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具有收缩表面的二阶流体驻点流动的级数解*

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摘要: 研究具有收缩表面的边界层流动的解析解. 通过相似变换, 将偏微分方程简化为可用同伦分析法(HAM)求解的常微分方程. 然后讨论了具有收缩表面的二维轴对称流动.

关 键 词: 驻点流动; 二阶流体; 收缩平面; 同伦分析法

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引言

由于非 Newton 流体在工程和工业领域的广泛应用, 人们对其研究的兴趣日益增加. 至今为止提出了多种非 Newton 流体的模型, 其中对二阶流体模型的研究最多^[1-15]. 另外在塑料片材的空气动力挤压、玻璃纤维、造纸和高分子片材制造等领域, 非 Newton 流体的边界层流动有着重要作用. 在 Sakiadis^[16] 前期研究的基础上, 许多作者对延伸表面上的边界层流动进行了讨论^[17-24]. 现有文献表明, 研究收缩表面上的边界层流动^[25-30]还不多.

本文在考虑了热传递效应的同时, 对收缩表面上二阶流体的驻点流动进行了研究. 同伦分析法是求解非线性问题的强有力的工具, 本文应用同伦分析法^[31-45]给出了二维问题和轴对称问题的级数解, 并求得级数解的收敛性. 给出了图形结果并进行了讨论.

1 公式的建立

考虑收缩表面上不可压缩二阶流体的二维驻点流动. x, y, z 轴上的速度分量分别用 u, v, w 表示. 假设无限远处驻点流动速度为 $u = ax, w = -az$. 延伸(收缩)表面上驻点流动速度为 $u = b(x + c), w = 0$. 其中 $b > 0$ 为延伸率($b < 0$ 为收缩率), $-c$ 为延伸原点位置. 流体流动和传热控制方程^[30, 46]如下:

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0, \quad (1)$$

$$u \frac{\partial u}{\partial x} + w \frac{\partial u}{\partial z} = -\frac{1}{\rho} \frac{\partial p}{\partial x} + v \frac{\partial^2 u}{\partial z^2} + \frac{\alpha_1}{\rho} \left[u \frac{\partial^3 u}{\partial x \partial z^2} + \frac{\partial u}{\partial x} \frac{\partial^2 u}{\partial z^2} + \frac{\partial u}{\partial z} \frac{\partial^2 u}{\partial x \partial z} + w \frac{\partial^3 u}{\partial z^3} \right], \quad (2)$$

$$\rho c_p \left[u \frac{\partial T}{\partial x} + w \frac{\partial T}{\partial z} \right] = k \cdot \cdot \cdot ^2 T, \quad (3)$$

其中, $\nu = \mu/\rho$ 为动黏度, ρ 为密度, α_1 为二阶参数, c_p 为比热比, T 为温度, $k (> 0)$ 为热传导系

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数, 方程忽略了耗散项.

2 二维驻点流动

定义^[30]

$$\eta = \sqrt{(a/N)} z, \quad u = axf'(\eta) + bch(\eta), \quad v = 0, \quad w = -\sqrt{a/N}f(\eta), \quad (4)$$

$$\theta = (T - T_\infty) / (T_0 - T_\infty). \quad (5)$$

方程(1)恒满足, 通过方程(2)和(3)成为

$$f_{\eta\eta}^{\circledast} + ff_{\eta\eta}^{\circledast} + f_{\eta}^{\circledast} + \beta(2ff_{\eta\eta}^{\circledast} + f_{\eta\eta}^{\circledast} - ff_{\eta\eta}^{\circledast}) = 0, \quad (6)$$

$$h_{\eta\eta}^{\circledast} + fh_{\eta\eta}^{\circledast} - f_{\eta\eta}^{\circledast} + \beta(hf_{\eta\eta}^{\circledast} + f_{\eta\eta}^{\circledast} + f_{\eta\eta}^{\circledast} - fh_{\eta\eta}^{\circledast}) = 0, \quad (7)$$

$$\theta_{\eta\eta}^{\circledast} + Pr\theta_{\eta\eta}^{\circledast} = 0, \quad (8)$$

其中 $\beta = \alpha_1 a / (\rho V)$.

