

# 完整 Coriolis 力作用下的非线性近惯性波<sup>\*</sup>

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**摘要:** 从包含有完整 Coriolis 力作用下的大气运动原始基本方程组出发, 通过尺度分析, 采用多重尺度法及摄动展开法, 推导了中高纬大气非线性近惯性波振幅演化所满足的 Korteweg-de Vries 方程. 从演化方程的结果可以看出 Coriolis 参数水平分量对非线性近惯性波的影响, 主要体现在对频散效应的修正及与基本流的相互作用, 从理论上解释了完整 Coriolis 力作用下的中高纬地区大气非线性近惯性波运动的物理机制.

**关键词:** 近惯性波; 完整 Coriolis 力; Korteweg-de Vries 方程

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## 引 言

大气运动是由一系列方程所描述的, 主要包括热力学方程、连续性方程、状态方程、动量方程以及能量方程等. 由于方程精确形式的复杂性, 研究者试图寻求各种近似方法来简化方程组, 如浅水模式近似、静力近似等. 浅水模式近似是常用的近似方法之一, 其忽略了动量方程中四项度量项, 更重要的是忽略了动量方程中 Coriolis 力水平分量项, 称之为“传统近似”<sup>[1]</sup>. “传统近似”将动量方程简化为二维问题, 且还能够保持一些基本物理原理, 如角动量守恒<sup>[2-4]</sup>. 在“传统近似”下, 大气 Rossby 孤立波的产生或者影响因子是很多学者关心的问题<sup>[5-15]</sup>. 目前, 考虑完善的 Coriolis 力水平分量的研究还不是很多.

对于中高纬地区大气运动, 从定量角度而言, “传统近似”是合适的. Kasahara 指出忽略垂直方向的加速度比忽略 Coriolis 水平分量所带来的误差可能更大<sup>[16]</sup>. 但是就动力学角度而言, “传统近似”是有争议的<sup>[17]</sup>, 因此建议在弹性近似中包含 Coriolis 水平分量项, 称为“非传统近似”. Gerkema 和 Shrira 从含有完整 Coriolis 力的基本方程组出发, 考虑了“非传统近似”下的近惯性波<sup>[18]</sup>. Dellar 和 Salmon 通过变分原理得到具有完整 Coriolis 力作用的位涡守恒方程<sup>[19]</sup>.

对于正压流体, Long 在 1964 年做了开创性的研究, 得到在  $\beta$  平面近似下 Rossby 波振幅演变满足 Korteweg-de Vries 方程<sup>[20]</sup>. 随后罗德海和张永利等还分别研究了 Rossby 波振幅演变下的 Schrödinger 方程<sup>[21-22]</sup>. Boyd 用多重尺度法, 从基本方程导出在正压流体中小振幅 Rossby 孤立波振幅演变满足非线性 KdV 方程和 mKdV 方程. 笔者从能量的角度出发分别研究了正压模式和正压准地转模式下的能量守恒问题<sup>[23-24]</sup>. 但是大气空间等压面和等密度面是相交的, 亦

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即大气是斜压的,常常为了使问题简化,将大气看做是一种理想化的大气状态分布(正压大气);对于斜压大气的研究,有从大尺度环流指数结合大气的斜压性讨论了温带气旋和风暴轴 20 世纪变化的可能原因<sup>[25]</sup>,郝世峰等<sup>[26]</sup>证明了采用半解析方法求解大气原始方程组是可行的,为大气数值模拟的构建提供了一个新的思路.滕代高等<sup>[27]</sup>对斜压大气中台风涡旋自组织的问题进行了初步研究,研究表明和正压大气的结果类似.这些结果都是对斜压大气实际应用很好的补充与推广,但是对斜压大气理论方面的认识并不多.

Rossby 波在大气大尺度循环中扮演着至关重要的角色,对于 Rossby 波的研究将是今后大气动力学方面的一个重点.本文在考虑了完整 Coriolis 力的情况下,从最原始的大气基本方程组出发,得到了斜压大气下 Rossby 波振幅所满足的 KdV 方程,并且进一步分析了 Coriolis 力对 Rossby 波的影响.

