

立方准晶压电材料的半空间问题*

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摘要: 考虑了立方准晶压电材料的半空间问题, 给出了反平面机械载荷和面内电载荷作用下立方准晶压电材料弹性问题的控制方程, 结合半无限区域表面边界条件, 利用算子理论和复变函数方法获得了立方准晶压电材料半空间问题一般解的表达式. 基于一般解得到了集中线力作用下, 半空间问题的声子场和相位子场的位移、应力以及电位移的解析表达式.

关键词: 立方准晶压电材料; 复变函数法; 半空间; 线性力

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The Half Space Problem of Cubic Quasicrystal Piezoelectric Materials

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Abstract: The half space problem of cubic quasicrystal piezoelectric materials was considered. The governing equations of elasticity for cubic quasicrystal piezoelectric materials under anti-plane deformation and in-plane electric field were given. Combined with the surface boundary conditions in the semi-infinite region, a general solution was obtained by means of the operator theory and the complex function method. Then the analytical expressions of the displacements and stresses of the phonon field and the phason field, and the electric displacements of the half space problem under concentrated linear surface forces, were derived.

Key words: cubic quasicrystal piezoelectric material; complex function method; half space; linear force

0 引言

1984 年, 以色列科学家 Shechtman 采用急速冷凝法研究 Al-Mn 合金时发现了准晶材料^[1], 其具有准周

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期的长程平移对称性和取向对称性,由于准晶材料特殊的物理性能,使其具有广泛的应用前景.Ding等^[2]建立了准晶线弹性理论.范天佑^[3]通过引入复变量或广义复变量,研究了若干准晶断裂力学问题.郭俊宏等^[4]构造保角映射,解决了一维六方准晶材料中含双裂纹的椭圆孔口反平面剪切问题.Li等^[5]研究了十八次对称准晶体的弹性问题.肖万伸等^[6]研究了一维六方准晶复合材料夹杂界面层中螺旋型位错与夹杂以及无限大基体的干涉效应.Wang等^[7]研究了均匀十次准晶材料裂纹尖端附近的弹性场.Zhang等^[8]研究了二维六方准晶材料半空间上的摩擦接触问题和半平面黏着接触问题.

压电效应是准晶材料重要的物理性质之一,在其应用中可能会遇到复杂的机电负载,因此研究准晶压电材料对外部施加载荷的响应非常重要.文献[9-10]发展了准晶压电材料的线弹性理论.Zhang等^[11]获得了一维正交压电准晶材料平面弹性问题的一般解.Li等^[12]采用算子理论方法获得了一维六方压电准晶的三维弹性问题的一般解.Fan等^[13]发展了含复杂缺陷一维六方压电准晶的间断有限元方法.白巧梅等^[14]利用复变函数方法得到了一维六方准晶压电材料裂纹尖端的应力分布和场强度因子的解析表达式.Li等^[15]研究了考虑热效应的一维六方压电准晶中的三维裂纹问题.刘兴伟等^[16]利用复变函数方法研究了一维六方压电准晶中正 n 边形孔边裂纹的反平面问题.Cheng等^[17]利用 Trefftz 方法研究了一维六方压电准晶反平面断裂问题.目前,关于三维准晶弹性问题的研究较少,然而实际应用中三维准晶材料的占比非常高.周旺民等^[18]考虑了立方准晶中的位错诱导弹性场.Gao等^[19]采用复变函数方法研究了含椭圆孔立方准晶断裂力学问题.Li等^[20]研究了三维二十面体准晶的 Stroh 形式,并将其应用于位错问题的研究.Long等^[21]研究了立方准晶圆盘的热弹性问题.三维准晶半空间问题的 Green 函数解是研究层合材料、界面问题等实际问题的理论基础,尚未看到有关研究.

本文研究了在反平面机械载荷和面内电载荷作用下立方准晶压电材料的半空间问题.首先给出了控制方程,然后采用复变函数方法,对半无限域区域表面边界条件进行积分,获得了立方准晶压电材料半空间问题的基本解.在此基础上,给出了集中线力作用下立方准晶压电材料半空间问题应力、位移的解析表达式.