相应的边界条件为

$$\begin{cases} f(0) = 0, & f'(0) = b/a = \alpha, \\ f'(\infty) = 1, & h(0) = 1, \\ h(\infty) = 0, & \theta(\infty) = 0 \end{cases} \quad (9)$$

式中的上撇号表示对 η 求导, 且 $Pr = N/k$.

2.1 收缩表面上二维驻点流动的解

以下求解收缩表面上二阶流体驻点流动. 为了用 HAM 求解, 我们选择以下初始近似值和辅助的线性算子:

$$f_{01}(\eta) = (1 - \alpha)(e^{-\eta} - 1) + \eta, \quad (10)$$

$$h_{01}(\eta) = e^{-\eta}, \quad (11)$$

$$\theta_{01}(\eta) = e^{-\eta}, \quad (12)$$

$$\mathcal{L}_{01}[\hat{f}(\eta; p)] = \frac{\partial^3 \hat{f}(\eta; p)}{\partial \eta^3} + \frac{\partial^2 \hat{f}(\eta; p)}{\partial \eta^2}, \quad (13)$$

$$\mathcal{L}_{02}[\hat{h}(\eta; p)] = \frac{\partial^2 \hat{h}(\eta; p)}{\partial \eta^2} + \frac{\partial \hat{h}(\eta; p)}{\partial \eta}, \quad (14)$$

$$\mathcal{L}_{03}[\hat{\theta}(\eta; p)] = \frac{\partial^2 \hat{\theta}(\eta; p)}{\partial \eta^2} + \frac{\partial \hat{\theta}(\eta; p)}{\partial \eta}, \quad (15)$$

式中下标01表示第 1 种情况, 其他情况亦同. 辅助的线性算子具有属性:

$$\mathcal{L}_{01}[C_1 + C_2 \eta + C_3 e^{-\eta}] = 0, \quad (16)$$

$$\mathcal{L}_{02}[C_4 + C_5 e^{-\eta}] = 0, \quad (17)$$

$$\mathcal{L}_{03}[C_6 + C_7 e^{-\eta}] = 0, \quad (18)$$

其中 C_i ($i = 1, 2, \dots, 7$) 为任意常数. 如果 $p \in [0, 1]$ 为一个嵌入参数, E_i ($i = 1, 2, 3$) 为非零的辅助参数, 则 0 阶和 m 阶变形问题如下:

0 阶变形问题

$$(1-p)\mathcal{L}_{01}[\hat{f}(\eta; p) - f_{01}(\eta)] = pE_1\mathcal{N}_1[\hat{f}(\eta; p)], \quad (19)$$

$$(1-p)\mathcal{L}_{02}[\hat{h}(\eta; p) - h_{01}(\eta)] = pE_2\mathcal{N}_2[\hat{h}(\eta; p), \hat{f}(\eta; p)], \quad (20)$$

$$(1-p)\mathcal{L}_{03}[\hat{\theta}(\eta; p) - \theta_{01}(\eta)] = pE_3\mathcal{N}_3[\hat{\theta}(\eta; p), \hat{f}(\eta; p)], \quad (21)$$

$$\hat{f}(0; p) = 0, \quad \hat{f}'(0; p) = \alpha, \quad \hat{f}'(\infty; p) = 1, \quad (22)$$

$$\hat{h}(0; p) = 1, \quad \hat{h}'(\infty; p) = 0, \quad (23)$$

$$\hat{\theta}(0; p) = 1, \quad \hat{\theta}'(\infty; p) = 0, \quad (24)$$

$$\mathcal{N}_1[\hat{f}(\eta; p)] = \frac{\partial^3 \hat{f}(\eta; p)}{\partial \eta^3} + \hat{f}'(\eta; p) \frac{\partial^2 \hat{f}(\eta; p)}{\partial \eta^2} - \left[\frac{\partial \hat{f}(\eta; p)}{\partial \eta} \right]^2 + 1 +$$