## 1 大气动力学方程组的摄动展开

将垂直方向的气压梯度力与压力表示成扰动气压梯度与浮力之和,并采用 Boussinesq 近似,此时,大气运动的基本方程组为

$$\begin{cases} \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} = -\frac{1}{\rho_0} \frac{\partial p}{\partial x} + f_v - f_H u, \\ \frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} = -\frac{1}{\rho_0} \frac{\partial p}{\partial y} - f_u, \\ \frac{\partial w}{\partial t} + u \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + w \frac{\partial w}{\partial z} = -\frac{1}{\rho_0} \frac{\partial p}{\partial z} + g \frac{\theta}{\theta_0} + f_H u, \\ \frac{\partial \theta}{\partial t} + u \frac{\partial \theta}{\partial x} + v \frac{\partial \theta}{\partial y} + w \Delta = 0, \\ \frac{\partial(\rho_0 u)}{\partial x} + \frac{\partial(\rho_0 v)}{\partial y} + \frac{\partial(\rho_0 w)}{\partial z} = 0, \end{cases} \quad (1)$$

其中,  $\theta_0, \rho_0$  分别是环境流场的位温与密度,它们只是高度的函数,

$$\Delta = \frac{d\theta_0}{dz}. \quad (2)$$

再将各变量写成其特征尺度与无量纲的乘积:

$$\begin{cases} (x, y) = L(x', y'), Z = D(Z'), f = f^{-1}(t'), \\ (u, v) = U(u', v'), w = \frac{U}{L} D(w'), \theta = \delta\theta(\theta'), \\ \delta p_{x,y} = \frac{P}{gH} fLU(p'), \delta p_z = \frac{P}{\theta_0} \delta\theta(p'), \rho_0 = \frac{P}{gH}(\rho_s), \end{cases} \quad (3)$$

其中,  $H$  是均值大气的高度,  $P$  是地面的特征尺度,  $\delta p_{x,y}$  表示水平方向的气候变化,  $\delta p_z$  则是其垂直方向的变化,“'”表示无量纲量.

将式(3)代入式(1),可以得到如下方程组:

$$\begin{cases}
 \frac{\partial u}{\partial t} + R_0 u \frac{\partial u}{\partial x} + R_0 v \frac{\partial u}{\partial y} + R_0 w \frac{\partial u}{\partial z} = -\frac{1}{\rho_s} \frac{\partial p}{\partial x} + V - \frac{f_H D}{fL} W, \\
 \frac{\partial v}{\partial t} + R_0 u \frac{\partial v}{\partial x} + R_0 v \frac{\partial v}{\partial y} + R_0 w \frac{\partial v}{\partial z} = -\frac{1}{\rho_s} \frac{\partial p}{\partial y} - u, \\
 \frac{\partial w}{\partial t} + R_0 u \frac{\partial w}{\partial x} + R_0 v \frac{\partial w}{\partial y} + R_0 w \frac{\partial w}{\partial z} = \frac{gL\delta\theta}{Dfu\theta_0} \left( -\frac{1}{\rho_s} \frac{\partial p}{\partial z} + \theta \right) + \frac{f_H L}{fD} u, \\
 \frac{\partial \theta}{\partial t} + R_0 u \frac{\partial \theta}{\partial x} + R_0 v \frac{\partial \theta}{\partial y} + R_0 w \frac{\partial \theta}{\partial z} + \frac{UD\Delta}{fL\delta\theta} w = 0, \\
 \frac{\partial(\rho_0 u)}{\partial x} + \frac{\partial(\rho_0 v)}{\partial y} + \frac{\partial(\rho_0 w)}{\partial z} = 0.
 \end{cases} \quad (4)$$

如下定义形态比:  $\delta = D/L$ . 定义 Coriolis 水平分量与垂直分量比为:  $\gamma = f_H/f$  且假设  $\delta \cdot \gamma \ll \gamma/\delta \ll 1$ , 这样做是符合要求的. 由于式(4)中第四式第二项比较小, 为了量纲上的平衡, 故有

$$\frac{UD\Delta}{fL\delta\theta} \sim o(1), \quad (5a)$$

$$\delta\theta \sim \frac{UD\Delta}{fL} \sim \Delta D. \quad (5b)$$

由于  $R_0 = U/(fL)$  为 Rossby 数, 考虑中尺度大气, 则  $R_0 \sim o(1)$ , 从而有

$$\frac{gL\delta\theta}{DfU\theta_0} \sim \frac{gL\Delta D}{DfU\theta_0} \sim \frac{g\Delta}{f^2\theta_0} \sim \frac{N^2}{f^2}, \quad (6)$$

