}{\partial\Theta} \ln(\cos\theta) - \frac{1}{2} V \sin(2\Theta) \frac{\partial}{\partial V} \ln(\cos\theta) \right), \\
A_{\theta V} = & - \frac{1}{Q} \left[\frac{\partial}{\partial\Theta} \left(\frac{\cos\Theta}{VR_0} \right) \frac{\partial}{\partial V} \left(\frac{\cos\Theta}{b\rho VR_0 \cos\theta} \right) + \frac{\partial}{\partial\Theta} \left(\frac{\sin\Theta}{VR_0 \cos\theta} \right) \frac{\partial}{\partial V} \left(\frac{\sin\Theta}{b\rho VR_0} \right) \right] = \\
& - \frac{1}{Q\rho V^3 R_0^2 \cos\theta} \left(\frac{1}{2} V \sin(2\Theta) \frac{\partial}{\partial V} \ln(\cos\theta) + (1 - Ma^2) \sin^2\Theta \frac{\partial}{\partial\Theta} \ln(\cos\theta) \right).
\end{aligned}$$

例4 流面是回转面的情形,它在文献[9]中被 Wu(吴仲华)称为 S_1 流面. 设回转面 S 的旋转轴是 z 轴,生成曲线为 C ,其参数表示为

$$r = R(s), z = Z(s) = s,$$

其中 s 为 C 的弧长参数, C 的弧长为 $L, 0 \leq s \leq L, R(s) > 0$. 令 $x^1 = s, x^2 = \phi, x^3$ 是 S 上一点的经度, $\phi \in (0, 2\pi]$, 由(48)式,回转面 S 的度量张量为

$$\begin{aligned}
a_{11} &= R'(s)^2 + Z'(s)^2 = R'(s)^2 + 1, \quad a_{12} = a_{21} = 0, \\
a_{22} &= R(s)^2, \quad a = (R'(s)^2 + 1)R(s)^2.
\end{aligned}$$

从而(41)和(42)式给出

$$\begin{aligned}
Q = & - \frac{1}{V^3 R(s) \sqrt{R'(s)^2 + 1}} \left[1 - \frac{1}{2} V \sin(2\Theta) \left(\frac{\partial}{\partial V} \ln \sqrt{R'(s)^2 + 1} + \frac{\partial}{\partial\Theta} \ln R(s) - \right. \right. \\
& \left. \frac{\partial}{\partial V} \ln R(s) \frac{\partial}{\partial\Theta} \ln \sqrt{R'(s)^2 + 1} \right) - \frac{1}{2} \sin(2\Theta) \frac{\partial}{\partial\Theta} \ln \frac{R(s)}{\sqrt{R'(s)^2 + 1}} + \\
& \left. V \cos^2\Theta \frac{\partial}{\partial V} \ln \sqrt{R'(s)^2 + 1} + V \sin^2\Theta \frac{\partial}{\partial V} \ln R(s) \right],
\end{aligned}$$

$$b = 1,$$

$$\begin{aligned}
A_{VV} = & - \frac{1}{Q} \left[\frac{\partial}{\partial V} \left(\frac{\cos\Theta}{V \sqrt{R'(s)^2 + 1}} \right) \frac{\partial}{\partial V} \left(\frac{\cos\Theta}{b\rho VR(s)} \right) + \frac{\partial}{\partial V} \left(\frac{\sin\Theta}{VR(s)} \right) \frac{\partial}{\partial V} \left(\frac{\sin\Theta}{b\rho V \sqrt{R'(s)^2 + 1}} \right) \right] = \\
& - \frac{1}{Q\rho V^4 R(s) \sqrt{R'(s)^2 + 1}} \left(1 - Ma^2 + V \frac{\partial}{\partial V} \ln R(s) + V \frac{\partial}{\partial V} \ln \sqrt{R'(s)^2 + 1} - \right. \\
& \left. V Ma^2 \cos^2\Theta \frac{\partial}{\partial V} \ln \sqrt{R'(s)^2 + 1} - V Ma^2 \sin^2\Theta \frac{\partial}{\partial V} \ln R(s) + \right. \\
& \left. V^2 \frac{\partial}{\partial V} \ln R(s) \frac{\partial}{\partial V} \ln \sqrt{R'(s)^2 + 1} \right), \\
A_{\theta\theta} = & - \frac{1}{Q} \left[\frac{\partial}{\partial\Theta} \left(\frac{\cos\Theta}{V \sqrt{R'(s)^2 + 1}} \right) \frac{\partial}{\partial\Theta} \left(\frac{\cos\Theta}{b\rho VR(s)} \right) + \frac{\partial}{\partial\Theta} \left(\frac{\sin\Theta}{VR(s)} \right) \frac{\partial}{\partial\Theta} \left(\frac{\sin\Theta}{b\rho V \sqrt{R'(s)^2 + 1}} \right) \right] = \\
& \frac{1}{Q\rho V^2 R(s) \sqrt{R'(s)^2 + 1}} \left(1 + \frac{\partial}{\partial V} \ln R(s) \frac{\partial}{\partial V} \ln \sqrt{R'(s)^2 + 1} \right),
\end{aligned}$$