$$\beta \left[2 \frac{\partial \hat{f}(\eta; p)}{\partial \eta} \frac{\partial^3 \hat{f}(\eta; p)}{\partial \eta^3} + \left(\frac{\partial^2 \hat{f}(\eta; p)}{\partial \eta^2} \right)^2 - \hat{f}(\eta; p) \frac{\partial^4 \hat{f}(\eta; p)}{\partial \eta^4} \right], \quad (25)$$

$$\begin{aligned} \mathcal{N}_2 [\hat{f}(\eta; p), \hat{h}(\eta; p)] &= \frac{\partial^2 \hat{h}(\eta; p)}{\partial \eta^2} + \hat{f}(\eta; p) \frac{\partial \hat{h}(\eta; p)}{\partial \eta} - \hat{h}(\eta; p) \frac{\partial \hat{f}(\eta; p)}{\partial \eta} + \\ &\quad \beta \left[\hat{h}(\eta; p) \frac{\partial^3 \hat{f}(\eta; p)}{\partial \eta^3} + \frac{\partial \hat{f}(\eta; p)}{\partial \eta} \frac{\partial^2 \hat{h}(\eta; p)}{\partial \eta^2} \right] + \\ &\quad \beta \left[\frac{\partial^2 \hat{f}(\eta; p)}{\partial \eta^2} \frac{\partial \hat{h}(\eta; p)}{\partial \eta} - \hat{f}(\eta; p) \frac{\partial^3 \hat{h}(\eta; p)}{\partial \eta^3} \right], \end{aligned} \quad (26)$$

$$\mathcal{N}_3 [\hat{\theta}(\eta; p), \hat{f}(\eta; p)] = \frac{\partial^2 \hat{\theta}(\eta; p)}{\partial \eta^2} + Pr \hat{f}(\eta; p) \frac{\partial \hat{\theta}(\eta; p)}{\partial \eta}, \quad (27)$$

m 阶变形问题

$$\mathcal{L}_{01} [f_m(\eta) - X_m f_{m-1}(\eta)] = E_1 \mathcal{R}_{lm}(\eta), \quad (28)$$

$$\mathcal{L}_{02} [h_m(\eta) - X_m h_{m-1}(\eta)] = E_2 \mathcal{R}_{2m}(\eta), \quad (29)$$

$$\mathcal{L}_{03} [\theta_m(\eta) - X_m \theta_{m-1}(\eta)] = E_3 \mathcal{R}_{3m}(\eta), \quad (30)$$

$$\begin{cases} f_m(0) = 0 & f'_m(0) = 0 & f''_m(\infty) = 0 \\ h_m(0) = 0 & h'_m(\infty) = 0 & \theta_m(0) = 0 & \theta'_m(\infty) = 0 \end{cases} \quad (31)$$

$$\begin{aligned} \mathcal{R}_{lm}(\eta) &= f_{m-1}^\odot(\eta) + (1 - X_m) + \sum_{k=0}^{m-1} [f_{m-1-k} f'_k - f'_{m-1-k} f''_k] + \\ &\quad \beta \sum_{k=0}^{m-1} [2f'_{m-1-k} f_k^\odot + f''_{m-1-k} f''_k - f_{m-1-k} f''_k], \end{aligned} \quad (32)$$

$$\begin{aligned} \mathcal{R}_{2m}(\eta) &= h''_{m-1}(\eta) + \sum_{k=0}^{m-1} [h'_{m-1-k} f'_k - h_{m-1-k} f''_k] + \\ &\quad \beta \sum_{k=0}^{m-1} [h_{m-1-k} f_k^\odot + f'_{m-1-k} h''_k + h'_{m-1-k} f''_k - f''_{m-1-k} h''_k], \end{aligned} \quad (33)$$

$$\mathcal{R}_{3m}(\eta) = \theta''_{m-1}(\eta) + Pr \sum_{k=0}^{m-1} \theta'_{m-1-k} f'_k, \quad (34)$$

$$X_m = \begin{cases} 0 & m \leq 1 \\ 1 & m > 1 \end{cases} \quad (35)$$

通过 MATHEMATICA 符号计算软件, 可以得到方程 (28) ~ (30) 的前几阶近似解. 得到 f, h, θ 的解

$$f(\eta) = \sum_{m=0}^{\infty} f_m(\eta) = \lim_{M \rightarrow \infty} \left[\sum_{m=0}^M a_{m,0}^0 + \sum_{n=1}^{M+1} e^{-(n+1)\eta} \left(\sum_{m=n-1}^M \sum_{k=1}^{2n-1} a_{m,n}^k \eta^k \right) \right], \quad (36)$$