其中,  $g\Delta/\theta_0 = N^2$  是 Brunt-Väisälä 频率. 记  $\varepsilon = f^2/N^2$ , 则  $\varepsilon \ll 1$ , 在如上的假设及定义下, 方程组(4)变为如下形式:

$$\begin{cases}
 \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} = -\frac{1}{\rho_s} \frac{\partial p}{\partial x} + v - \delta\gamma w, \\
 \frac{\partial v}{\partial t} + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial y} + w \frac{\partial v}{\partial z} = -\frac{1}{\rho_s} \frac{\partial p}{\partial y} - u, \\
 \frac{\partial w}{\partial t} + u \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + w \frac{\partial w}{\partial z} = \varepsilon^{-1} \left( \frac{1}{\rho_s} \frac{\partial p'}{\partial z} + \theta \right) + \frac{\gamma}{\delta} u, \\
 \frac{\partial \theta}{\partial t} + u \frac{\partial \theta}{\partial x} + v \frac{\partial \theta}{\partial y} + w \theta = 0, \\
 \frac{\partial \rho_s u}{\partial x} + \frac{\partial \rho_s v}{\partial y} + \frac{\partial \rho_s w}{\partial z} = 0.
 \end{cases} \quad (7)$$

记  $\alpha = \delta\gamma, \beta = \gamma/\delta$  表征带有水平分量的方程项系数.

## 2 多重尺度法、摄动展开法

为了导出 KdV 方程, 作如下的 G-M 变换, 令

$$\begin{cases}
 \xi = \varepsilon^{1/2}(x - ct), \\
 T = \varepsilon^{3/2}t,
 \end{cases} \quad (8)$$

则有

$$\begin{cases} \frac{\partial}{\partial x} = \varepsilon^{1/2} \frac{\partial}{\partial \xi}, \\ \frac{\partial}{\partial t} = -c\varepsilon^{1/2} \frac{\partial}{\partial \xi} + \varepsilon^{3/2} \frac{\partial}{\partial T}, \\ \frac{\partial}{\partial y} = \frac{\partial}{\partial y}, \quad \frac{\partial}{\partial z} = \frac{\partial}{\partial z}. \end{cases} \quad (9)$$

将  $u, v, w, p, \theta$  按参数  $\varepsilon$  展开, 得到

$$\begin{cases} u = \bar{U}(y, z) + \varepsilon u_0 + \varepsilon^2 u_1 + \varepsilon^3 u_2 + \dots, \\ v = \varepsilon(\varepsilon^{1/2} v_0 + \varepsilon^{3/2} v_1 + \dots), \\ w = \varepsilon(\varepsilon^{1/2} w_0 + \varepsilon^{3/2} w_1 + \dots), \\ \theta = \bar{\theta}(y, z) + \varepsilon \theta_0 + \varepsilon^2 \theta_1 + \varepsilon^3 \theta_2 + \dots, \\ p = \bar{p}(y, z) + \varepsilon p_0 + \varepsilon^2 p_1 + \varepsilon^3 p_2, \end{cases} \quad (10)$$

这里的  $\bar{U}, \bar{\theta}, \bar{p}$  分别是基本气流的速度、位温和气压场, 它们只是  $y, z$  的函数, 将式(9)、(10)代入到式(7), 得到如下的方程组:

$$\begin{cases} \left( -\varepsilon^{1/2} c \frac{\partial}{\partial \xi} + \varepsilon^{3/2} \frac{\partial}{\partial T} \right) (\bar{u} + u') + (\bar{u} + u') \varepsilon^{1/2} \frac{\partial}{\partial \xi} (\bar{u} + u') + v \frac{\partial}{\partial y} (\bar{u} + u') + \\ w \frac{\partial}{\partial z} (\bar{u} + u') = -\frac{1}{\rho_s} \varepsilon^{1/2} \frac{\partial}{\partial \xi} (\bar{p}(y, z) + p') + v - \alpha w, \\ \left( -\varepsilon^{1/2} c \frac{\partial}{\partial \xi} + \varepsilon^{3/2} \frac{\partial}{\partial T} \right) v + (\bar{u} + u') \varepsilon^{1/2} \frac{\partial}{\partial \xi} v + v \frac{\partial}{\partial y} v + w \frac{\partial}{\partial z} v = \\ -\frac{1}{\rho_s} \frac{\partial}{\partial \xi} (\bar{p}(y, z) + p') - (\bar{u} + u'), \\ \left( -\varepsilon^{1/2} c \frac{\partial}{\partial \xi} + \varepsilon^{3/2} \frac{\partial}{\partial T} \right) w + (\bar{u} + u') \varepsilon^{1/2} \frac{\partial}{\partial \xi} w + v \frac{\partial}{\partial y} w + w \frac{\partial}{\partial z} w = \\ \varepsilon^{-1} \left( -\frac{1}{\rho_s} \frac{\partial}{\partial z} (\bar{p}(y, z) + p') + \bar{\theta} + \theta' \right) + \beta (\bar{u} + u'), \\ \left( -\varepsilon^{1/2} c \frac{\partial}{\partial \xi} + \varepsilon^{3/2} \frac{\partial}{\partial T} \right) (\bar{\theta} + \theta') + (\bar{u} + u') \varepsilon^{1/2} \frac{\partial}{\partial \xi} (\bar{\theta} + \theta') + \\ v \frac{\partial}{\partial y} (\bar{\theta} + \theta') + w = 0, \\ \varepsilon^{1/2} \frac{\partial \rho_s (\bar{u} + u')}{\partial \xi} + \frac{\partial \rho_s v}{\partial y} + \frac{\partial \rho_s w}{\partial z} = 0. \end{cases} \quad (11)$$