1 立方准晶压电材料的基本方程

在空间直角坐标系下,立方准晶压电材料反平面问题的本构方程为^[22]

$$\begin{pmatrix} \sigma_{yz} \\ \sigma_{zx} \\ H_{yz} \\ H_{zx} \\ D_x \\ D_y \end{pmatrix} = \begin{pmatrix} C_{44} & 0 & R_3 & 0 & -e_{14} & 0 \\ 0 & C_{44} & 0 & R_3 & 0 & -e_{14} \\ R_3 & 0 & K_{44} & 0 & -d_{123} & 0 \\ 0 & R_3 & 0 & K_{44} & 0 & -d_{123} \\ e_{14} & 0 & d_{123} & 0 & \lambda_{11} & 0 \\ 0 & e_{14} & 0 & d_{123} & 0 & \lambda_{11} \end{pmatrix} \begin{pmatrix} 2\varepsilon_{yz} \\ 2\varepsilon_{zx} \\ 2\omega_{yz} \\ 2\omega_{zx} \\ E_x \\ E_y \end{pmatrix}, \quad (1)$$

其中 $\sigma_{ij}, \varepsilon_{ij}$ 分别表示声子场的应力、应变; H_{ij}, ω_{ij} 分别表示相位子场的应力、应变; D_i 表示电位移; E_i 表示电场强度; C_{44} 为声子场弹性常数; K_{44} 为相位子场弹性常数; R_3 为声子场与相位子场耦合常数; e_{14} 和 d_{123} 分别为声子场和相位子场压电常数; λ_{11} 为介电常数.

平衡方程为(不考虑体力的情况)

$$\sigma_{iz,i} = 0, H_{iz,i} = 0, D_{i,i} = 0, \quad i = x, y; \quad (2)$$

几何方程为

$$\begin{cases} \varepsilon_{yz} = \frac{1}{2} \frac{\partial u_z}{\partial y}, \varepsilon_{zx} = \frac{1}{2} \frac{\partial u_z}{\partial x}, \omega_{yz} = \frac{1}{2} \frac{\partial w_z}{\partial y}, \\ \omega_{zx} = \frac{1}{2} \frac{\partial w_z}{\partial x}, E_x = -\frac{\partial \Phi}{\partial x}, E_y = -\frac{\partial \Phi}{\partial y}, \end{cases} \quad (3)$$

其中 u_z 表示声子场位移, w_z 表示相位子场位移, Φ 表示电势.

由方程(1)–(3)可以获得由位移和电势表示的控制方程:

$$\begin{cases} C_{44}\nabla^2 u_z + R_3\nabla^2 w_z + 2e_{14}\frac{\partial^2\Phi}{\partial x\partial y} = 0, \\ R_3\nabla^2 u_z + K_{44}\nabla^2 w_z + 2d_{123}\frac{\partial^2\Phi}{\partial x\partial y} = 0, \\ 2e_{14}\frac{\partial^2 u_z}{\partial x\partial y} + 2d_{123}\frac{\partial^2 w_z}{\partial x\partial y} - \lambda_{11}\nabla^2\Phi = 0, \end{cases} \quad (4)$$

其中 $\nabla^2 = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2}$ 为 Laplace 算子. 这样, 立方准晶压电材料的反平面弹性问题就归结为在适当的边界条件下求解方程(4).

方程(4)可以改写为^[13]

$$\mathbf{A}\mathbf{U} = \mathbf{0}, \quad (5)$$

其中 $\mathbf{U} = (u_z, w_z, \Phi)^T$, \mathbf{A} 是微分算子矩阵,

$$\mathbf{A} = \begin{pmatrix} C_{44}\nabla^2 & R_3\nabla^2 & 2e_{14}\frac{\partial^2}{\partial x\partial y} \\ R_3\nabla^2 & K_{44}\nabla^2 & 2d_{123}\frac{\partial^2}{\partial x\partial y} \\ 2e_{14}\frac{\partial^2}{\partial x\partial y} & 2d_{123}\frac{\partial^2}{\partial x\partial y} & -\lambda_{11}\nabla^2 \end{pmatrix}. \quad (6)$$

由方程(6)可知 \mathbf{A} 的行列式为

$$|\mathbf{A}| = a\frac{\partial^6}{\partial y^6} + b\frac{\partial^2}{\partial x^2}\frac{\partial^4}{\partial y^4} + b\frac{\partial^4}{\partial x^4}\frac{\partial^2}{\partial y^2} + a\frac{\partial^6}{\partial x^6}, \quad (7)$$

其中 $a = \lambda_{11}(R_3^2 - C_{44}K_{44})$, $b = 4(2e_{14}d_{123}R_3 - d_{123}^2C_{44} - e_{14}^2K_{44}) + 3\lambda_{11}(R_3^2 - C_{44}K_{44})$.