$$h(\eta) = \sum_{m=0}^{\infty} h_m(\eta) = \lim_{M \rightarrow \infty} \left[\sum_{n=1}^{M+1} e^{-(n+1)\eta} \left(\sum_{m=n-1}^M \sum_{k=0}^{2n-1} c_{m,n}^k \eta^k \right) \right], \quad (37)$$

$$\theta(\eta) = \sum_{m=0}^{\infty} \theta_m(\eta) = \lim_{M \rightarrow \infty} \left[\sum_{n=1}^{M+1} e^{-(n+1)\eta} \left(\sum_{m=n-1}^M \sum_{k=0}^{2n-1} b_{m,n}^k \eta^k \right) \right], \quad (38)$$

3 轴对称收缩表面上的轴对称驻点流动

通过变换^[30]

$$\begin{cases} \eta(x, y) = \sqrt{(a\mathcal{N})} z & u = axg'(\eta) + bcl(\eta), \quad v = ayg'(\eta), \\ w = -2\sqrt{a\mathcal{N}}g(\eta), \quad \theta = (T - T_\infty)/(T_0 - T_\infty), \end{cases} \quad (39)$$

由方程 (2) 和 (3) 得到

$$g^{\circ} + 2gg' - g'^2 + 1 + \beta(2g'g^{\circ} + g''^2 - 2gg') = 0, \quad (40)$$

$$\dot{l} + 2g\dot{l} - g'l + \beta(lg^{\circ} + g'l + g'\dot{l} - 2g\dot{l}) = 0, \quad (41)$$

$$\ddot{\theta} + 2Pr g \dot{\theta} = 0, \quad (42)$$

相应的边界条件^[30]为

$$\begin{cases} g(0) = 0 & g'(0) = b/a = \alpha \\ g'(\infty) = 1 & l(0) = 1 \\ l(\infty) = 0 & \theta(\infty) = 0 \end{cases} \quad (43)$$

采用前小节的推导过程, 得到轴对称收缩表面上的轴对称驻点流动解:

$$g(\eta) = \sum_{m=0}^{\infty} g_m(\eta) = \lim_{M \rightarrow \infty} \left[\sum_{m=0}^M a_{m,0} + \sum_{n=1}^{2M+1} e^{-(n+1)\eta} \left(\sum_{m=n-1}^{2M} \sum_{k=0}^{2n+1-n} a_{m,n}^k \eta^k \right) \right], \quad (44)$$

$$l(\eta) = \sum_{m=0}^{\infty} l_m(\eta) = \lim_{M \rightarrow \infty} \left[\sum_{n=1}^{2M+1} e^{-(n+1)\eta} \left(\sum_{m=n-1}^{2M} \sum_{k=0}^{2n+1-n} c_{m,n}^k \eta^k \right) \right], \quad (45)$$

$$\theta(\eta) = \sum_{m=0}^{\infty} \theta_m(\eta) = \lim_{M \rightarrow \infty} \left[\sum_{n=1}^{2M+1} e^{-(n+1)\eta} \left(\sum_{m=n-1}^{2M} \sum_{k=0}^{2n+1-n} b_{m,n}^k \eta^k \right) \right]. \quad (46)$$