$\varepsilon$  的零级近似,

$$\begin{cases} -\frac{1}{\rho_s} \frac{\partial \bar{p}}{\partial y} - \bar{u} = 0, \\ -\frac{1}{\rho_s} \frac{\partial \bar{p}}{\partial z} + \bar{\theta} = 0. \end{cases} \quad (12)$$

上式表明基本气流是地转平衡和静力平衡, 对基本气流还可以进一步假设

$$\left| \frac{1}{\rho_s^2} \frac{\partial \rho_s}{\partial y} \right| \ll 1, \quad \frac{\partial \bar{u}}{\partial z} = -\frac{\partial \bar{\theta}}{\partial y}. \quad (13)$$

$\varepsilon$  的一级近似,

$$o(\varepsilon^{3/2}): (\bar{u} - c) \frac{\partial}{\partial \xi} u_0 + (\bar{u}_y - 1)v_0 + (\bar{u}_z + \alpha)w_0 + \frac{1}{\rho_s} \frac{\partial p_0}{\partial \xi} = 0, \quad (14)$$

$$o(\varepsilon^1): \frac{1}{\rho_s} \frac{\partial p_0}{\partial y} + u_0 = 0, \quad (15)$$

$$o(\varepsilon^0): -\frac{1}{\rho_s} \frac{\partial p_0}{\partial z} + \theta_0 + \beta \bar{u} = 0, \quad (16)$$

$$o(\varepsilon^{3/2}): (\bar{u} - c) \frac{\partial \theta'_0}{\partial \xi} + \bar{\theta}_y v_0 + w_0 = 0, \quad (17)$$

$$o(\varepsilon^{3/2}): \frac{\partial(\rho_s u_0)}{\partial \xi} + \frac{\partial(\rho_s v_0)}{\partial y} + \frac{\partial(\rho_s w_0)}{\partial z} = 0; \quad (18)$$

$\varepsilon$  的二级近似,

$$o(\varepsilon^{5/2}): (\bar{u} - c) \frac{\partial}{\partial \xi} u_1 + (\bar{u}_y - 1)v_1 + (\bar{u}_z - \alpha)w_1 + \frac{1}{\rho_s} \frac{\partial p_1}{\partial x} =$$

$$- \left( \frac{\partial}{\partial T} u_0 + u_0 \frac{\partial u_0}{\partial \xi} + v_0 \frac{\partial u_0}{\partial y} + w_0 \frac{\partial u_0}{\partial z} \right), \quad (19)$$

$$o(\varepsilon^2): \frac{1}{\rho_s} \frac{\partial p_1}{\partial y} + u_1 = -(\bar{u} - c) \frac{\partial v_0}{\partial \xi}, \quad (20)$$

$$o(\varepsilon^1): \frac{1}{\rho_s} \frac{\partial p_1}{\partial z} - \theta_1 = \beta u_0, \quad (21)$$

$$o(\varepsilon^{5/2}): (\bar{u} - c) \frac{\partial \theta_1}{\partial \xi} + \bar{\theta}_y v_1 + w_1 = - \left( \frac{\partial}{\partial T} \theta_0 + u_0 \frac{\partial \theta_0}{\partial \xi} + v_0 \frac{\partial \theta_0}{\partial y} \right), \quad (22)$$

$$o(\varepsilon^{5/2}): \frac{\partial \rho_s u_1}{\partial \xi} + \frac{\partial \rho_s v_1}{\partial y} + \frac{\partial \rho_s w_1}{\partial z} = 0. \quad (23)$$