$$\begin{aligned}
 A_{v\theta} = & -\frac{1}{Q} \left[\frac{\partial}{\partial V} \left(\frac{\cos\Theta}{V\sqrt{R'(s)^2 + 1}} \right) \frac{\partial}{\partial\Theta} \left(\frac{\cos\Theta}{b\rho VR(s)} \right) + \frac{\partial}{\partial V} \left(\frac{\sin\Theta}{VR(s)} \right) \frac{\partial}{\partial\Theta} \left(\frac{\sin\Theta}{b\rho V\sqrt{R'(s)^2 + 1}} \right) \right] = \\
 & \frac{1}{Q\rho V^3 R(s) \sqrt{R'(s)^2 + 1}} \left(\cos^2\Theta \frac{\partial}{\partial V} \ln R(s) + \sin^2\Theta \frac{\partial}{\partial V} \ln \sqrt{R'(s)^2 + 1} + \right. \\
 & \left. \frac{1}{2} V \sin(2\Theta) \frac{\partial}{\partial V} \ln \sqrt{R'(s)^2 + 1} - \frac{1}{2} V \sin(2\Theta) \frac{\partial}{\partial V} \ln R(s) + \right. \\
 & \left. V \cos^2\Theta \frac{\partial}{\partial V} \ln \sqrt{R'(s)^2 + 1} \frac{\partial}{\partial\Theta} \ln R(s) + V \sin^2\Theta \frac{\partial}{\partial V} \ln R(s) \frac{\partial}{\partial\Theta} \ln \sqrt{R'(s)^2 + 1} \right), \\
 A_{\theta v} = & -\frac{1}{Q} \left[\frac{\partial}{\partial\Theta} \left(\frac{\cos\Theta}{V\sqrt{R'(s)^2 + 1}} \right) \frac{\partial}{\partial V} \left(\frac{\cos\Theta}{b\rho VR(s)} \right) + \frac{\partial}{\partial\Theta} \left(\frac{\sin\Theta}{VR(s)} \right) \frac{\partial}{\partial V} \left(\frac{\sin\Theta}{b\rho V\sqrt{R'(s)^2 + 1}} \right) \right] = \\
 & \frac{1}{Q\rho V^3 R(s) \sqrt{R'(s)^2 + 1}} \left(\frac{1}{2} V \sin(2\Theta) \frac{\partial}{\partial V} \ln R(s) - \frac{1}{2} V \sin(2\Theta) \frac{\partial}{\partial V} \ln \sqrt{R'(s)^2 + 1} + \right. \\
 & \left. (1 - Ma^2) \cos^2\Theta \frac{\partial}{\partial\Theta} \ln \sqrt{R'(s)^2 + 1} + (1 - Ma^2) \sin^2\Theta \frac{\partial}{\partial\Theta} \ln R(s) + \right. \\
 & \left. V \cos^2\Theta \frac{\partial}{\partial\Theta} \ln \sqrt{R'(s)^2 + 1} \frac{\partial}{\partial V} \ln R(s) + V \sin^2\Theta \frac{\partial}{\partial\Theta} \ln R(s) \frac{\partial}{\partial V} \ln \sqrt{R'(s)^2 + 1} \right).
 \end{aligned}$$

例5 螺旋面情形,在直角坐标系下其参数表示是

$$y^1 = r \cos(\omega_1 t), \quad y^2 = r \sin(\omega_1 t), \quad y^3 = \omega_2 t,$$

其中, $0 \leq r \leq R_0, 0 < t \leq 2\pi, \omega_1, \omega_2 > 0$. 令 $x^1 = r, x^2 = t$, 由(48)式有

$$a_{11} = 1, \quad a_{22} = \omega_1^2 r^2 + t^2, \quad a_{12} = a_{21} = 0, \quad a = \omega_1^2 r^2 + t^2.$$