下面我们引入位移函数 F , 其满足方程

$$\nabla_1^2\nabla_2^2\nabla_3^2F = 0, \quad (8)$$

其中 $\nabla_i^2 = \frac{\partial^2}{\partial x^2} + \frac{1}{t_i^2}\frac{\partial^2}{\partial y^2}$ ($i = 1, 2, 3$); t_i^2 ($i = 1, 2, 3$) 为方程 $at^6 - bt^4 + bt^2 - a = 0$ 的 3 个根.

根据算子理论, 方程(5)的一般解可表示为

$$u_z = A_{i1}F, w_z = A_{i2}F, \Phi = A_{i3}F, \quad i = 1, 2, 3. \quad (9)$$

取 $i = 2$, 由方程(6)可知 $|\mathbf{A}|$ 的代数余子式为

$$\begin{cases} A_{21} = \lambda_{11}R_3\frac{\partial^4}{\partial x^4} + 2(\lambda_{11}R_3 + 2e_{14}d_{123})\frac{\partial^4}{\partial x^2\partial y^2} + \lambda_{11}R_3\frac{\partial^4}{\partial y^4}, \\ A_{22} = -\lambda_{11}C_{44}\frac{\partial^4}{\partial x^4} - 2(\lambda_{11}C_{44} + 2e_{14}^2)\frac{\partial^4}{\partial x^2\partial y^2} - \lambda_{11}C_{44}\frac{\partial^4}{\partial y^4}, \\ A_{23} = 2(e_{14}R_3 - d_{123}C_{44})\left(\frac{\partial^4}{\partial x^3\partial y} + \frac{\partial^4}{\partial x\partial y^3}\right). \end{cases} \quad (10)$$

把方程(10)代入方程(9)得

$$u_z = \lambda_{11}R_3\frac{\partial^4F}{\partial x^4} + 2(\lambda_{11}R_3 + 2e_{14}d_{123})\frac{\partial^4F}{\partial x^2\partial y^2} + \lambda_{11}R_3\frac{\partial^4F}{\partial y^4}, \quad (11)$$

$$w_z = -\lambda_{11}C_{44}\frac{\partial^4F}{\partial x^4} - 2(\lambda_{11}C_{44} + 2e_{14}^2)\frac{\partial^4F}{\partial x^2\partial y^2} - \lambda_{11}C_{44}\frac{\partial^4F}{\partial y^4}, \quad (12)$$

$$\Phi = 2(e_{14}R_3 - d_{123}C_{44})\left(\frac{\partial^4F}{\partial x^3\partial y} + \frac{\partial^4F}{\partial x\partial y^3}\right). \quad (13)$$

假设复函数 $F(x, y)$ 的形式为 $F(x, \mu y)$, 则 μ 须满足如下特征方程^[23]:

$$a\mu^6 + b\mu^4 + b\mu^2 + a = 0. \quad (14)$$

方程(14)有6个纯虚数根:

$$\mu_1 = is_1 = i, \mu_2 = is_2 = i \frac{\sqrt{b+a} + \sqrt{b-3a}}{2\sqrt{a}}, \mu_3 = is_3 = i \frac{\sqrt{b+a} - \sqrt{b-3a}}{2\sqrt{a}},$$

$$\mu_4 = -\mu_1, \mu_5 = -\mu_2, \mu_6 = -\mu_3,$$

其中 $i = \sqrt{-1}$, $s_1 = 1$, $\mu_2\mu_3 = -1$ (或 $s_2s_3 = 1$).