### 3 KdV 方程的导出

引入新的变量:

$$\rho_s u_0 = u'_0, \quad \rho_s v_0 = v'_0, \quad \rho_s w_0 = w'_0, \quad \rho_s \theta_0 = \theta'_0, \quad p_0 = p'_0, \quad (24)$$

$$\rho_s u_1 = u'_1, \quad \rho_s v_1 = v'_1, \quad \rho_s w_1 = w'_1, \quad \rho_s \theta_1 = \theta'_1, \quad p_1 = p'_1. \quad (25)$$

于是,可将方程(14)~(18)、(19)~(23)写为

$$\begin{cases} (\bar{u} - c) \frac{\partial u_i}{\partial \xi} + (\bar{u}_y - 1)v_i + (\bar{u}_z + \alpha)w_i + \frac{\partial p_i}{\partial \xi} = Au_i, \\ \frac{\partial p_i}{\partial y} + u_i = Av_i, \\ \frac{\partial p_i}{\partial z} - \theta_i = Aw_i, \\ (\bar{u} - c) \frac{\partial \theta_i}{\partial \xi} + \bar{\theta}_y v_i + w_i = A\theta_i, \\ \frac{\partial u_i}{\partial \xi} + \frac{\partial v_i}{\partial y} + \frac{\partial w_i}{\partial z} = 0, \quad i = 0, 1, \end{cases} \quad (26)$$

其中

$$Au_0 = Av_0 = A\theta_0, \quad Aw_0 = \beta \bar{\rho}_s, \quad (27)$$

$$Au_1 = -\frac{\partial u_0}{\partial T} - \frac{1}{\rho_s} \left( u_0 \frac{\partial u_0}{\partial \xi} + v_0 \frac{\partial v_0}{\partial y} \right) - u_0 \frac{\partial}{\partial z} \left( \frac{u_0}{\rho_s} \right), \quad (28)$$

$$Av_1 = -(\bar{u} - c) \frac{\partial v_0}{\partial \xi}, \quad (29)$$

$$Aw_1 = \beta u_0, \quad (30)$$

$$A\theta_1 = -\frac{\partial \theta_0}{\partial T} - \frac{1}{\rho_s} \left( u_0 \frac{\partial \theta_0}{\partial \xi} + v_0 \frac{\partial \theta_0}{\partial y} \right). \quad (31)$$

下面将对方程(26)进行消元,得到

$$\begin{aligned} & \left\{ \frac{\partial}{\partial z} (\bar{u} - c) \frac{\partial}{\partial z} + \bar{\theta}_{y_2} \frac{1}{(\bar{u}_z + \alpha) \bar{\theta}_y - \bar{u}_y + 1} \left[ -(\bar{u} - c) \frac{\partial}{\partial y} + 1 - \right. \right. \\ & \quad \left. \left. (\bar{u}_z + \alpha) (\bar{u} - c) \frac{\partial}{\partial z} \right] + (\bar{\theta}_y - 1) \frac{\partial}{\partial y} \left\{ \frac{1}{(\bar{u}_z + \alpha) \bar{\theta}_y - \bar{u}_y + 1} \times \right. \right. \\ & \quad \left. \left. \left[ -(\bar{u} - c) \frac{\partial}{\partial y} + 1 - (\bar{u}_z + \alpha) (\bar{u} - c) \frac{\partial}{\partial z} \right] \right\} \right\} \frac{\partial p_i}{\partial \xi} + \frac{\partial^2 p_i}{\partial y \partial \xi} = \\ & \quad - \bar{\theta}_{y_2} \frac{1}{(\bar{u}_z + \alpha) \bar{\theta}_y - \bar{u}_y + 1} \left[ (\bar{u} - c) \frac{\partial}{\partial \xi} (Av_i) - Au_i + \right. \\ & \quad \left. (\bar{u}_z + \alpha) (\bar{u} - c) \frac{\partial}{\partial \xi} (Aw_i) + (\bar{u}_z + \alpha) A\theta_i \right] - \\ & \quad (\bar{\theta}_y - 1) \frac{\partial}{\partial y} \left\{ \frac{1}{(\bar{u}_z + \alpha) \bar{\theta}_y - \bar{u}_y + 1} \left[ (\bar{u} - c) \frac{\partial}{\partial \xi} (Av_i) - \right. \right. \\ & \quad \left. \left. Au_i + (\bar{u}_z + \alpha) (\bar{u} - c) \frac{\partial}{\partial \xi} (Aw_i) + (\bar{u}_z + \alpha) A\theta_i \right] \right\} + \\ & \quad \frac{\partial}{\partial z} (\bar{u} - c) \frac{\partial}{\partial \xi} (Aw_i) + \frac{\partial}{\partial z} (A\theta_i) + \frac{\partial}{\partial \xi} (Av_i). \end{aligned} \quad (32)$$