从而根据(41)和(42)式可以得到

$$\begin{aligned}
 Q = & -\frac{1}{V^3 \sqrt{\omega_1^2 r^2 + t^2}} \left(1 - \frac{1}{2} \sin(2\Theta) \frac{\partial}{\partial\Theta} \ln \sqrt{\omega_1^2 r^2 + t^2} + V \sin^2\Theta \frac{\partial}{\partial V} \ln \sqrt{\omega_1^2 r^2 + t^2} \right), \\
 b = & 1, \\
 A_{wv} = & -\frac{1}{Q} \left[\frac{\partial}{\partial V} \left(\frac{\cos\Theta}{V} \right) \frac{\partial}{\partial V} \left(\frac{\cos\Theta}{b\rho V \sqrt{\omega_1^2 r^2 + t^2}} \right) + \frac{\partial}{\partial V} \left(\frac{\sin\Theta}{V \sqrt{\omega_1^2 r^2 + t^2}} \right) \frac{\partial}{\partial V} \left(\frac{\sin\Theta}{b\rho V} \right) \right] = \\
 & -\frac{1}{Q\rho V^4 \sqrt{\omega_1^2 r^2 + t^2}} \left(1 - Ma^2 + V \frac{\partial}{\partial V} \ln \sqrt{\omega_1^2 r^2 + t^2} - VMa^2 \sin^2\Theta \frac{\partial}{\partial V} \ln \sqrt{\omega_1^2 r^2 + t^2} \right), \\
 A_{\theta\theta} = & -\frac{1}{Q} \left[\frac{\partial}{\partial\Theta} \left(\frac{\cos\Theta}{V} \right) \frac{\partial}{\partial\Theta} \left(\frac{\cos\Theta}{b\rho V \sqrt{\omega_1^2 r^2 + t^2}} \right) + \frac{\partial}{\partial\Theta} \left(\frac{\sin\Theta}{V \sqrt{\omega_1^2 r^2 + t^2}} \right) \frac{\partial}{\partial\Theta} \left(\frac{\sin\Theta}{b\rho V} \right) \right] = \\
 & -\frac{1}{Q\rho V^2 \sqrt{\omega_1^2 r^2 + t^2}}, \\
 A_{v\theta} = & -\frac{1}{Q} \left[\frac{\partial}{\partial V} \left(\frac{\cos\Theta}{V} \right) \frac{\partial}{\partial\Theta} \left(\frac{\cos\Theta}{b\rho V \sqrt{\omega_1^2 r^2 + t^2}} \right) + \frac{\partial}{\partial V} \left(\frac{\sin\Theta}{V \sqrt{\omega_1^2 r^2 + t^2}} \right) \frac{\partial}{\partial\Theta} \left(\frac{\sin\Theta}{b\rho V} \right) \right] = \\
 & -\frac{1}{Q\rho V^3 \sqrt{\omega_1^2 r^2 + t^2}} \left(\cos^2\Theta \frac{\partial}{\partial\Theta} \ln \sqrt{\omega_1^2 r^2 + t^2} - \frac{V \sin(2\Theta)}{2} \frac{\partial}{\partial V} \ln \sqrt{\omega_1^2 r^2 + t^2} \right), \\
 A_{\theta v} = & -\frac{1}{Q} \left[\frac{\partial}{\partial\Theta} \left(\frac{\cos\Theta}{V} \right) \frac{\partial}{\partial V} \left(\frac{\cos\Theta}{b\rho V \sqrt{\omega_1^2 r^2 + t^2}} \right) + \frac{\partial}{\partial\Theta} \left(\frac{\sin\Theta}{V \sqrt{\omega_1^2 r^2 + t^2}} \right) \frac{\partial}{\partial V} \left(\frac{\sin\Theta}{b\rho V} \right) \right] = \\
 & -\frac{1}{Q\rho V^3 \sqrt{\omega_1^2 r^2 + t^2}} \left(\frac{1}{2} V \sin(2\Theta) \frac{\partial}{\partial V} \ln \sqrt{\omega_1^2 r^2 + t^2} + \right.
 \end{aligned}$$

$$(1 - Ma^2) \sin^2 \Theta \frac{\partial}{\partial \Theta} \ln \sqrt{\omega_1^2 r^2 + t^2}.$$

致谢 作者在此感谢编辑和审稿人,感谢他们对稿件的认真阅读以及帮助改进稿件的宝贵意见。

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Hodograph Method of Flow on Two-Dimensional Manifold

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Abstract: For some special flow, especially the potential flow in the plane, there are obvious advantages using the tool of hodograph method. For the realistic flow, there exists stream surface, namely, two-dimensional manifold, on which the velocity vector of the flow lies its tangent space. By introducing the stream function and potential function, the hodograph method for potential flow on a surface was established with the help of tensor analysis, which provided a kind of analysis method. For the derived hodograph equation, the characteristic equation and its characteristic roots were also derived, from which the type of the hodograph equation of the second order can be classified. Moreover, some examples for special surfaces were given.

Key words: hodograph method; potential flow; stream surface; stream function; potential function