根据解析函数的性质和方程(8), 位移函数 F 可以表示为

$$F = 2\text{Re} \sum_{k=1}^3 F_k(z_k), \quad (15)$$

其中 $\text{Re}(\cdot)$ 表示实部, $F_k(z_k)$ 为关于 $z_k = x + \mu_k y$ ($k = 1, 2, 3$) 的任意解析函数. 结合方程(1)、(3)、(11)、(12)、(13)可知, 应力和电位移的复表示为

$$\sigma_{yz} = -4e_{14}(d_{123}C_{44} - e_{14}R_3) \text{Re} \sum_{k=1}^3 (\mu_k - \mu_k^3) F_k^{(5)}(z_k), \quad (16)$$

$$\sigma_{zx} = 4e_{14}(d_{123}C_{44} - e_{14}R_3) \text{Re} \sum_{k=1}^3 (\mu_k^2 - \mu_k^4) F_k^{(5)}(z_k), \quad (17)$$

$$H_{yz} = \text{Re} \sum_{k=1}^3 (l\mu_k + m\mu_k^3 + n\mu_k^5) F_k^{(5)}(z_k), \quad (18)$$

$$H_{zx} = \text{Re} \sum_{k=1}^3 (n + m\mu_k^2 + l\mu_k^4) F_k^{(5)}(z_k), \quad (19)$$

$$D_x = 2\lambda_{11}(d_{123}C_{44} - e_{14}R_3) \text{Re} \sum_{k=1}^3 (\mu_k - \mu_k^5) F_k^{(5)}(z_k), \quad (20)$$

$$D_y = -2\lambda_{11}(d_{123}C_{44} - e_{14}R_3) \text{Re} \sum_{k=1}^3 (1 - \mu_k^4) F_k^{(5)}(z_k), \quad (21)$$

其中

$$l = 2\lambda_{11}(R_3^2 - C_{44}K_{44}) - 4d_{123}^2C_{44} + 4e_{14}d_{123}R_3,$$

$$m = 4\lambda_{11}(R_3^2 - C_{44}K_{44}) - 4d_{123}^2C_{44} - 8e_{14}^2K_{44} + 12e_{14}d_{123}R_3,$$

$$n = 2\lambda_{11}(R_3^2 - C_{44}K_{44}).$$

2 立方压电准晶材料半空间问题基本解

假设立方压电准晶材料所占半空间区域为 $y = 0$ 下方区域, 半空间表面受力电载荷为 $\sigma_{yz} = S_1^*(x)$, $H_{yz} = S_2^*(x)$, $\Phi = \Phi^*(x)$, 如图1所示.

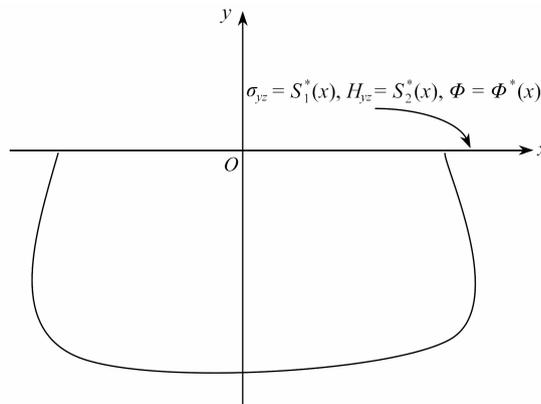


图1 力电载荷作用下的半无限区域

Fig. 1 The semi-infinite region under electromechanical load

由于当 $y = 0$ 时, $z_1 = z_2 = z_3 = \xi, \xi$ 为实数,则方程(13)、(16)、(18)可以改写为

$$\begin{cases} \sum_{k=1}^3 (s_k + s_k^3) g'_k(\xi) = \sum_{k=1}^3 (s_k + s_k^3) \overline{g'_k(\xi)} + \frac{iS_1^*(\xi)}{2e_{14}(d_{123}C_{44} - e_{14}R_3)}, \\ \sum_{k=1}^3 (ls_k - ms_k^3 + ns_k^5) g'_k(\xi) = \sum_{k=1}^3 (ls_k - ms_k^3 + ns_k^5) \overline{g'_k(\xi)} - 2iS_2^*(\xi), \\ \sum_{k=1}^3 (s_k - s_k^3) g'_k(\xi) = \sum_{k=1}^3 (s_k - s_k^3) \overline{g'_k(\xi)} - \frac{iE^*(\xi)}{2(d_{123}C_{44} - e_{14}R_3)}, \end{cases} \quad (22)$$