当  $i = 0$  时, 方程(32)右端  $Au_0 = Av_0 = A\theta_0 = 0, Aw_0 = \rho \bar{u}(y, z)$ , 记

$$\ell_{y,z} = \frac{\partial}{\partial z} (\bar{u} - c) \frac{\partial}{\partial z} + \bar{\theta}_{y,z} \frac{1}{(\bar{u}_z + \alpha) \bar{\theta}_y - \bar{u}_y + 1} \times$$

$$\begin{aligned} & \left[ -(\bar{u} - c) \frac{\partial}{\partial y} + 1 - (\bar{u}_2 + \alpha)(\bar{u} - c) \frac{\partial}{\partial z} \right] + \\ & (\bar{\theta}_y - 1) \frac{\partial}{\partial y} \left\{ \frac{1}{(\bar{u}_2 + \alpha)\bar{\theta}_y - \bar{u}_y + 1} \left[ -(\bar{u} - c) \frac{\partial}{\partial y} + 1 - \right. \right. \\ & \left. \left. (\bar{u}_2 + \alpha)(\bar{u} - c) \frac{\partial}{\partial z} \right] \right\} + \frac{\partial}{\partial y}, \end{aligned} \quad (33)$$

则  $\ell_{y,p}(\partial p_0 / \partial \xi) = 0$ . 方程(32)是一个变量可分离的方程, 设其解为

$$p_0 = \hat{p}_0(y, z) n_0(T, \xi), \quad (34)$$

从而有

$$\ell_{y,p}(\hat{p}_0) = 0. \quad (35)$$

在一定条件下可以解出  $\hat{p}_0$  与特征值  $c$ , 并进而求得全部解为

$$\begin{cases} u_0 = \hat{u}_0(y, z) n_0, & v_0 = \hat{v}_0(y, z) n_0 \xi, \\ w_0 = \hat{w}_0(y, z) n_0 \xi, & \theta_0 = \hat{\theta}_0(y, z) n_0, \end{cases} \quad (36)$$

其中,  $n_0(T, \xi)$  为已知. 将式(31)代入式(28)~(31), 得

$$\begin{aligned} Au_1 = & -\frac{\partial n_0}{\partial T} \hat{u}_0 - \frac{1}{\rho_s} \left( \hat{u}_0^2 n_0 \frac{\partial n_0}{\partial \xi} + \hat{v}_0 \hat{u}_0 n_0 \frac{\partial n_0}{\partial \xi} \right) - \hat{w}_0 \frac{\partial}{\partial z} \left( \frac{\hat{u}_0}{\rho_s} \right) n_0 \cdot n_0 \xi = \\ & -\hat{u}_0 n_0 T - \left( \frac{1}{\rho_s} \hat{u}_0 + \frac{1}{\rho_s} \hat{u}_0 \hat{v}_0 + \hat{w}_0 \frac{\partial}{\partial z} \left( \frac{\hat{u}_0}{\rho_s} \right) \right) n_0 \cdot n_0 \xi, \end{aligned} \quad (37)$$

$$Av_1 = -(\bar{u} - c_0) \hat{v}_0 n_0 \xi \xi, \quad (38)$$

$$Aw_1 = \beta \hat{u}_0 n_0, \quad (39)$$

$$A\theta_1 = -\hat{\theta}_0 n_{0T} - \frac{1}{\rho_s} (\hat{u}_0 \hat{\theta}_0 + \hat{v}_0 \hat{\theta}_{0y}) n_0 n_0 \xi. \quad (40)$$