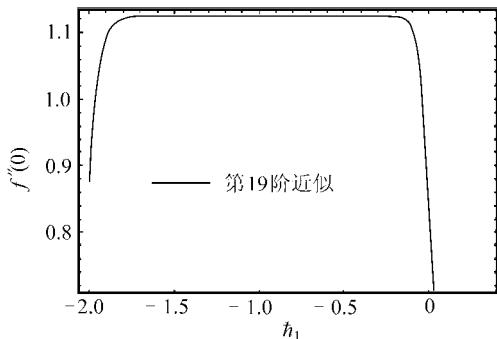


图 1 二维驻点流中 f' 的 E 曲线

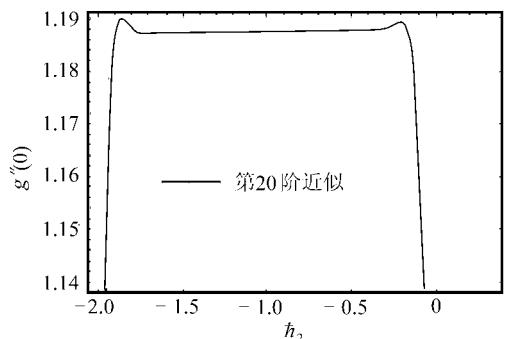


图 2 轴对称收缩表面上轴对称驻点流中 g 的 E 曲线

4 结果与讨论

通过方程 (36) ~ (38) 和方程 (44) ~ (46) 的计算, 得到两个问题的解析解, 包含非零的辅助参数 E_i ($i = 1, 2$), 调整该参数用来控制解的收敛性. E 曲线^[31] 定义为: 在 E 所有可能取值的有效区域内呈一条水平线段. 图 1 和图 2 分别给出了本文中第 19 阶和第 20 阶的 E 曲线, 从图中可以看出, E 值的允许范围分别为 $-1.8 \leq E_1 \leq -0.3$ 和 $-1.9 \leq E_2 \leq -0.3$.

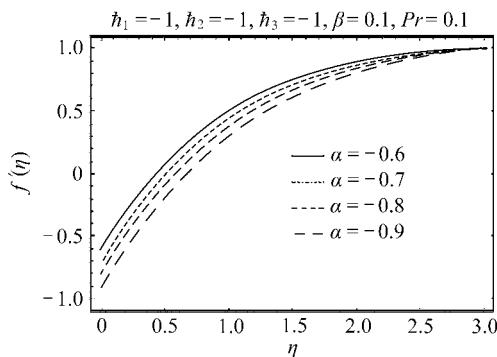


图 3 二维驻点流动中收缩参数 α 对 f' 的影响

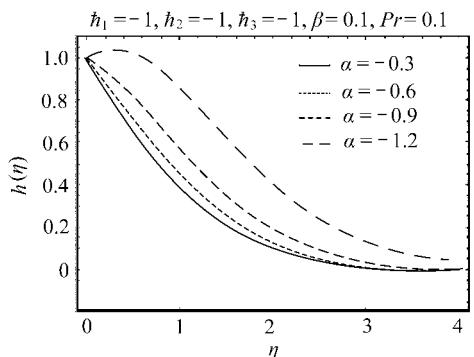


图 4 二维驻点流动中收缩参数 α 对 h 的影响

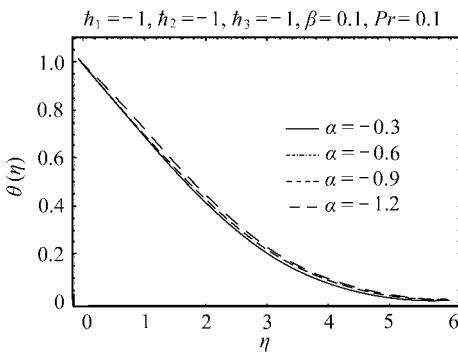
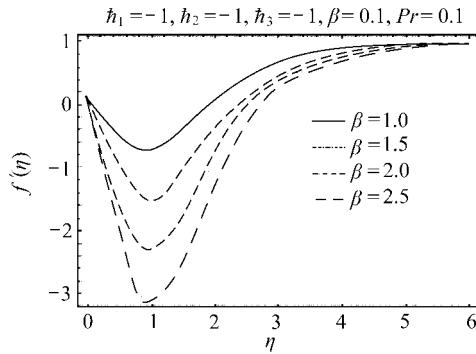
图 5 二维驻点流动中收缩参数 α 对 θ 的影响图 6 二维驻点流动中二阶参数 β 对 f' 的影响

图 3~图 7 给出了二维驻点流动的速度 f' , h 和温度 θ . 其中图 3~图 5 显示了不同收缩参数 $\alpha < 0$ 时, η 与无量纲速度 f' , h 和温度 θ 之间的关系. f' 随 α 的增大而减小, 而 h 和 θ 随 α 的增大而增大.