其中

$$g'_k(z_k) = F_k^{(5)}(z_k), \quad k = 1, 2, 3.$$

对方程(22)积分可得

$$\begin{cases} g'_1(z_1) = - \int_{-\infty}^{+\infty} a_1 \left(\frac{d_{123}}{e_{14}} S_1^* - S_2^* \right) \frac{1}{\xi - z_1} d\xi, \\ g'_2(z_2) = - \int_{-\infty}^{+\infty} \frac{a_1 s_3^3}{1 + s_3^2} (a_2 S_1^* + S_2^*) \frac{1}{\xi - z_2} d\xi - \\ \int_{-\infty}^{+\infty} \frac{s_3^3}{1 + s_3^2} \left(\frac{1}{8\pi(C_{44}d_{123} - e_{14}R_3)} + a_1 a_3 (1 - s_3^2) \right) \frac{E^*}{\xi - z_2} d\xi, \\ g'_3(z_3) = - \int_{-\infty}^{+\infty} \frac{a_1}{s_3(1 + s_3^2)} (a_2 S_1^* + S_2^*) \frac{1}{\xi - z_3} d\xi - \\ \int_{-\infty}^{+\infty} \frac{1}{s_3(1 + s_3^2)} \left(\frac{1}{8\pi(C_{44}d_{123} - e_{14}R_3)} + a_1 a_3 \left(1 - \frac{1}{s_3^2} \right) \right) \frac{E^*}{\xi - z_3} d\xi, \end{cases} \quad (23)$$

其中 $a_i (i = 1, 2, 3)$ 为常数(见附录),方程(23)为立方压电准晶材料半空间问题基本解,结合边界条件,可以得到弹性场分析.作为具体应用,下面讨论集中线力作用下立方压电准晶材料半空间问题.

3 集中线力作用在半空间表面

假设集中线力沿 z 轴方向作用于半空间表面,这里取 $S_1^*(\xi) = S_1 \delta(\xi), S_2^*(\xi) = S_2 \delta(\xi)$, 其中 δ 为 Delta 函数, S_1, S_2 为单位长度线性力,电势为常量,即 $E^* = 0$.则由方程(23)可得

$$g_1(z_1) = a_1 \left(\frac{d_{123}}{e_{14}} S_1 - S_2 \right) \ln z_1, \quad (24)$$

$$g_2(z_2) = \frac{a_1 s_3^3}{1 + s_3^2} (a_2 S_1 + S_2) \ln z_2, \quad (25)$$

$$g_3(z_3) = \frac{a_1}{s_3(1 + s_3^2)} (a_2 S_1 + S_2) \ln z_3. \quad (26)$$

由方程(24)——(26)可得声子场和相位子场的位移、电势表达式为

$$u_z = - a_4 d_{123} \ln(x^2 + y^2) + a_5 a_6 [\ln(x^2 + s_2^2 y^2) + \ln(x^2 + s_3^2 y^2)], \quad (27)$$

$$w_z = a_4 e_{14} \ln(x^2 + y^2) - a_5 a_7 [\ln(x^2 + s_2^2 y^2) + \ln(x^2 + s_3^2 y^2)], \quad (28)$$

$$\Phi = a_5 a_8 \left(- \tan^{-1} \frac{s_2 y}{x} + \tan^{-1} \frac{s_3 y}{x} \right), \quad (29)$$

其中 $a_i (i = 4, 5, \dots, 8)$ 为常数(见附录).当不考虑相位子场时,声子场位移表达式可以退化为

$$u_z = - \frac{S_1}{2\pi C_{44}} \ln(x^2 + y^2), \quad (30)$$

且电势处处为零,与文献[24]结果一致.由方程(24)——(26)也可得到声子场和相位子场应力及电位移表达

式(见附录)。

下面讨论声子场位移、相位子场位移和电势分布情况,材料常数为^[12]

$$C_{44} = 5.0 \times 10^{10} \text{ N}\cdot\text{m}^{-2}, K_{44} = 3 \times 10^8 \text{ N}\cdot\text{m}^{-2}, R_3 = 1.2 \times 10^9 \text{ N}\cdot\text{m}^{-2},$$

$$e_{14} = -0.138 \text{ C}\cdot\text{m}^{-2}, d_{123} = -0.16 \text{ C}\cdot\text{m}^{-2}, \lambda_{11} = 8.26 \times 10^{-11} \text{ C}^2\cdot\text{N}^{-1}\cdot\text{m}^{-2},$$

$$S_1 = 2\,000 \text{ N}\cdot\text{m}^{-1}, S_2 = 2\,500 \text{ N}\cdot\text{m}^{-1}.$$