由于上述两级方程的齐次部分均相同, 从而当  $i = 1$  时, 方程(32)有解的条件可以归结为

$$\begin{aligned} & \iint \hat{p}_0^* \left\{ \frac{\bar{\theta}_{y2}}{(\bar{u}_2 + \alpha)\bar{\theta}_y - \bar{u}_y + 1} \left[ -(\bar{u} - c)^2 v_0 n_0 \xi \xi \xi \right] + \hat{u}_0 n_0 T + \right. \\ & \left. \left( \frac{1}{\rho_s} \hat{u}_0^2 + \frac{1}{\rho_s} \hat{u}_0 \hat{v}_0 + \hat{u}_0 \frac{\partial}{\partial z} \left( \frac{\hat{u}_0}{\rho_s} \right) n_0 n_0 \xi \right) + (\bar{u}_2 + \alpha)(\bar{u} - c)(\beta \hat{u}_0 n_0 \xi) + \right. \\ & \left. (\bar{u}_2 + \alpha) \left( -\hat{\theta}_0 n_0 T - \frac{1}{\rho_s} (\hat{u}_0 \hat{\theta}_0 + \hat{v}_0 \hat{\theta}_{0y}) n_0 n_0 \xi \right) + \right. \\ & \left. (\bar{\theta}_y - 1) \frac{\partial}{\partial y} \left\{ \frac{1}{(\bar{u}_2 + \alpha)\bar{\theta}_y - \bar{u}_y + 1} \left[ -(\bar{u} - c)^2 \hat{v}_0 n_0 \xi \xi \xi \right] + \hat{u}_0 n_0 T + \right. \right. \\ & \left. \left. \left( \frac{1}{\rho_s} \hat{u}_0 + \frac{1}{\rho_s} \hat{u}_0 \hat{v}_0 + \hat{u}_0 \frac{\partial}{\partial z} \left( \frac{\hat{u}_0}{\rho_s} \right) n_0 n_0 \xi \right) + (\bar{u}_2 + \alpha)(\bar{u} - c)(\beta \hat{u}_0 n_0 \xi) + \right. \right. \\ & \left. \left. (\bar{u}_2 + \alpha) \left( -\hat{\theta}_0 n_0 T - \frac{1}{\rho_s} (\hat{u}_0 \hat{\theta}_0 + \hat{v}_0 \hat{\theta}_{0y}) n_0 n_0 \xi \right) \right\} - \frac{\partial}{\partial z} (\bar{u} - c)(\beta \hat{u}_0 n_0 \xi) + \right. \\ & \left. \left( -\frac{\partial \hat{\theta}_0}{\partial z} n_0 T - \frac{\partial}{\partial z} \frac{1}{\rho_s} (\hat{u}_0 \hat{\theta}_0 + \hat{v}_0 \hat{\theta}_{0y}) n_0 n_0 \xi \right) + (-\bar{u} - c) \hat{v}_0 n_0 \xi \xi \xi \right\} dy dz = 0. \quad (41) \end{aligned}$$

将方程(41)整理后, 得到

$$A_1 \frac{\partial n_0}{\partial T} + A_2 \frac{\partial n_0}{\partial \xi} + A_3 n_0 \frac{\partial n_0}{\partial \xi} + A_4 \frac{\partial^3 n_0}{\partial \xi^3} = 0, \quad (42)$$

其中

$$A_1 = \iint \hat{\rho}_0^* \left\{ \frac{\bar{\theta}_{y2}}{(\bar{u}_2 + \alpha)\bar{\theta}_y - \bar{u}_y + 1} (\hat{u}_0 - (\bar{u}_2 + \alpha)\hat{\theta}_0) + (\bar{\theta}_y - 1) \frac{\partial}{\partial y} \left[ \frac{\hat{u}_0}{(\bar{u}_2 + \alpha)\bar{\theta}_y - \bar{u}_y + 1} - (\bar{u}_2 + \alpha)\bar{\theta}_0 \right] - \frac{\partial \hat{\theta}_0}{\partial z} \right\} dydz, \quad (43)$$

$$A_2 = \iint \hat{\rho}_0^* \left\{ \frac{\bar{\theta}_{y2}}{(\bar{u}_2 + \alpha)\bar{\theta}_y - \bar{u}_y + 1} (\beta \hat{u}_0) (\bar{u}_2 + \alpha) (\bar{u} - c) + (\bar{\theta}_y - 1) \frac{\partial}{\partial y} \left[ \frac{1}{(\bar{u}_2 + \alpha)\bar{\theta}_y - \bar{u}_y + 1} (\beta \hat{u}_0) (\bar{u}_2 + \alpha) (\bar{u} - c) \right] - \beta \frac{\partial}{\partial z} [(\bar{u} - c)\hat{u}_0] \right\} dydz, \quad (44)$$