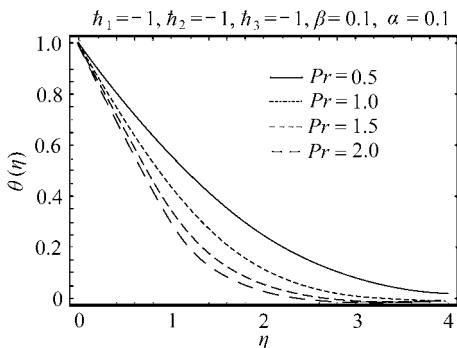
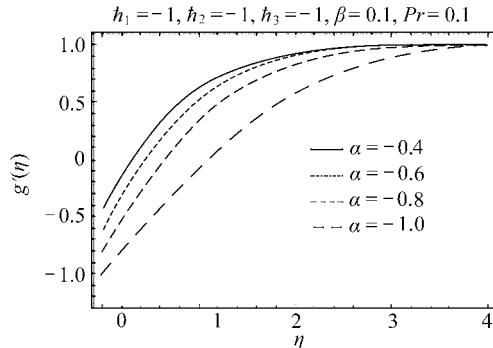
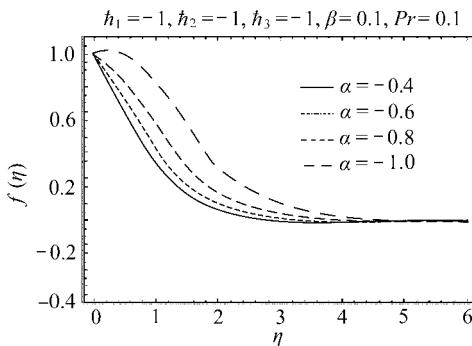
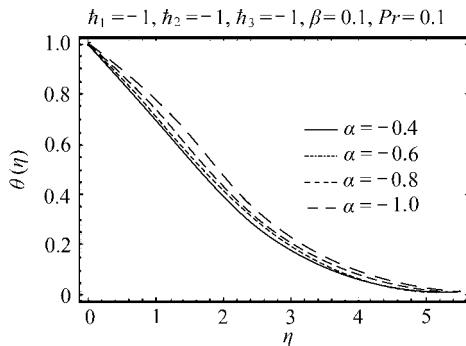
图 7 二维驻点流动中 Prandtl 数对 θ 的影响图 8 轴对称收缩表面上的轴对称驻点流动中收缩参数 α 对 g' 的影响

图 6 给出了二阶参数 β 对 f' 的影响, f' 随 β 的增大而减小; 图 7 给出了 Prandtl 数对 θ 的影响, θ 随 Prandtl 数的增大而减小.

图 8~图 10 给出了轴对称收缩表面上轴对称驻点流动时, 对于不同的 α , β 和 Pr 值, g' , l , θ 和 η 之间的关系. 从图中可以看出, g' 随收缩参数 α 的增大而增大, 而 l 和 θ 随 α 的增大而减小.

图 9 轴对称收缩表面上的轴对称驻点流动中收缩参数 α 对 l 的影响图 10 轴对称收缩表面上的轴对称驻点流动中收缩参数 α 对 θ 的影响

5 总 结

本文对收缩表面上二阶流体的驻点流动进行了研究. 通过应用同伦分析法, 得到二维驻点

流动和轴对称收缩表面两种情况的有效级数解，并给出了结果的收敛性。最后给出本文的图形结果，并分析了不同参数对结果的影响。从本文的分析可以看出，对于强非线性问题，同伦分析法对控制和调整问题的收敛区域，提供了一个简易的方法，该方法可应用于很多高度非线性的问题。

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Series Solutions for the Stagnation Flow of a Second Grade Fluid Over a Shrinking Sheet

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Abstract The analytic solutions of boundary layer flows bounded by a shrinking sheet are derived. Using similarity transformations the partial differential equations were reduced into the ordinary differential equations which were then solved by homotopy analysis method (HAM). Two-dimensional and axisymmetric shrinking flow cases were discussed.

Key words stagnation flow; second grade fluid; shrinking sheet; homotopy analysis method