图2中 $\bar{u}_z = u_z / (10^{-8} \text{ m})$ 为无量纲声子场位移,图3中 $\bar{w}_z = w_z / (10^{-6} \text{ m})$ 为无量纲相位子场位移.从图中可以看出,声子场和相位子场位移的等势线分别关于 x 轴、 y 轴对称,是从力的作用点出发的,并且在同一点处位移具有对数奇异性。

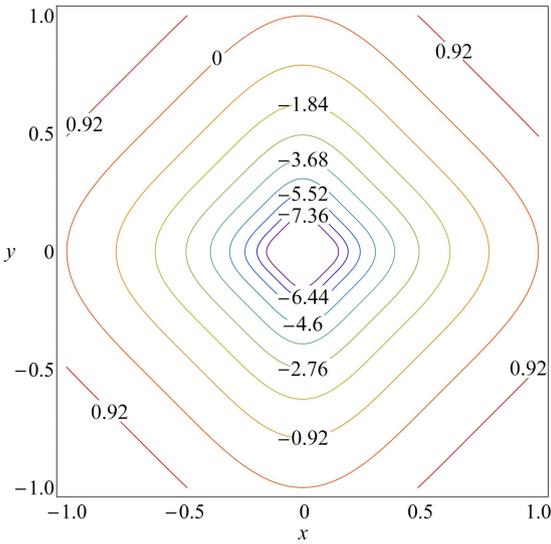


图2 无量纲声子场位移 \bar{u}_z 等势图

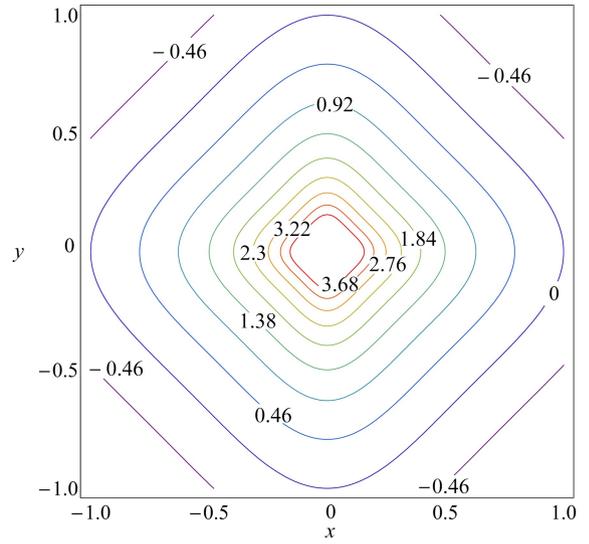


图3 无量纲相位子场位移 \bar{w}_z 等势图

Fig. 2 The contour of dimensionless phonon field displacement \bar{u}_z

Fig. 3 The contour of dimensionless phason field displacement \bar{w}_z

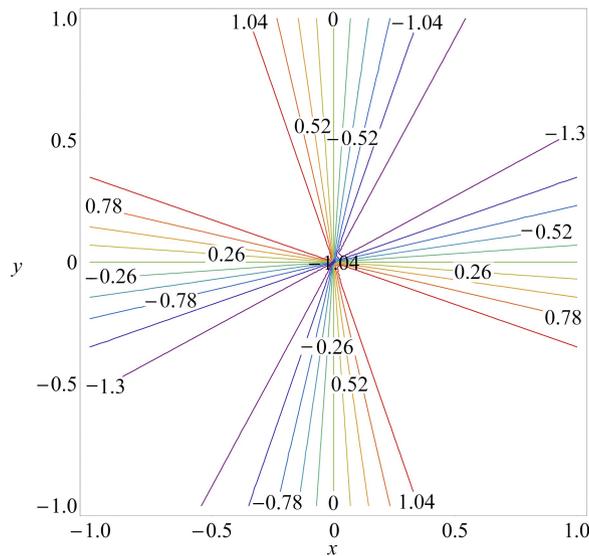


图4 无量纲电势 $\bar{\Phi}$ 等势图

Fig. 4 The contour of dimensionless potential $\bar{\Phi}$

图4中 $\bar{\Phi} = \Phi / (10^3 \text{ N}\cdot\text{m}\cdot\text{C}^{-1})$ 为无量纲电势.从图中可以看出,电势的等势线是直的,是从力的作用点出发,且 x, y 同号时电势值均为负, x, y 异号时电势值均为正。