$$A_3 = \iint \hat{\rho}_0^* \left\{ \frac{\bar{\theta}_{y2}}{(\bar{u}_2 + \alpha)\bar{\theta}_y - \bar{u}_y + 1} \left[ \left( \frac{1}{\rho_s} \hat{u}_0^2 + \frac{1}{\rho_s} \hat{u}_0 \hat{v}_0 + \hat{w}_0 \frac{\partial}{\partial z} \left( \frac{\hat{u}_0}{\rho_s} \right) \right) \right] - \frac{(\bar{u}_2 + \alpha)}{\rho_s} (\hat{u}_0 \hat{\theta}_0 + \hat{v}_0 \hat{\theta}_{0y}) \right\} + (\bar{\theta}_y - 1) \frac{\partial}{\partial y} \left[ \frac{\bar{\theta}_{y2}}{(\bar{u}_2 + \alpha)\bar{\theta}_y - \bar{u}_y + 1} \left( \hat{u}_0 \frac{\partial}{\partial z} \left( \frac{\hat{u}_0}{\rho_s} \right) + \frac{1}{\rho_s} \hat{u}_0^2 + \frac{1}{\rho_s} \hat{u}_0 \hat{v}_0 \right) - \frac{(\bar{u}_2 + \alpha)}{\rho_s} (\hat{u}_0 \hat{\theta}_0 + \hat{v}_0 \hat{\theta}_{0y}) \right] - \frac{\partial}{\partial z} \left( \frac{1}{\rho_s} (\hat{u}_0 \hat{\theta}_0 + \hat{v}_0 \hat{\theta}_{0y}) \right) \right\} dydz, \quad (45)$$

$$A_4 = \iint \hat{\rho}_0^* \left\{ \frac{\bar{\theta}_{y2} \hat{v}_0}{(\bar{u}_2 + \alpha)\bar{\theta}_y - \bar{u}_y + 1} [- (\bar{u} - c)^2] + (\bar{\theta}_y - 1) \frac{\partial}{\partial y} \left[ \frac{-\hat{v}_0 (\bar{u} - c)^2}{(\bar{u}_2 + \alpha) - \bar{u}_y + 1} \right] - (\bar{u} - c) \hat{v}_0 \right\} dydz, \quad (46)$$

$\hat{\rho}_0^*$  是  $\ell(\hat{\rho}_0) = 0$  的共轭方程的解,由下式定义:

$$\ell_{y,z}^*(\hat{\rho}_0^*) = 0. \quad (47)$$

上述得到的关于振幅  $n_0(T, \xi)$  的非线性方程为推广的 KdV 方程(即方程(42)),利用椭圆函数展开法,能够得到孤立波解为

$$A(\xi, T) = \frac{4\beta k^2(1 + m^2) + c_1 - \gamma'}{\alpha'} - \frac{12\beta k^2 m^2}{\alpha'} \operatorname{sn}^2(k(\xi - c_1 T)),$$

它包含了频散过程和非线性过程.特别注意系数  $A_2$ , 说明 Coriolis 力的水平分量也是影响赤道大气 Rossby 孤波的一个重要因子,会影响孤立波的频率特征,这里不需要借助于地形作用,也可以得到类似的结论.同时方程(42)中的  $A_2$  项表征由于 Coriolis 水平分量参数所得的项,这是与以往任何方程所不同的地方,亦即我们得到了带有水平分量的描述斜压大气的 Rossby 波动问题,这是以前所没有的结果.



## 4 结 论

本文从大气运动基本方程组出发,研究了完整 Coriolis 力作用下的中高纬非线性 Rossby 波振幅的演化规律,说明 Coriolis 水平分量也是产生赤道大气孤立波的重要因子,指出 Coriolis 力水平分量能够影响波动传播的频率特征.孤立波解也表明 Coriolis 水平分量对赤道非线性波动的影响.

需要指出的是,从直观上讲,由于本文对热力作用和摩擦作用没有考虑,无疑会造成与观测上的不同,所以这些需要进一步的讨论.

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# Nonlinear Near Inertial Waves With Complete Coriolis Effects

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**Abstract:** Based on the original basic equations of atmospheric motion under the action of the complete Coriolis force, through the scale analysis, the multi-scale method and the perturbation expansion method were used to derive the Korteweg-de Vries equation satisfying the amplitude evolution of the atmospheric near inertial wave at the mid-high latitudes. The results of the evolution equation show that, the influence of the horizontal component of the Coriolis parameter on the nonlinear near inertial wave mainly lies in the correction of the dispersion effect and the interaction with the elementary stream. The physical mechanism of atmospheric near inertial wave motion at the mid-high latitudes under the action of the complete Coriolis force was theoretically explained.

**Key words:** near inertial wave; complete Coriolis force; Korteweg-de Vries equation

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