4 结 论

本文采用复变函数方法获得了反平面机械载荷和面内电载荷作用下,立方准晶压电材料半空间问题的基本解.在此基础上,给出了集中线力作用下,立方准晶压电材料半空间问题的位移、应力和电场的解析表达式,并用数值结果说明了声子场、相位子场位移和电势的分布情况.本文获得的立方准晶压电材料半空间问题的基本解可应用于其他半空间边值问题的研究中.

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附 录

$$\begin{aligned}
 a_1 &= \frac{1}{8\pi(C_{44}d_{123}^2 + e_{14}(e_{14}K_{44} - 2d_{123}R_3))}, \\
 a_2 &= \frac{e_{14}K_{44} - d_{123}R_3}{C_{44}d_{123} - e_{14}R_3}, \\
 a_3 &= \frac{\lambda_{11}(C_{44}K_{44} - R_3^2)}{2(C_{44}d_{123} - e_{14}R_3)}, \\
 a_4 &= 4a_1(d_{123}S_1 - e_{14}S_2), \\
 a_5 &= a_1(a_2S_1 + S_2), \\
 a_6 &= \frac{-4d_{123}e_{14}s_3^2 + \lambda_{11}R_3(-1 + s_3^2)^2}{s_3(1 + s_3^2)}, \\
 a_7 &= \frac{-4e_{14}^2s_3^2 + \lambda_{11}C_{44}(-1 + s_3^2)^2}{s_3(1 + s_3^2)}, \\
 a_8 &= \frac{4(C_{44}d_{123} - e_{14}R_3)(-1 + s_3^2)}{1 + s_3^2}, \\
 \sigma_{yz} &= -b_1 \left(a_4 \frac{y}{x^2 + y^2} + 2a_5 e_{14} \left(\frac{s_2 y}{x^2 + s_2^2 y^2} + \frac{s_3 y}{x^2 + s_3^2 y^2} \right) \right), \\
 \sigma_{zx} &= -b_1 \left(a_4 \frac{x}{x^2 + y^2} + 2a_5 e_{14} \left(\frac{s_2 x}{x^2 + s_2^2 y^2} + \frac{s_3 x}{x^2 + s_3^2 y^2} \right) \right), \\
 H_{yz} &= a_4 b_2 \frac{y}{x^2 + y^2} + 2a_5 \left(b_3 \frac{s_2 y}{x^2 + s_2^2 y^2} + b_4 \frac{s_3 y}{x^2 + s_3^2 y^2} \right), \\
 H_{zx} &= a_4 b_2 \frac{x}{x^2 + y^2} + 2a_5 \left(b_4 \frac{s_2 x}{x^2 + s_2^2 y^2} + b_3 \frac{s_3 x}{x^2 + s_3^2 y^2} \right), \\
 D_x &= a_5 b_5 \left(\frac{s_2^2 y}{x^2 + s_2^2 y^2} - \frac{s_3^2 y}{x^2 + s_3^2 y^2} \right), \\
 D_y &= -a_5 b_5 \left(\frac{x}{x^2 + s_2^2 y^2} - \frac{x}{x^2 + s_3^2 y^2} \right),
 \end{aligned}$$

其中

$$\begin{aligned}
 b_1 &= 2(C_{44}d_{123} - e_{14}R_3), \\
 b_2 &= 2(e_{14}K_{44} - d_{123}R_3), \\
 b_3 &= \frac{-a_3 b_1(-1 + s_3^2)^2}{s_3^2(1 + s_3^2)} - \frac{a_8 d_{123}}{2} + \frac{2b_2 e_{14}}{1 + s_3^2}, \\
 b_4 &= \frac{-a_3 b_1(-1 + s_3^2)^2}{1 + s_3^2} + \frac{a_8 d_{123}}{2} + \frac{2b_2 e_{14} s_3^2}{1 + s_3^2},
 \end{aligned}$$

$$b_5 = \frac{\lambda_{11} a_8 (1 + s_3^2)}{2s_3}.$$

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